

# 第57回 自動制御連合講演会

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## Voltage Mode Control Using Triangular Wave Slope Modulation for DC-DC Buck Converter

Shu WU, Yasunori KOBORI, Nobukazu Tsukiji , Haruo KOBAYASHI

Division of Electronics and Informatics

Gunma University

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# OUTLINE

- Research Objective
- Proposed Triangular Wave Generator
  - Slope Adjustable Triangular Wave Generator
  - Improvement of Transient Response
  - Stability Analysis
- Simulation Results
  - Line Transient Response
  - Load Transient Response
- Conclusion

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# Transient Response

- 3 disturbance sources
  - Output reference signal ← 😊 Band-gap reference
  - Input voltage ← 😊 Line feed-forward control
  - Load 😞 Trouble

Fast dynamic current slew rate presents challenge in load transient response of power supplies

# Conventional Control Schemes

- Feedback

- Voltage-Mode Control (VMC)

- Easy to design and analyze
    - Without line feed-forward control
    - Limited bandwidth: slow response

- Current-Mode Control (CMC)

- Inherent line feed-forward control (for BUCK)
    - Wide band
    - Slope compensation
    - Current sensor

- Feed-forward

Complicated non-linear calculation

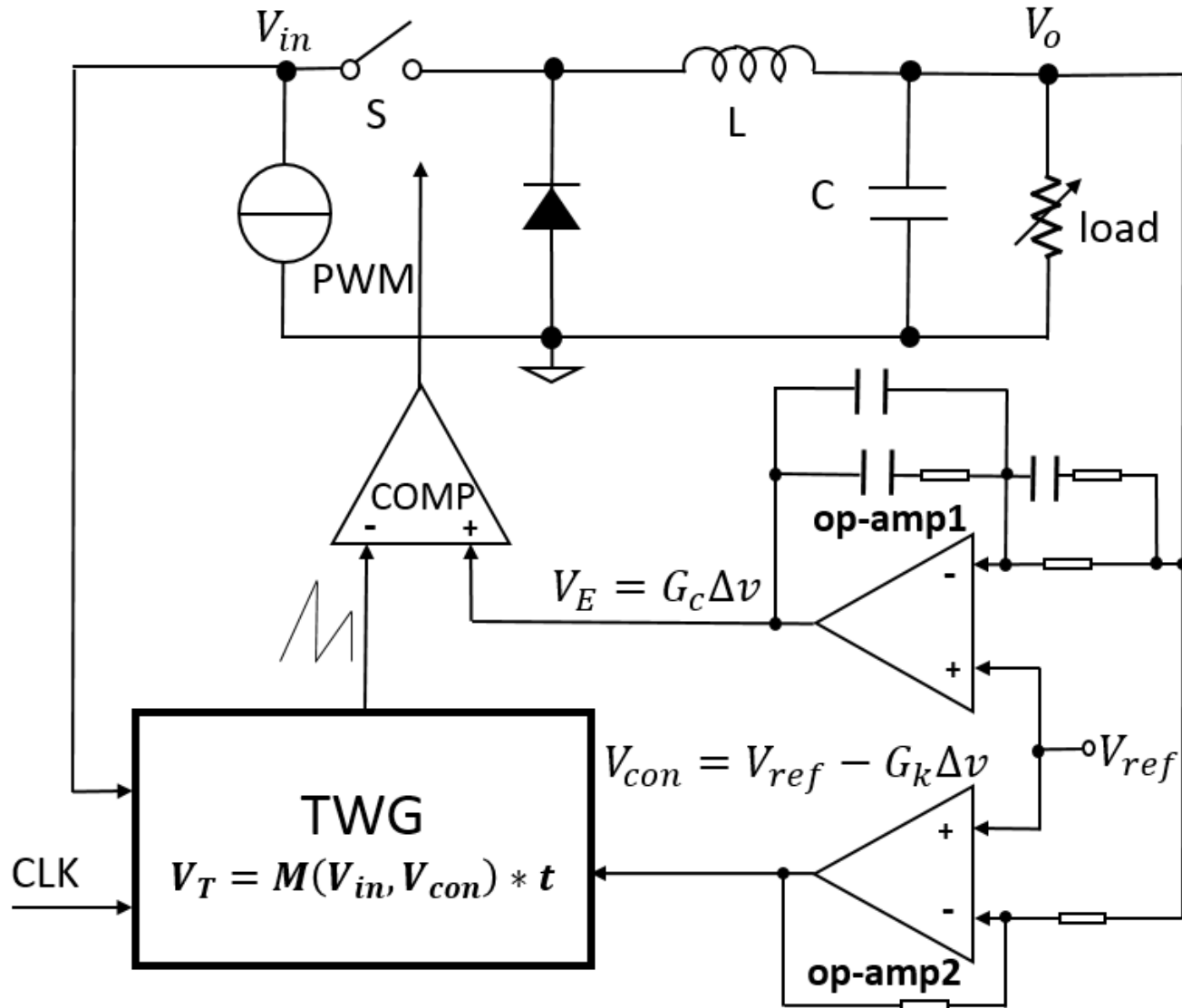
# Research Objective

- Design a slope adjustable triangular wave generator to improve transient response of DC-DC buck converter
  - **Based on VMC:**  
compared to CMC
    - Not require current sensor or slope compensation
  - **Slope is regulated by input and output voltages:**  
compared to conventional VMC
    - Provide line feed-forward control and wideband
  - **Simple:**  
compared to previous feed-forward control
    - Not require complicated calculation

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# System Configuration



## Op-amp1:

- Generate error signal
- Type 3 compensation

## Op-amp2:

- Amplify deviation
- Control variable of TWG

## TWG (Triangular Wave Generator):

Slope adjustable

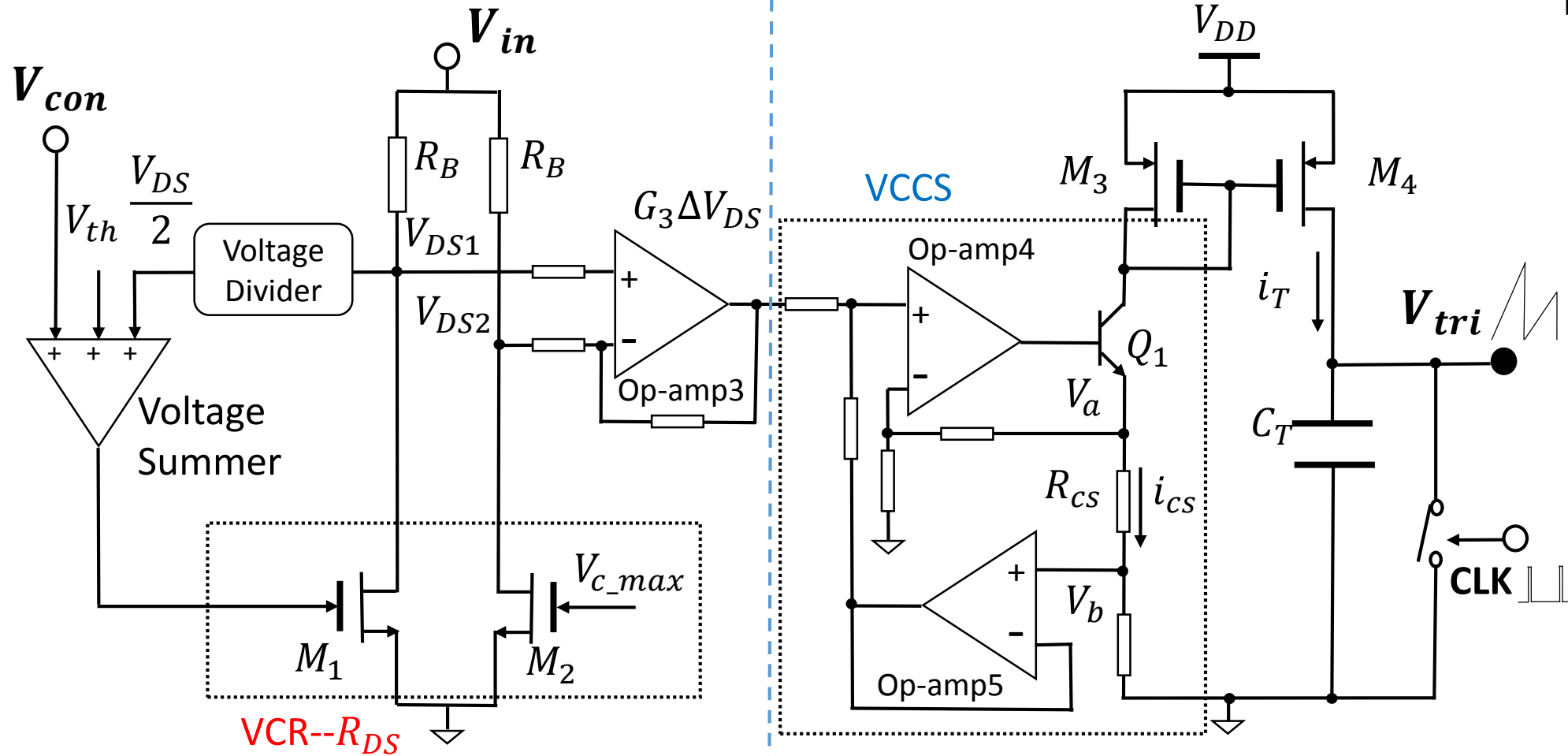
- Controlled by  $V_{in}$  and  $V_{con}$



# Triangular Wave Generator (1)

Part 1

Part 2

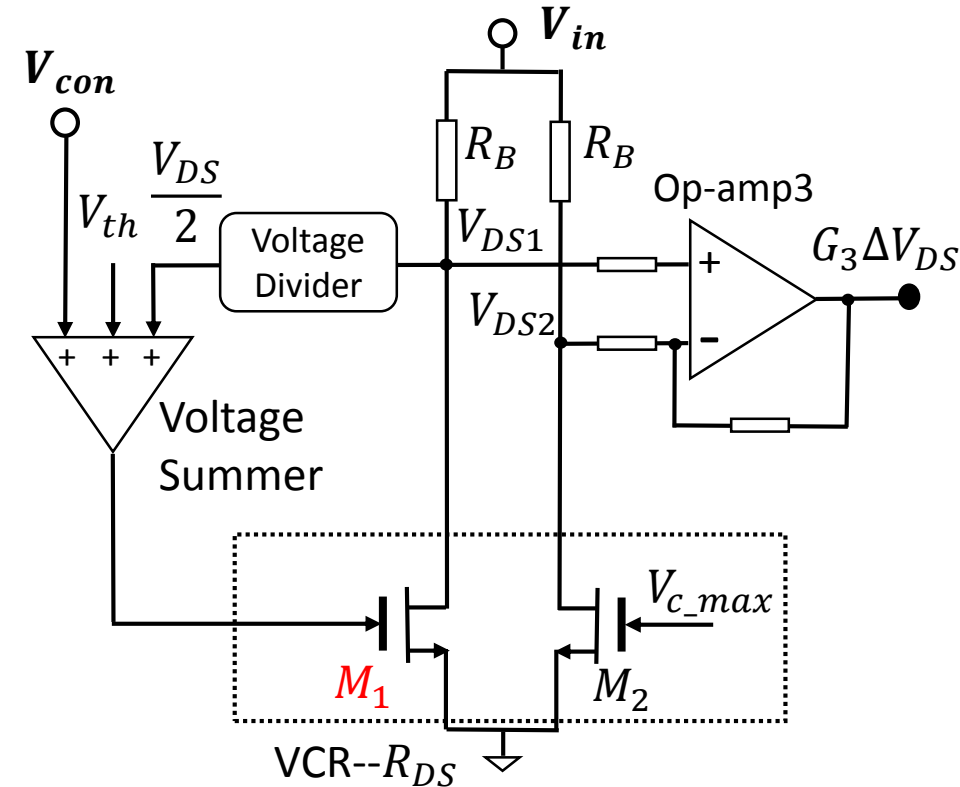


VCR: Voltage Controlled Resistor

VCCS: Voltage Controlled Current Source

# Triangular Wave Generator (2)---Part 1

- VCR



NMOS  $M_1$  operates in **triode** region

Equivalent resistor:

$$\frac{1}{R_{DS}} = \frac{I_D}{V_{DS}} = K_n \left( V_{GS} - V_{th} - \frac{V_{DS}}{2} \right)$$



$$\text{Set } V_{GS} = V_{th} + \frac{V_{DS}}{2} + V_{con}$$

$$R_{DS} = \frac{1}{K_n V_{con}}$$

If  $R_B \gg R_{DS}$

$$V_{DS} \approx \frac{1}{K_n R_B} \frac{V_{in}}{V_{con}}$$

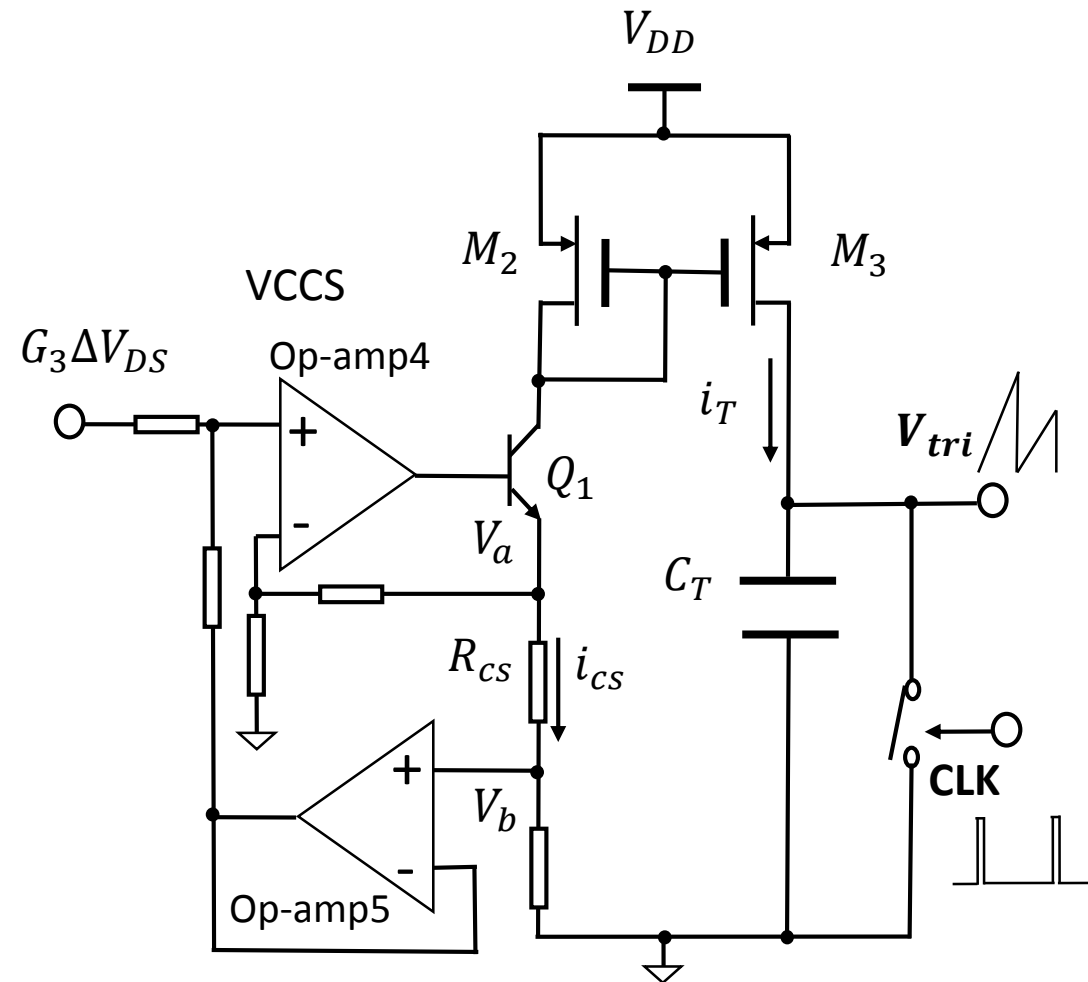
$$G_3 \Delta V_{DS} = \frac{G_3 V_{in}}{K_n R_B} \left( \frac{1}{V_{con}} - \frac{1}{V_{con\_max}} \right)$$

※  $K_n = \mu_n C_{ox} W/L$

$$V_{c\_max} = V_{th} + \frac{V_{DS}}{2} + V_{con\_max}$$

# Triangular Wave Generator (3)---Part 2

- VCCS & TWG



$$i_T = i_{CS} = \frac{V_a - V_b}{R_{CS}} = \frac{G_3 \Delta V_{DS}}{R_{CS}}$$

$$V_{tri} = \frac{i_T}{C_T} t$$

$$V_{tri} = V_{in} \left( a \frac{1}{V_{con}} - b \right) t = M(V_{in}, V_{con}) t$$

$$\text{Where } a = \frac{G_3}{K_n R_B R_{CS} C_T}, \quad b = \frac{a}{V_{con\_max}}$$

$$M \propto V_{in}, \quad M \propto \frac{1}{V_{con}}$$

# Line Transient Response Improvement

----- Line feed-forward control

Transfer function from error signal to output voltage  
(VMC buck converter)

$$V_{out} = \frac{1}{LCs^2 + \frac{L}{R}s + 1} \frac{V_{in}}{V_P} V_E$$

Since  $V_p = MT_s$ , and M depends on  $V_{in}$  (proportional) and  $V_{con}$



Input voltage change effects are reduced.

$V_P$  --- the peak of triangular wave

# Load Transient Response Improvement (1)

----- Additional duty cycle modulation

$\Delta d_1$  is caused by **slope** modulation

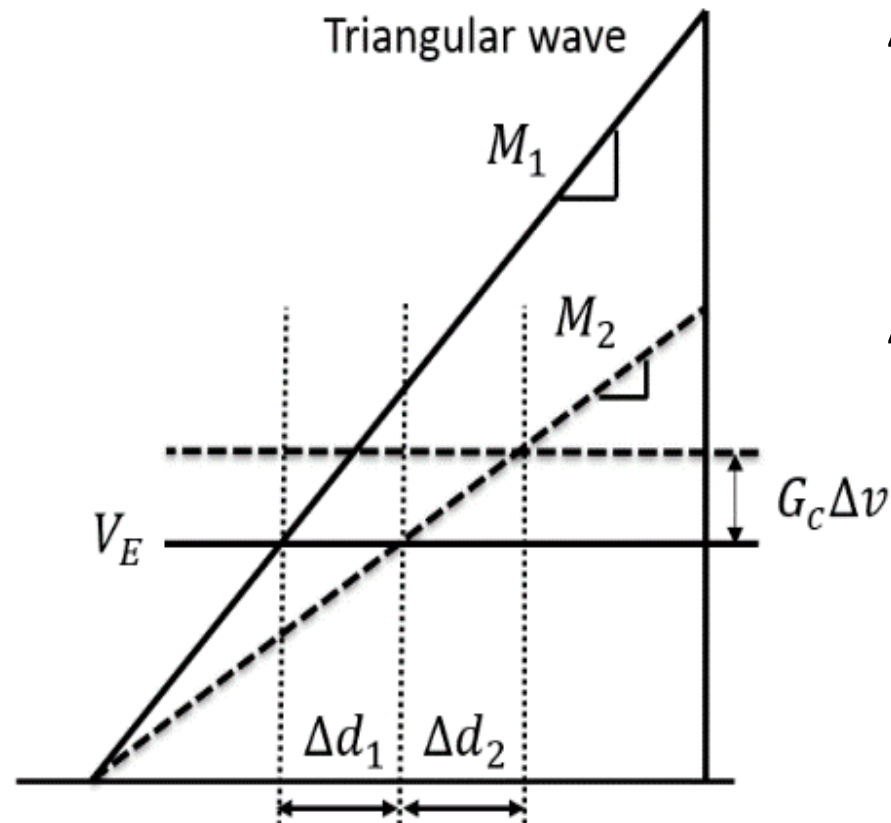
$$\Delta d_1 = \frac{V_E}{T_s} \left( \frac{1}{M_2} - \frac{1}{M_1} \right) = \frac{V_E}{T_s} \Delta \frac{1}{M}$$

$\Delta d_2$  is caused by **slope** and **error** modulations

$$\Delta d_2 = \frac{G_c \Delta v}{T_s} \left( \frac{1}{M_1} + \Delta \frac{1}{M} \right) = \frac{G_c \Delta v}{T_s M_1} + \frac{G_c \Delta v}{T_s} \Delta \frac{1}{M}$$

$$\Delta d = \Delta d_1 + \Delta d_2 = \underbrace{\left( \frac{V_E}{T_s} + \frac{G_c \Delta v}{T_s} \right) \Delta \frac{1}{M}}_{\text{Additional duty cycle modulation by proposed TWG--}\Delta d_s} + \underbrace{\frac{G_c \Delta v}{T_s M_1}}_{\text{Conventional VMC--}\Delta d_e}$$

Additional duty cycle modulation by proposed TWG-- $\Delta d_s$       Conventional VMC-- $\Delta d_e$



$$V_{p\_static} = T_s M_1$$

# Load Transient Response Improvement (2)

----- Non-linear control features

$$\Delta d = \left( \frac{V_E}{T_s} + \frac{G_c \Delta v}{T_s} \right) \left( \frac{(V_{ref} + G_k \Delta v)}{V_{in} (a - b(V_{ref} + G_k \Delta v))} - \frac{V_{ref}}{V_{in} (a - bV_{ref})} \right) + \frac{G_c \Delta v}{V_{p\_static}}$$



$$\Delta d = A \Delta v + \frac{G_c \Delta v}{V_{p\_static}}$$

$$A(\Delta v) = \frac{a G_k (V_E + G_c \Delta v)}{T_s V_{in} (a - b V_{ref}) (a - b V_{ref} - b G_k \Delta v)}$$

Large

Large

—————> Enable fast transient response

$\Delta v$



$A$



Non-linearly change

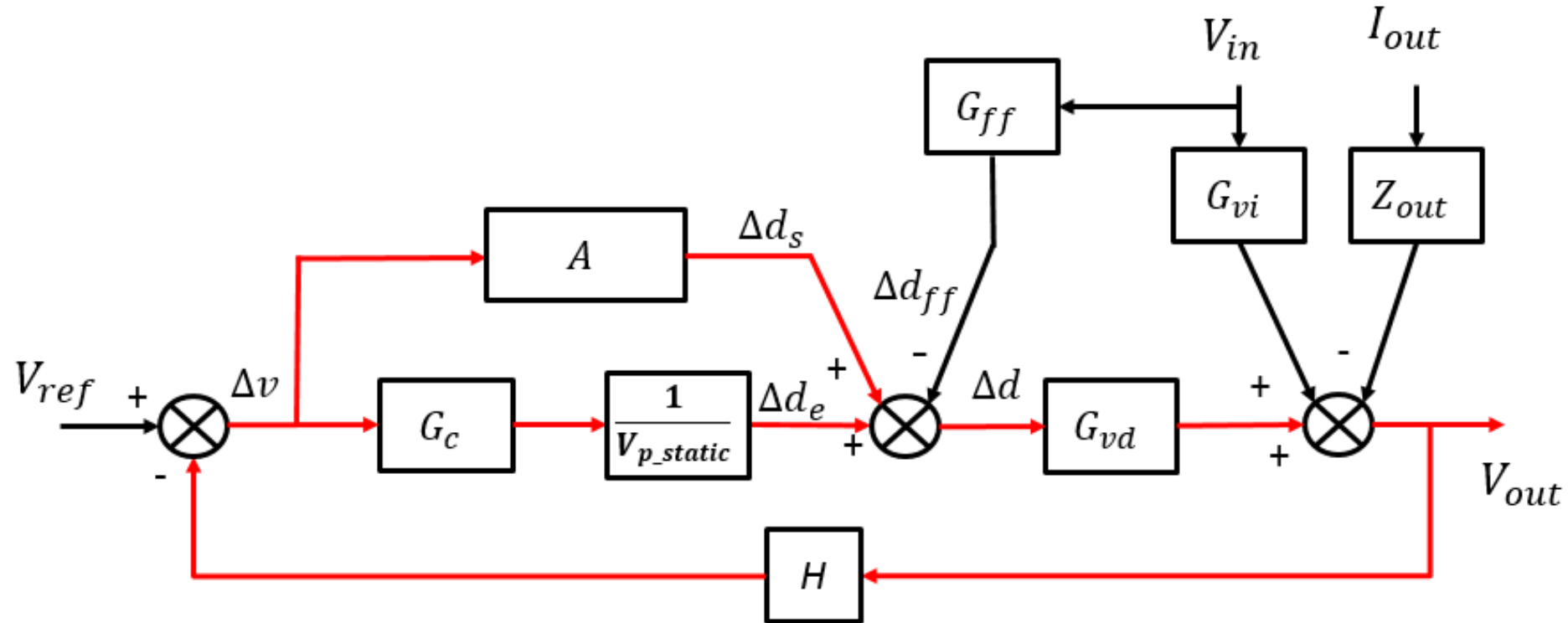
approach to 0

approach to a constant

—————> To ensure the loop stability

# System Block Diagram

Supposing  $\Delta v$  is enough small, and  $A$  is approximated as constant



$$\text{Open-loop transfer function: } T = \left( A + \frac{G_c}{V_{p\_static}} \right) G_{vd} H$$

# Example

## Power Stage

- $V_{in} = 5V$
- $V_{out} = 3.5V$
- $V_{p\_static} = 3V$
- $L = 10\mu H$  ( $ESR = 10m\Omega$ )
- $C = 50\mu F$  ( $ESR = 10m\Omega$ )
- $R = 35\Omega$
- $f_{switch} = 1MH$

## Phase Compensation

- Type 3 compensation
- $f_c = \frac{f_{switch}}{20} = 50kHz$
- $PM = 40^\circ$

Design for conventional VMC

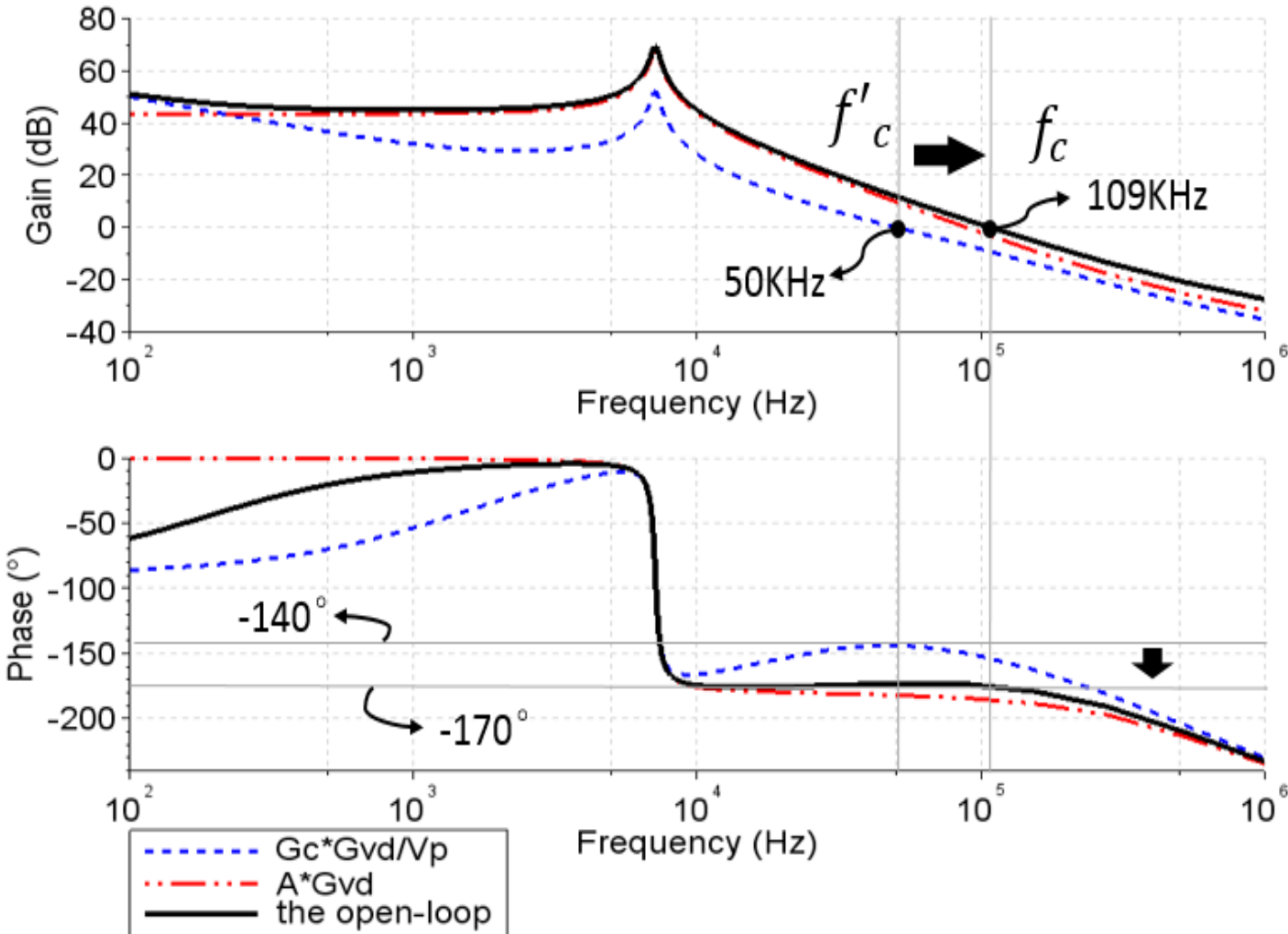
## TWG

- $G_k = 10$
- $R_B = 1k\Omega$
- $K_n \approx 3$
- $R_{cs} = 100\Omega$
- $C_T = 50pF$

**$A \approx 30$**



# Bode Plot

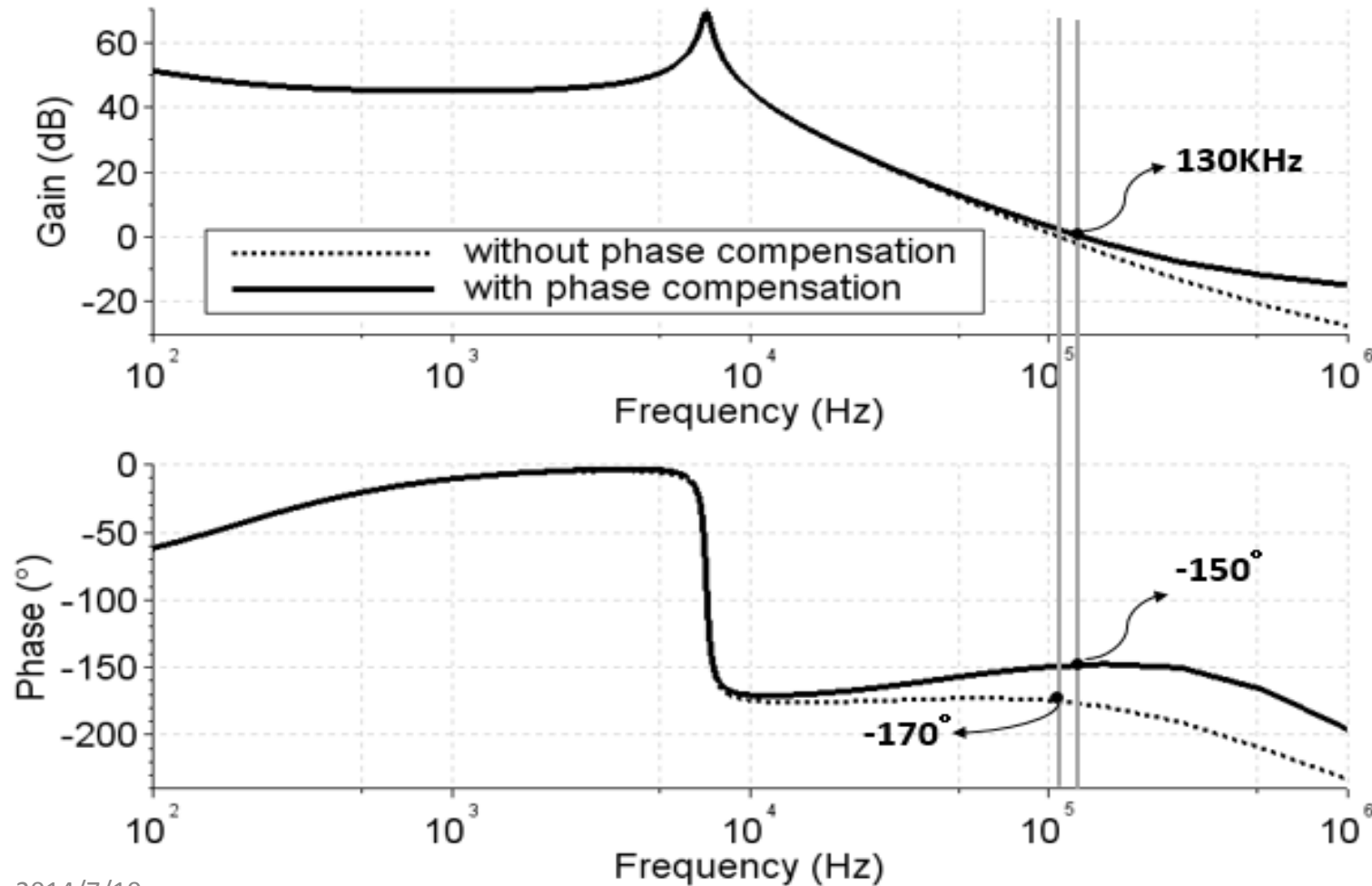


Compare to conventional VMC  
 ---  $(G_c G_{vd} / V_p)$

- Bandwidth is **increased**  
 50kHz  $\rightarrow$  109kHz
- Phase margin is **decreased**  
 40°  $\rightarrow$  10°

# Increase Phase Margin

Add a high frequency zero point to A:  $A \rightarrow A * (s + \omega_h)$



- Bandwidth

109kHz  $\rightarrow$  130kHz

- Phase Margin

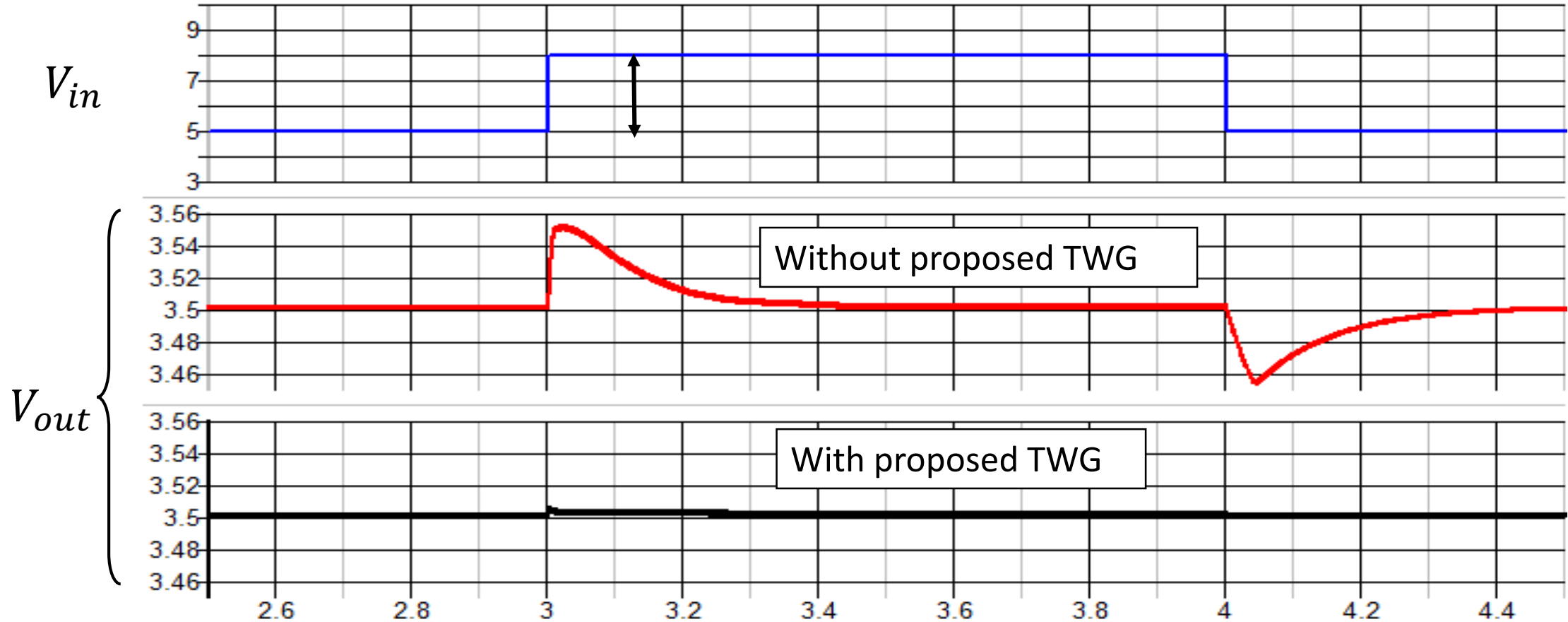
$10^\circ \rightarrow 30^\circ$

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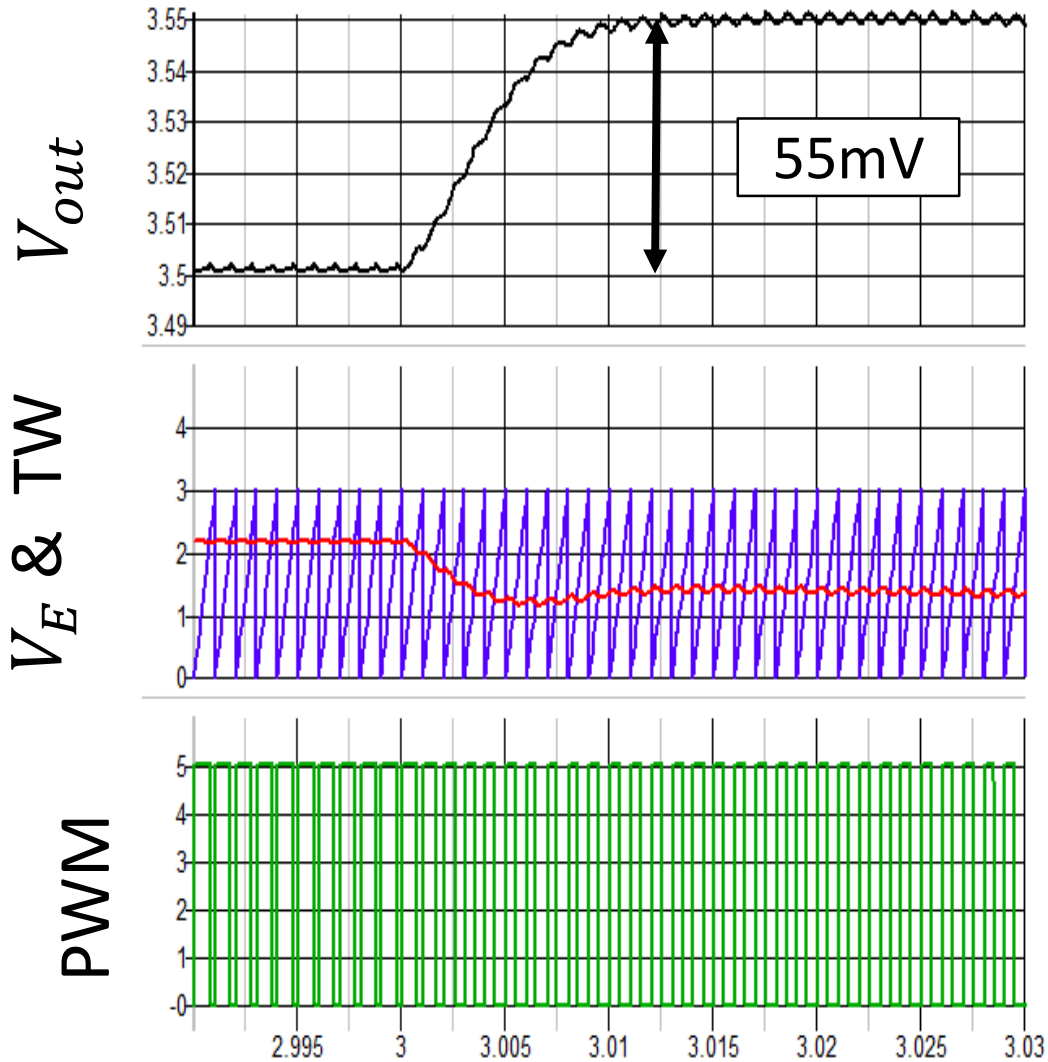
# Line Transient Response (1)

$V_{in}: 5V \leftrightarrow 8V$

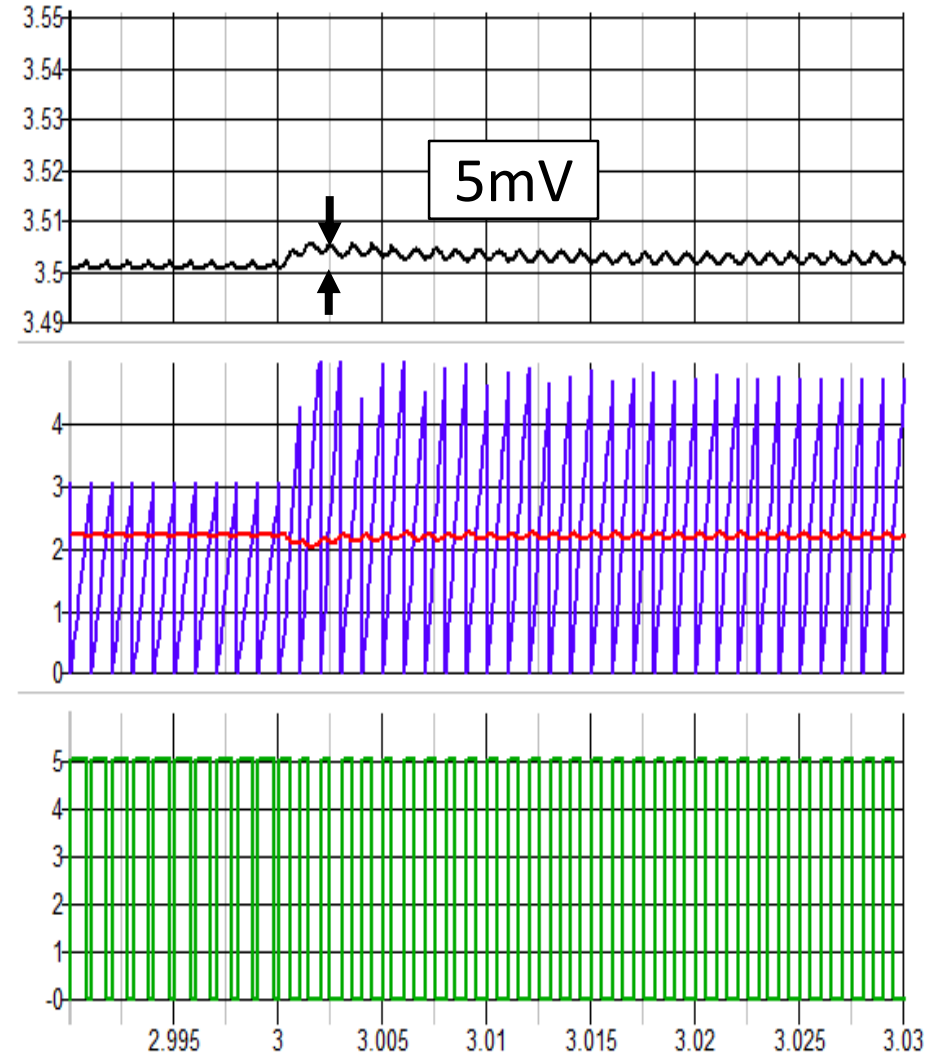


( Simulation conditions are shown in P16)

# Line Transient Response (2)



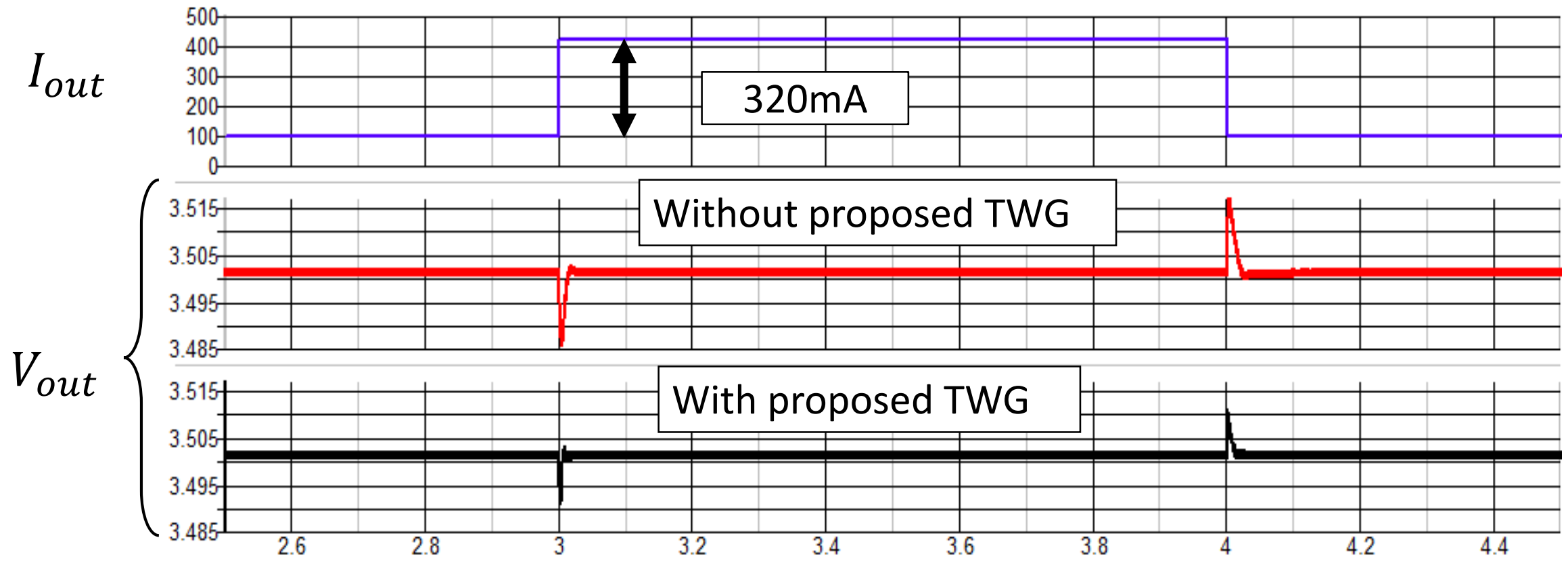
**Without** proposed TWG



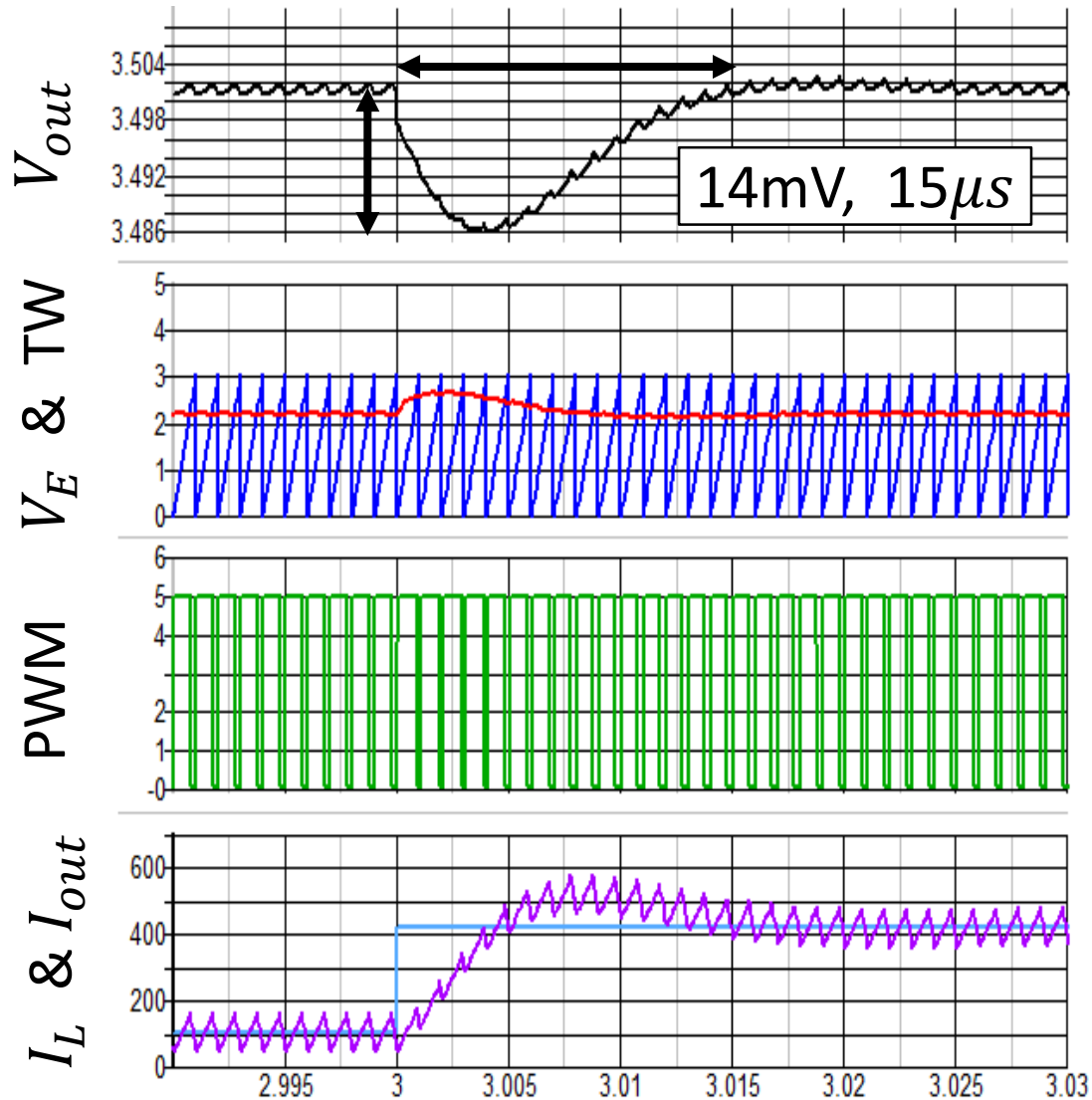
**With** proposed TWG

# Load Transient Response (1)

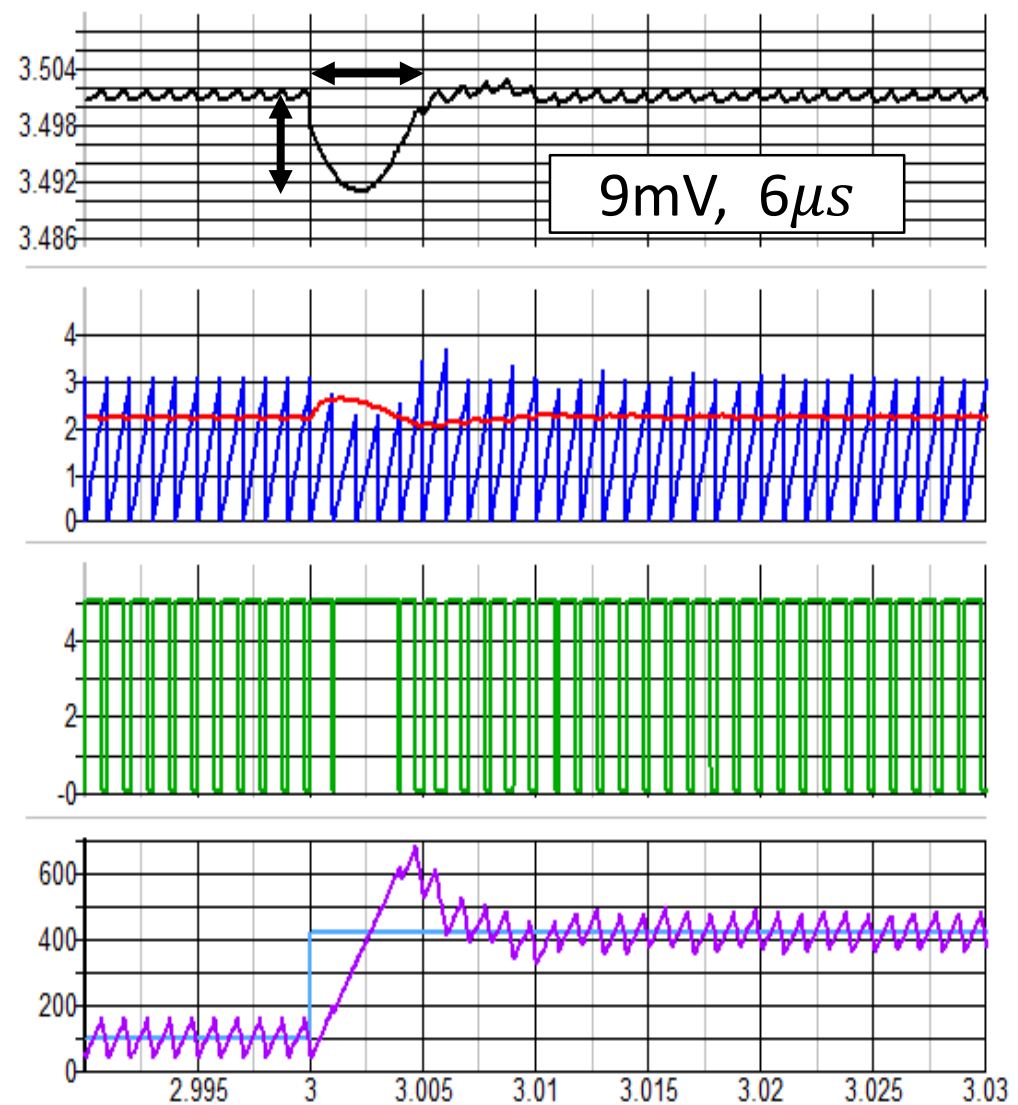
$I_{out}$ : 100mA  $\leftrightarrow$  420mA



# Load Transient Response (2) --- step up

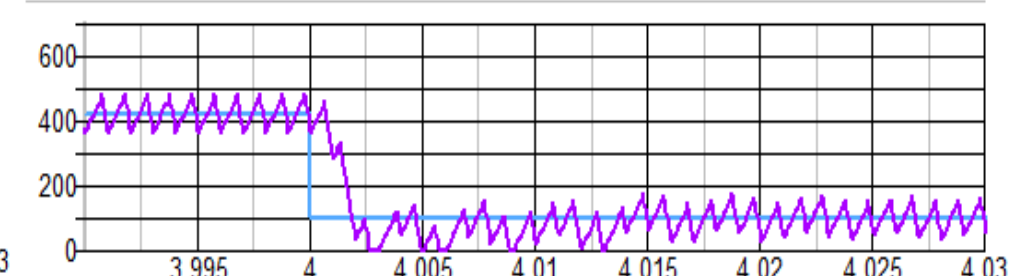
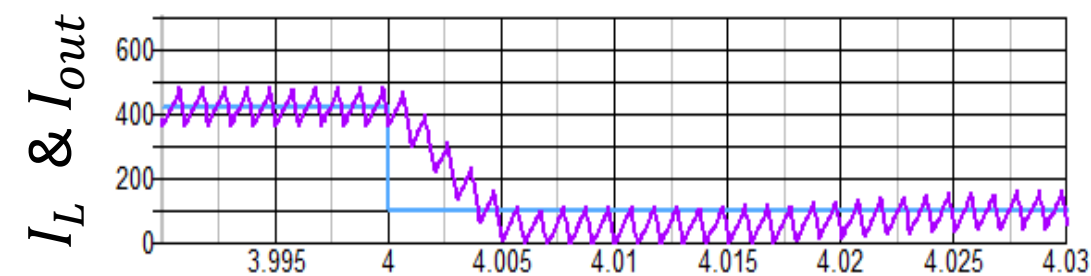
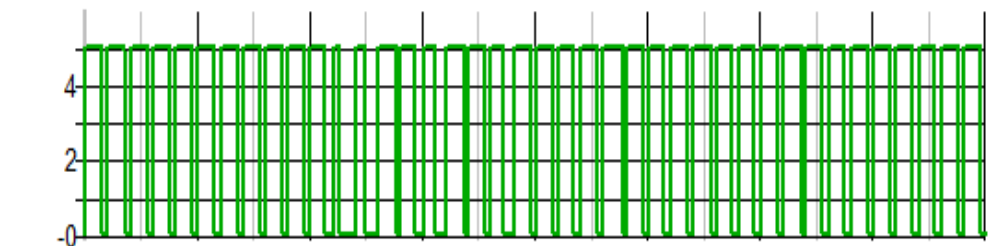
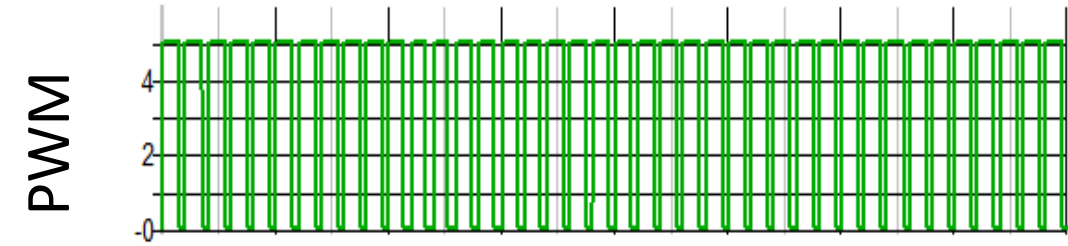
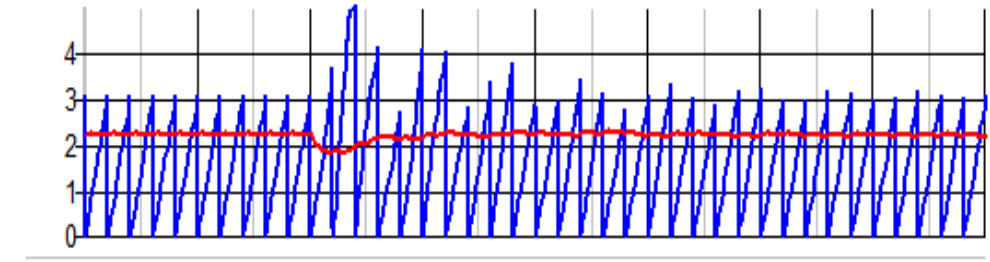
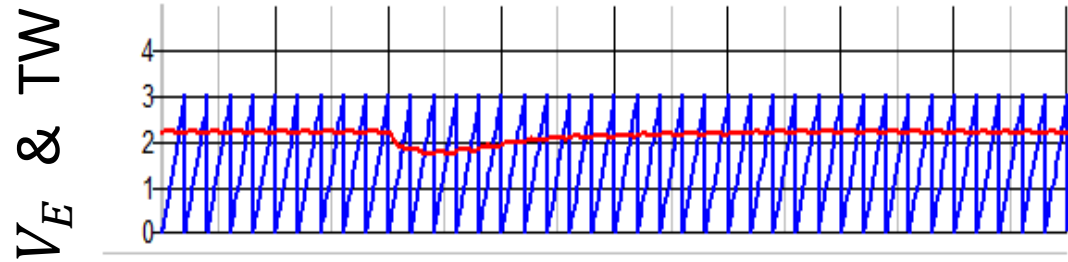
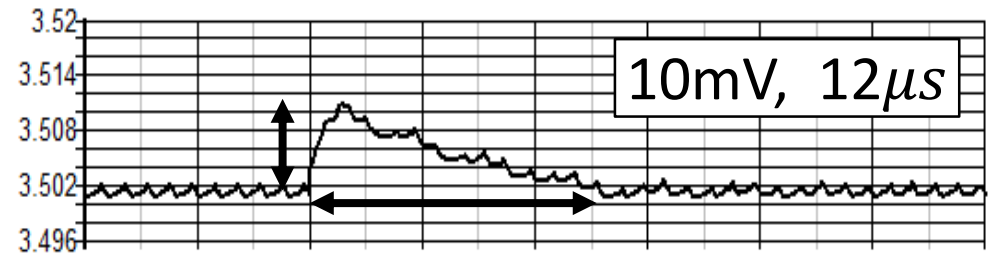
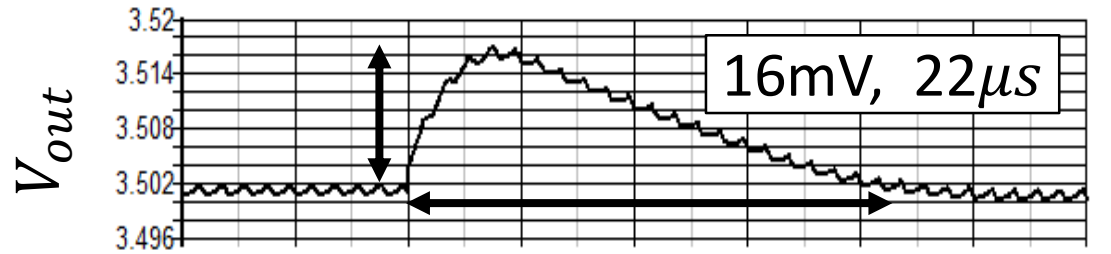


**Without** proposed TWG



**With** proposed TWG

# Load Transient Response (3) --- step down



**Without proposed TWG**

**With proposed TWG**



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# Conclusion

- Design a slope adjustable triangular wave generator for DC-DC converter.
  - Line and load transient response improvement
  - Simple
    - Not require current sensor or slope compensation
- Next Step  
Circuit implementation

# The End

Thanks for your attention

# Q&A

- The proposed method causes the phase margin decrease. How do you deal with this problem?

A: the reason of phase margin decrease is the phase of additional feedback loop ( $A \cdot G_{vd}$ ) is too low. Therefore I try to increase the phase of  $A \cdot G_{vd}$  at high frequency. We can add a high-frequency zero point in  $A$ . This can be realized through insert a appropriate capacitor in op-amp2 (Page 8) or op-amp3 (Page 9). By this way, the phase of  $A \cdot G_{vd}$  is increased at the crossover frequency, the phase margin also increase.