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群馬大学 GUNMA UNIVERSITY

Dynamic Performance Improvement of DC-DC Buck Converter by Slope Adjustable Triangular Wave Generator

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November 4, 2014

OUTLINE

- Research Objective
- Proposed Triangular Wave Generator
  - Slope Adjustable Triangular Wave Generator
  - Improvement of Transient Response
- Simulation Results
  - Line Transient Response
  - Load Transient Response
- Conclusion

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Transient Response

- 3 disturbance sources
  - Output reference signal ⬅ ☺ Band-gap reference
  - Input voltage ⬅ ☺ Line feed-forward control
  - Load ☹ Trouble

Fast dynamic current slew rate presents challenge in load transient response of power supplies

Conventional Control Schemes

- Feedback
  - Voltage-Mode Control (VMC)
    - Easy to design and analyze
    - Without line feed-forward control
    - Limited bandwidth: slow response
  - Current-Mode Control (CMC)
    - Inherent line feed-forward control (for BUCK)
    - Wide band
    - Slope compensation
    - Current sensor
- Feed-forward

Complicated non-linear calculation

Research Objective

- Design a slope adjustable triangular wave generator to improve transient response of DC-DC buck converter
  - **Based on VMC:**
    compared to CMC
    ---Not require current sensor or slope compensation
  - **Slope is regulated by input and output voltages:**
    compared to conventional VMC
    ---Provide line feed-forward control and wideband
  - **Simple:**
    compared to previous feed-forward control
    ---Not require complicated calculation

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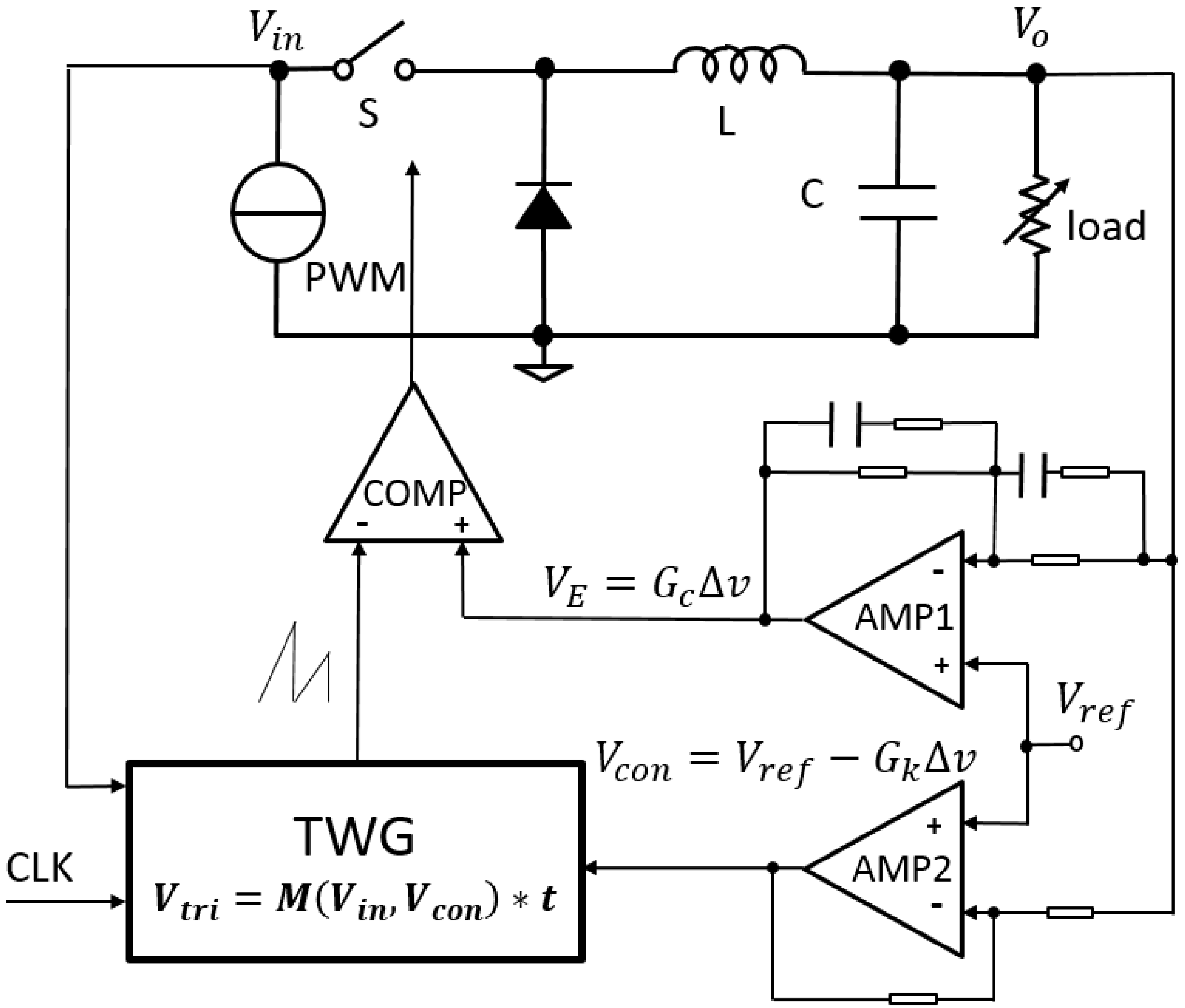
System Configuration



Op-amp1:

- Generate error signal
- Type 3 compensation

Op-amp2:

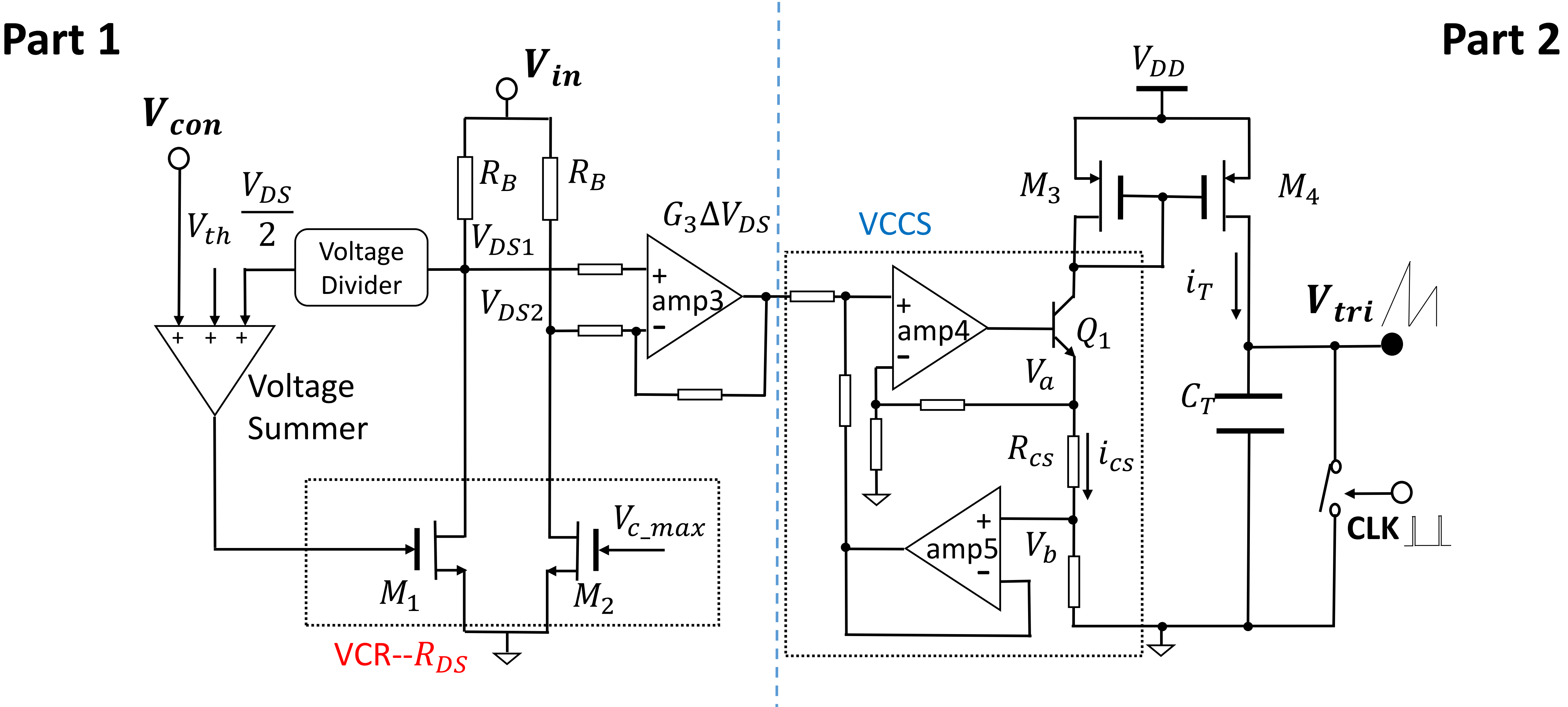
- Amplify deviation
- Control variable of TWG

TWG (Triangular Wave Generator):

Slope adjustable

- Controlled by V_{in} and V_{con}

Triangular Wave Generator (1)

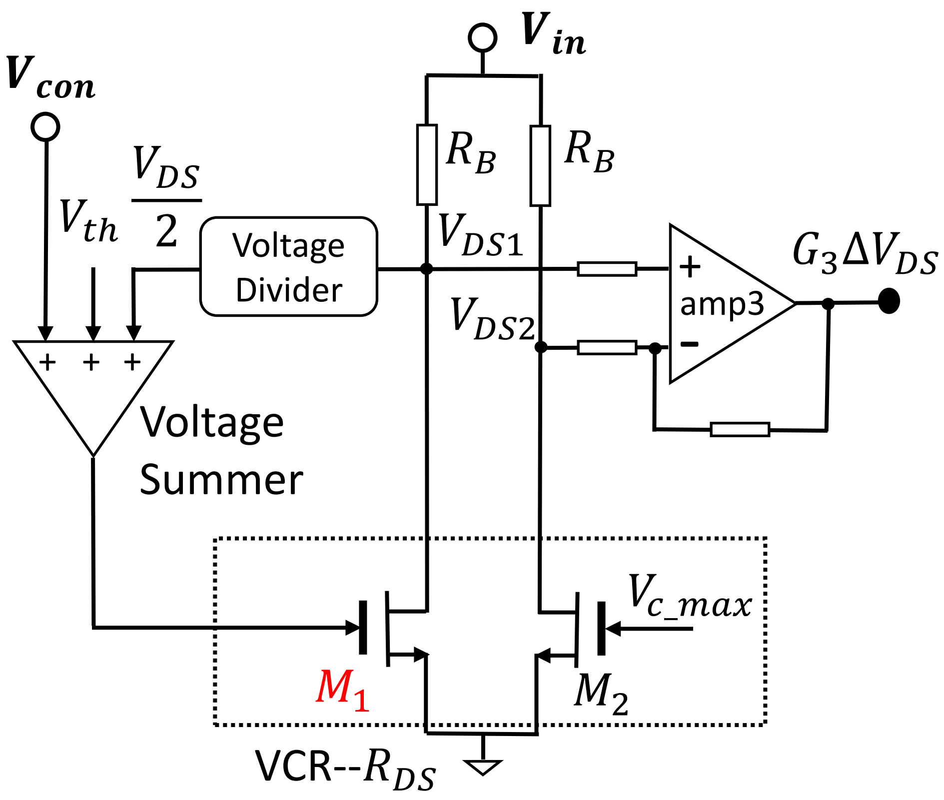


VCR: Voltage Controlled Resistor

VCCS: Voltage Controlled Current Source

Triangular Wave Generator (2)---Part 1

- VCR



NMOS M_1 operates in **triode** region

Equivalent resistor:

$$\frac{1}{R_{DS}} = \frac{I_D}{V_{DS}} = K_n\left(V_{GS} - V_{th} - \frac{V_{DS}}{2}\right)$$

Set $V_{GS} = V_{th} + \frac{V_{DS}}{2} + V_{con}$

$$R_{DS} = \frac{1}{K_n V_{con}}$$

If $R_B \gg R_{DS}$

$$V_{DS} \approx \frac{1}{K_n R_B}\frac{V_{in}}{V_{con}}$$

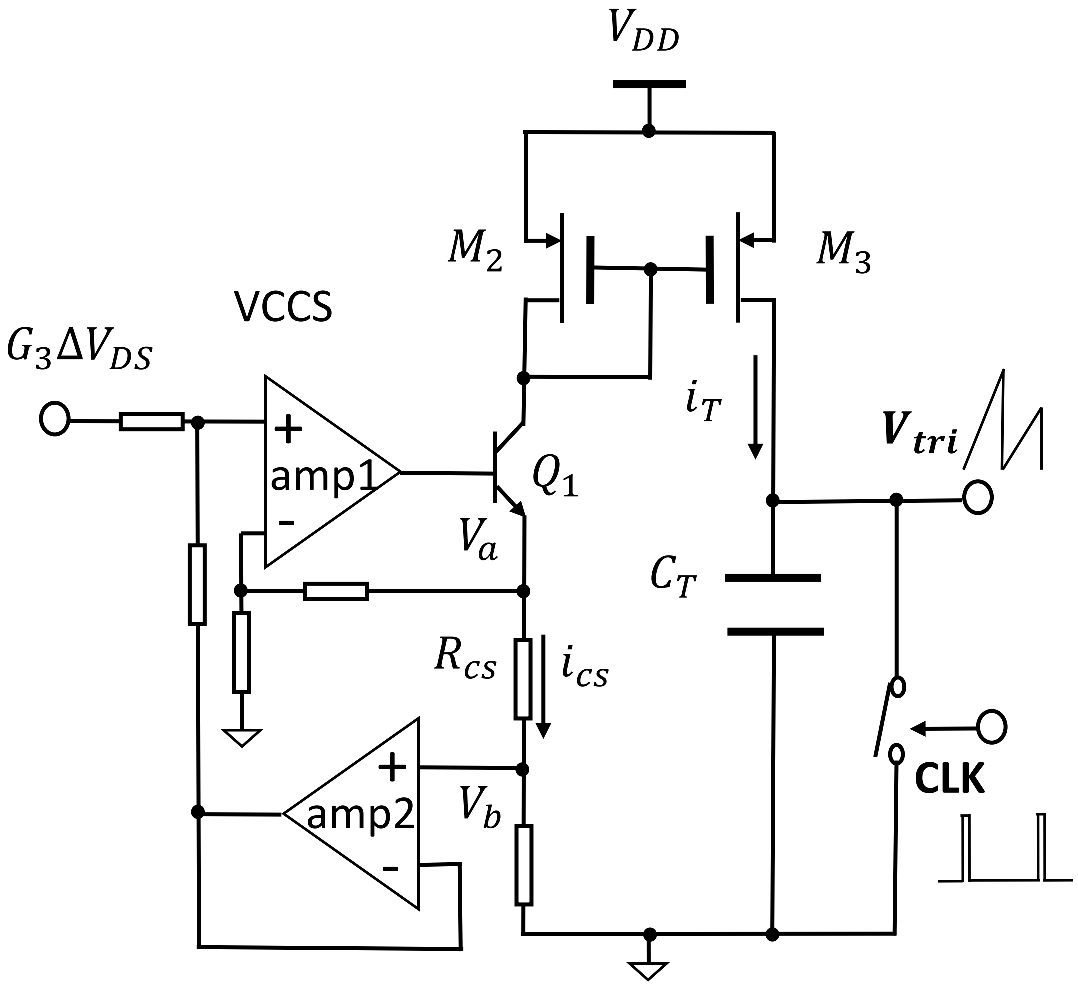
$$G_3\Delta V_{DS} = \frac{G_3 V_{in}}{K_n R_B}\left(\frac{1}{V_{con}} - \frac{1}{V_{con\_max}}\right)$$

※ $K_n = \mu_n C_{ox} W/L$

$V_{c\_max} = V_{th} + \frac{V_{DS}}{2} + V_{con\_max}$

Triangular Wave Generator (3)---Part 2

- VCCS & TWG



$$i_T = i_{CS} = \frac{V_a - V_b}{R_{CS}} = \frac{G_3 \Delta V_{DS}}{R_{CS}}$$

$$V_{tri} = \frac{i_T}{C_T} t$$

$$V_{tri} = V_{in}\left(a\frac{1}{V_{con}} - b\right)t = M(V_{in}, V_{con})t$$

Where $a = \dfrac{G_3}{K_n R_B R_{CS} C_T}$, $b = \dfrac{a}{V_{con\_max}}$

$$M \propto V_{in} \,,\; M \propto \frac{1}{V_{con}}$$

Line Transient Response Improvement

------ Line feed-forward control

Transfer function from error signal to output voltage (VMC buck converter)

$$V_{out} = \frac{1}{LCs^2 + \frac{L}{R}s + 1} \frac{V_{in}}{V_P} V_E$$

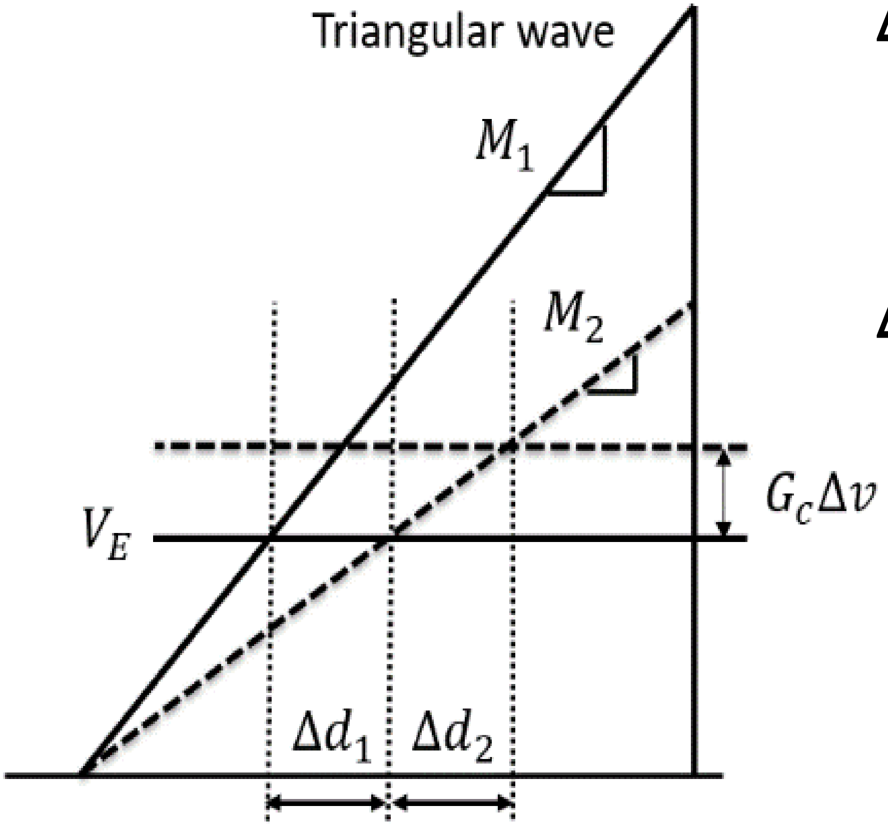
Since $V_p = MT_s$, and M depends on V_{in} (proportional) and V_{con}

Input voltage change effects are reduced.

V_P --- the peak of triangular wave

Load Transient Response Improvement

------ Additional duty cycle modulation



Δd_1 is caused by slope modulation

$$\Delta d_1 = \frac{V_E}{T_s}\left(\frac{1}{M_2} - \frac{1}{M_1}\right) = \frac{V_E}{T_s}\Delta\frac{1}{M}$$

Δd_2 is caused by slope and error modulations

$$\Delta d_2 = \frac{G_c\Delta v}{T_s}\left(\frac{1}{M_1} + \Delta\frac{1}{M}\right) = \frac{G_c\Delta v}{T_s M_1} + \frac{G_c\Delta v}{T_s}\Delta\frac{1}{M}$$

$$\boldsymbol{\Delta d = \Delta d_1 + \Delta d_2 = \underbrace{\boxed{\left(\frac{V_E}{T_s} + \frac{G_c\Delta v}{T_s}\right)\Delta\frac{1}{M}}}_{\text{Additional duty cycle modulation by proposed TWG--}\Delta d_s} + \underbrace{\boxed{\frac{G_c\Delta v}{T_s M_1}}}_{\text{Conventional VMC--}\Delta d_e}}$$

Additional duty cycle modulation by proposed TWG--Δd_s

Conventional VMC--Δd_e

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Simulation Conditions

Power Stage

- $V_{in} = 5V$
- $V_{out} = 3.5V$
- $V_{p\_static} = 3V$
- $L = 10\mu H\ (ESR = 10m\Omega)$
- $C = 50\mu F(ESR = 10m\Omega)$
- $R = 35\Omega$
- $f_{switch} = 1MH$

Phase Compensation

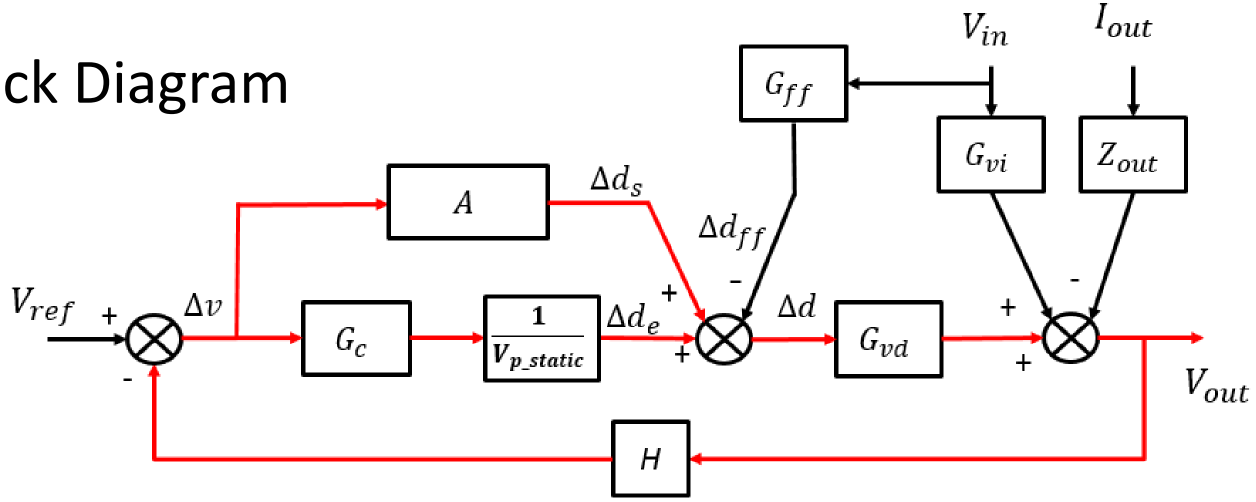
- Type 3 compensation
- $f_c = \frac{f_{switch}}{20} = 50kHz$
- $\text{PM} = 40°$

TWG

- $G_k = 10$
- $R_B = 1k\Omega$
- $K_n \approx 3$
- $R_{cs} = 100\Omega$
- $C_T = 50pF$

Frequency Characteristics

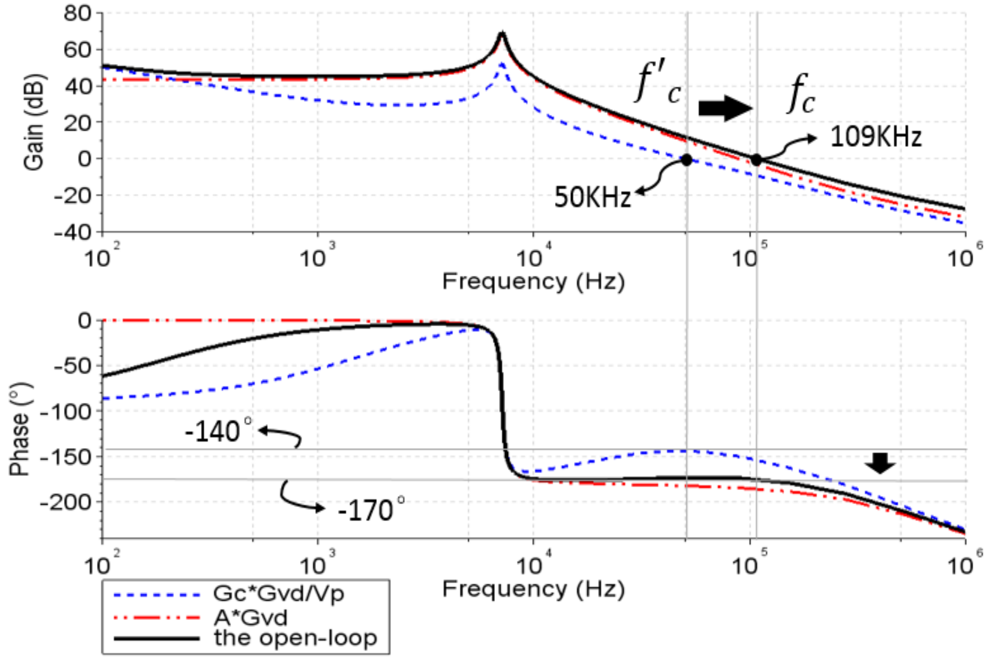
System Block Diagram



$$A = \frac{V_E G_k}{T_s V_{in}(a - bV_{ref})}$$

$$V_{p\_static} = T_s M_1$$

Bode Plot



Compared to conventional VMC --- $(G_c G_{vd}/V_p)$

- Bandwidth is increased
  50kHz → 109kHz
- Phase margin is decreased
  40° → 10 °

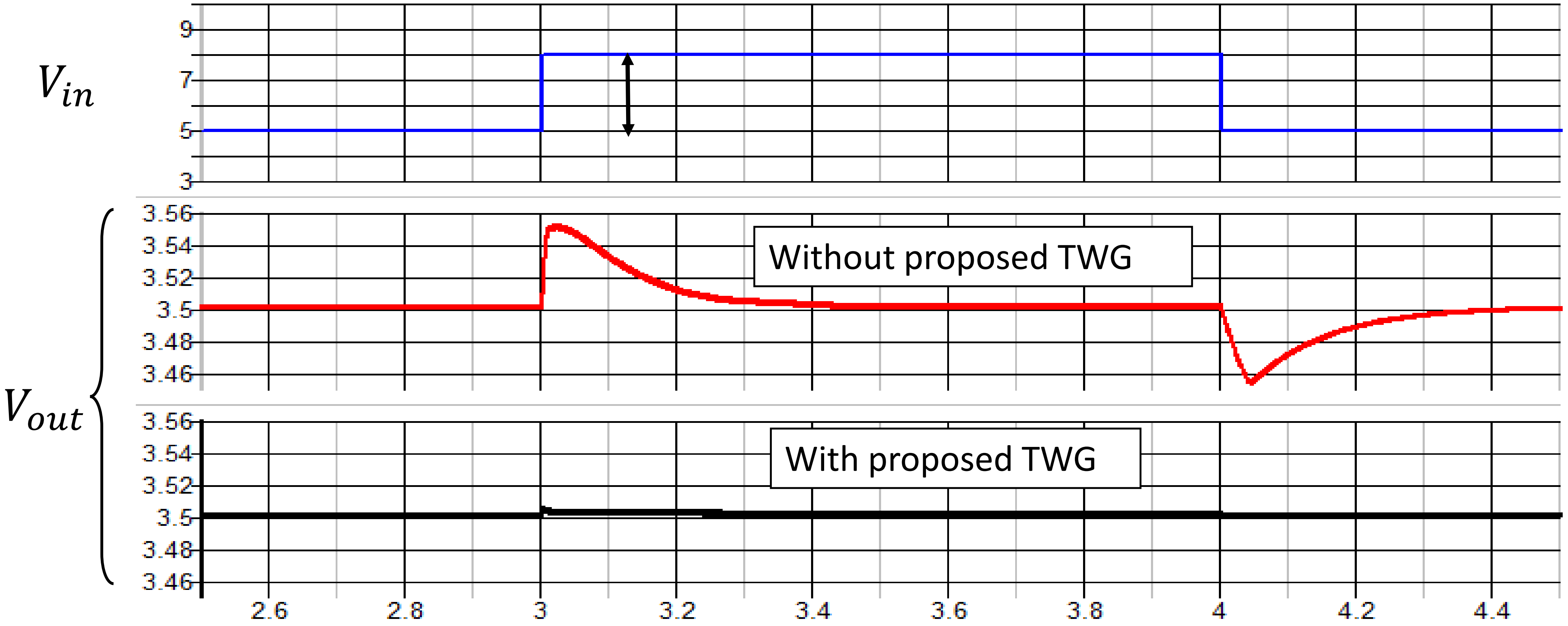
Adding a high frequency zero point

Phase margin is increased

Line Transient Response (1)

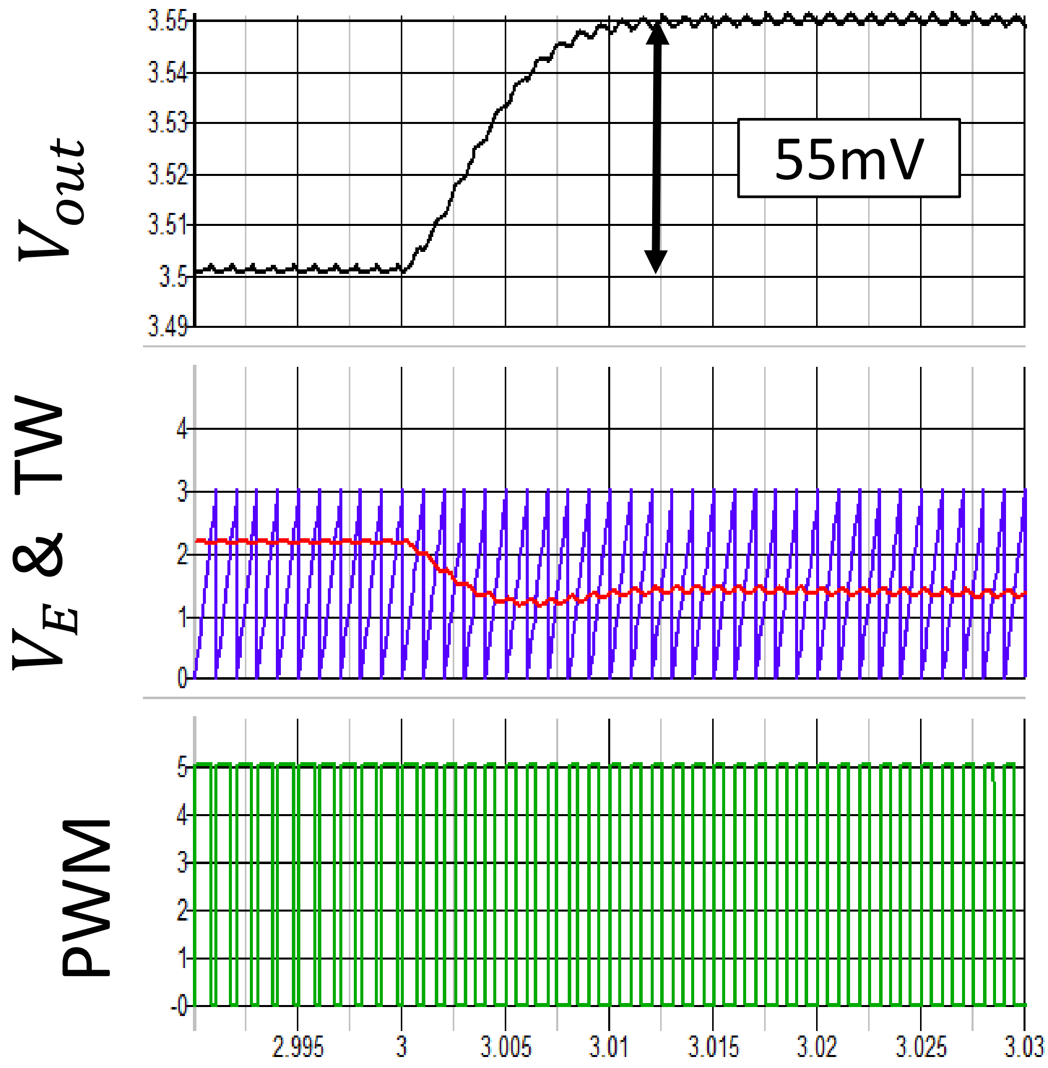
Simulation Tools: SIMetrix 6.2

V_{in}: 5V $\leftrightarrow$ 8V

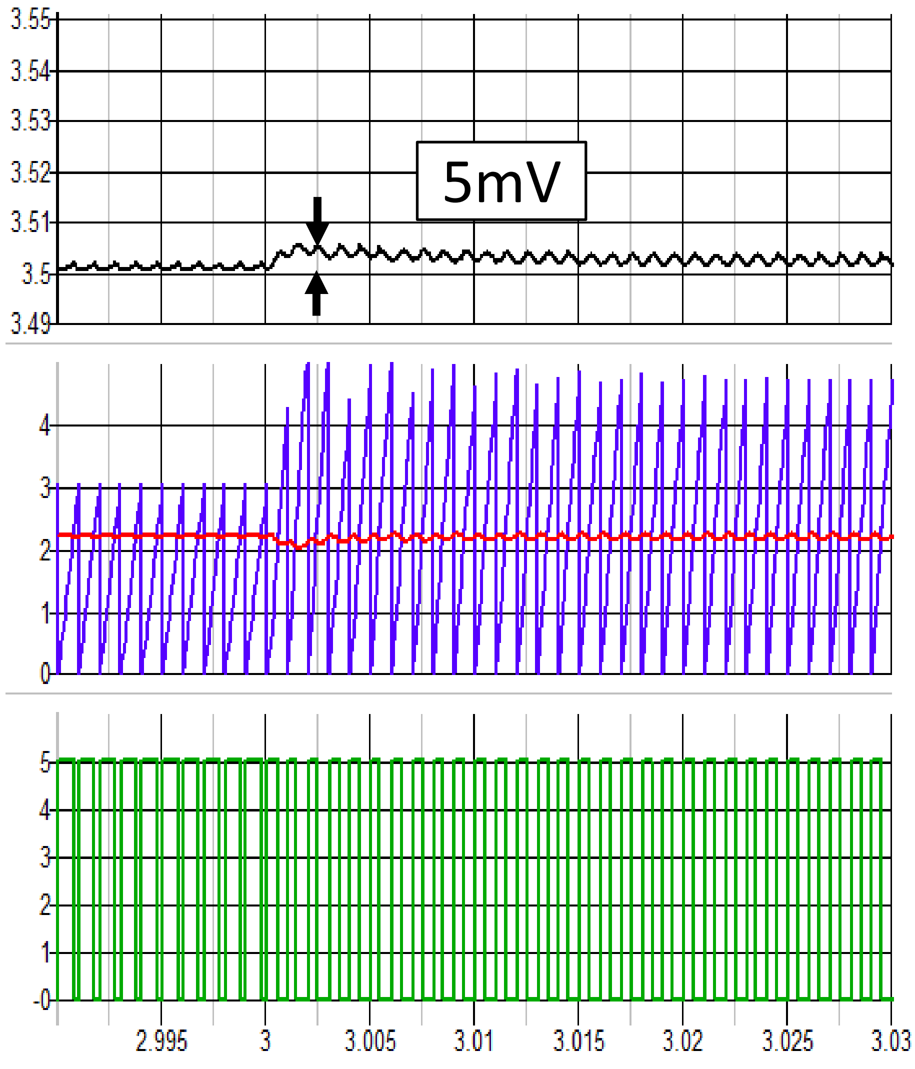


(Simulation conditions are shown in P19)

Line Transient Response (2)



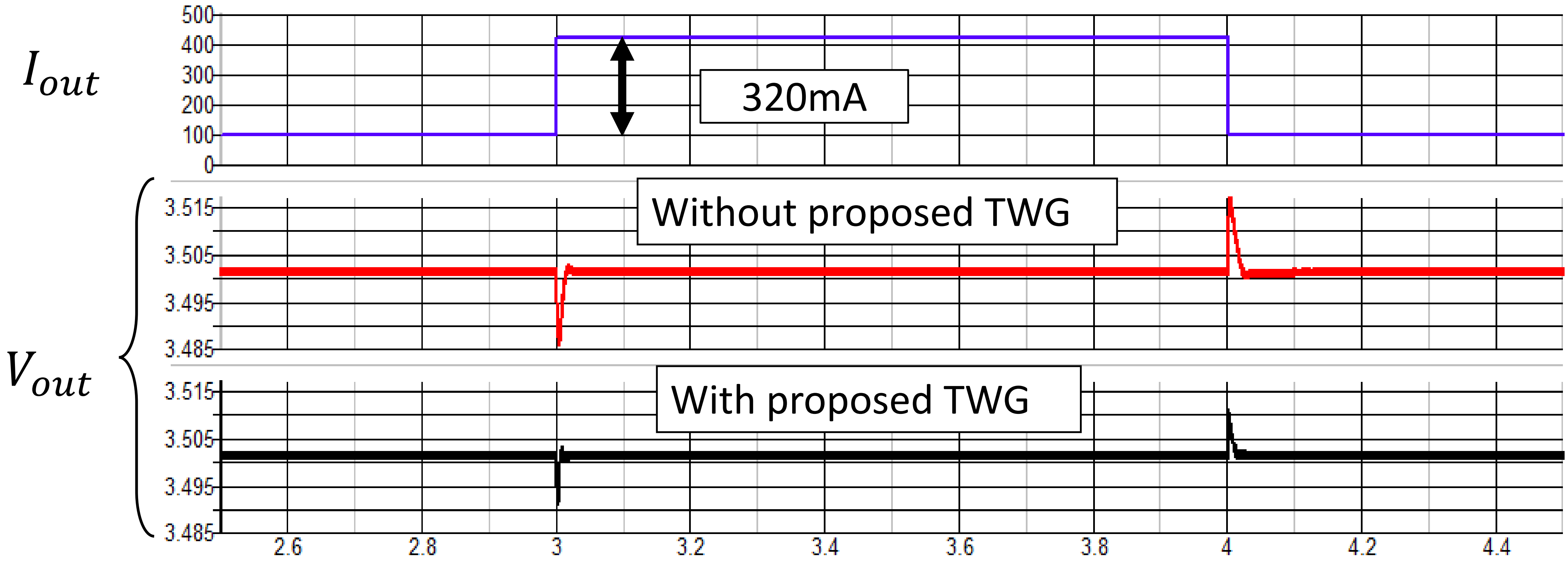
Without proposed TWG



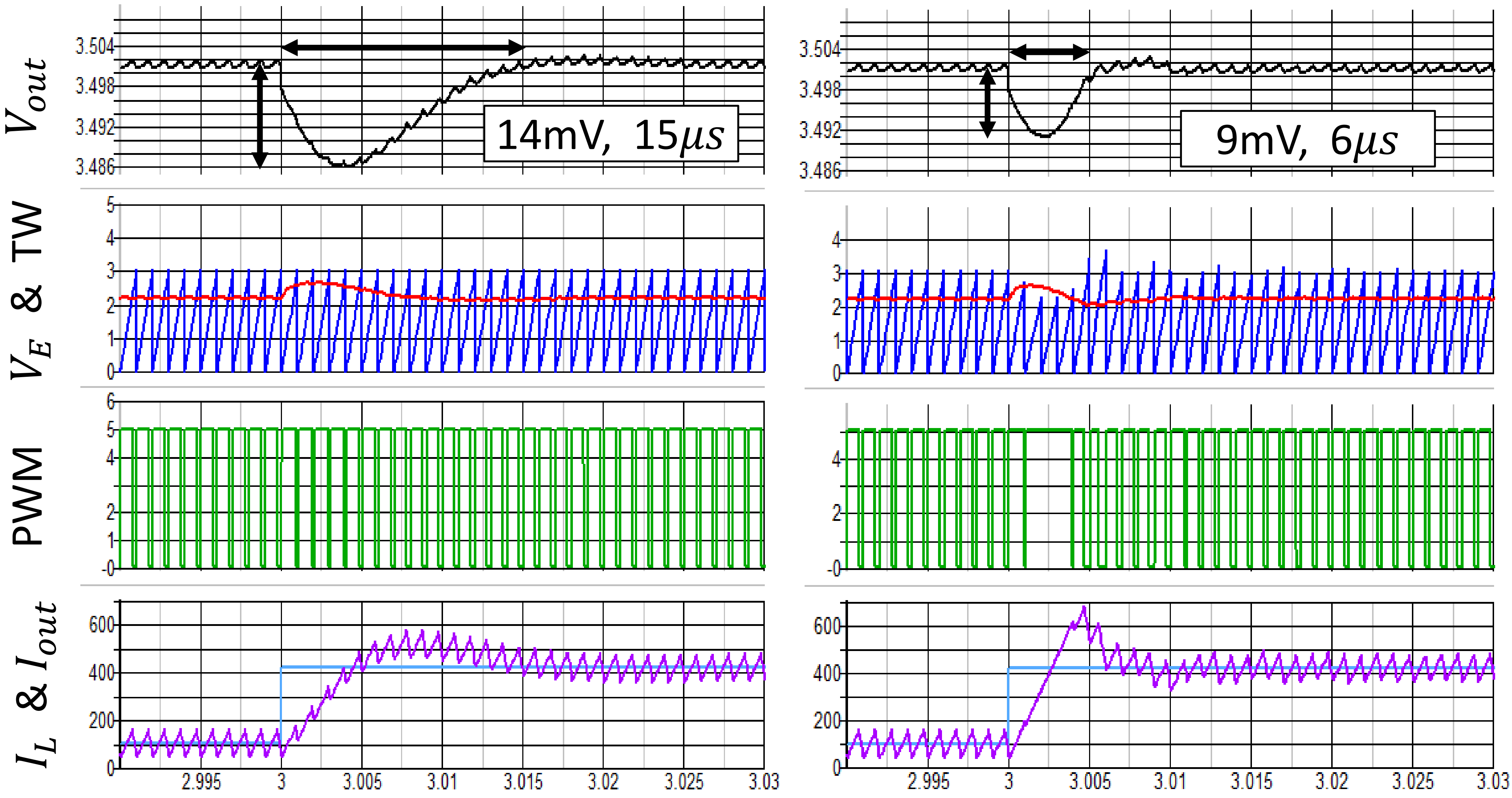
With proposed TWG

Load Transient Response (1)

I_{out}: 100mA ↔ 420mA

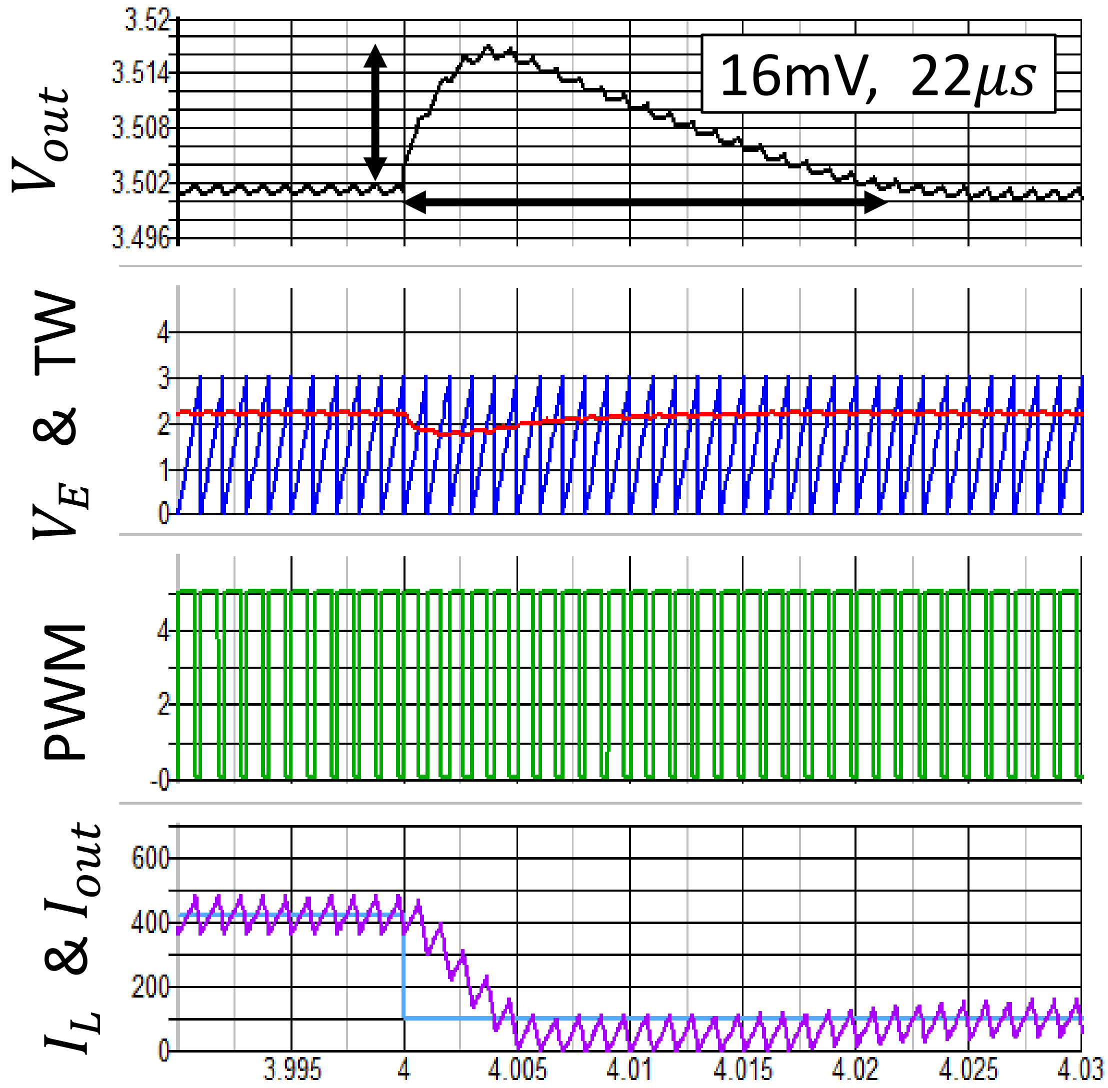


Load Transient Response (2) --- step up

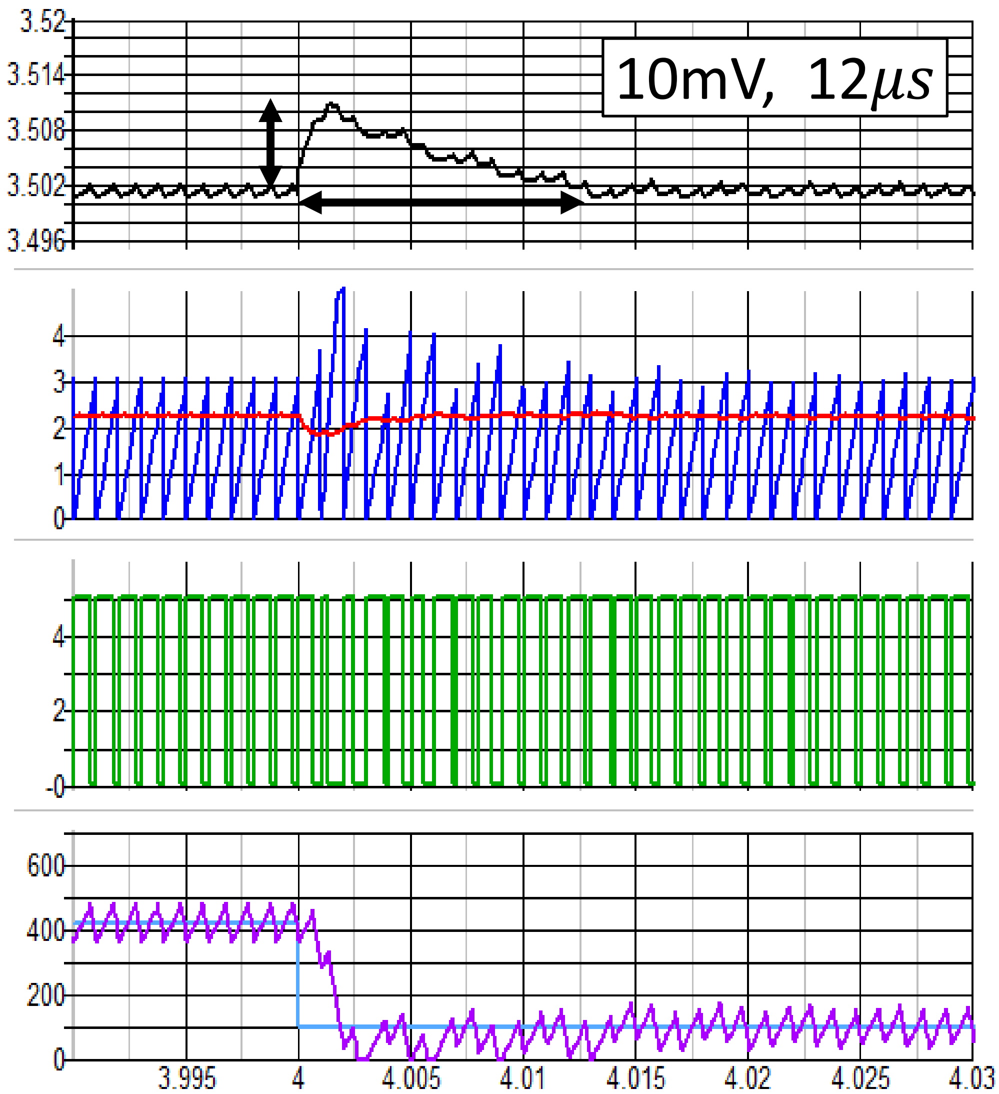


Without proposed TWG **With** proposed TWG

Load Transient Response (3) --- step down



Without proposed TWG



With proposed TWG

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Conclusion

- Design a slope adjustable triangular wave generator for DC-DC buck converter.
  - Line and load transient response improvement
  - Simple

    \- Not require current sensor or slope compensation

- Next Step

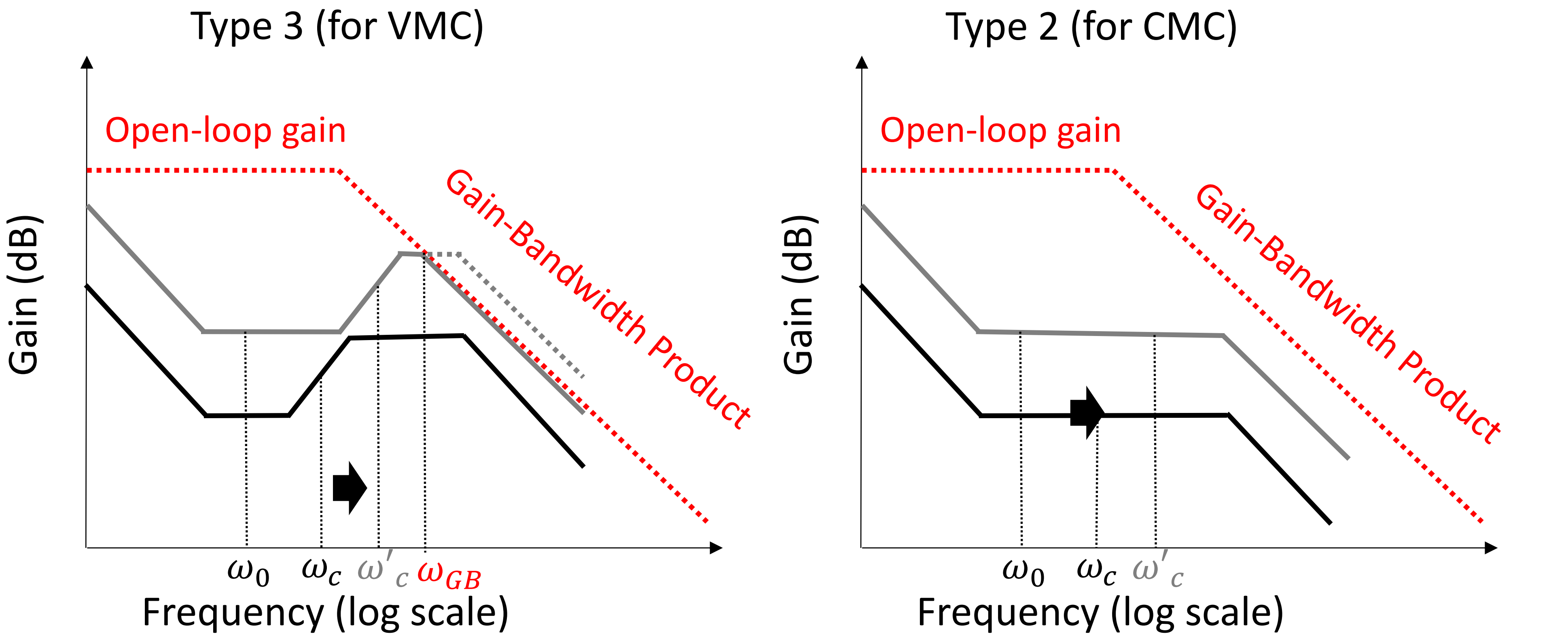
  Circuit implementation

The End

Thanks for your attention

Appendix (1)

Phase compensation & GBP limitation of op-amp



Appendix (2)

Non-linear control features

$$\Delta d = \left(\frac{V_E}{T_s} + \frac{G_c \Delta v}{T_s}\right)\left(\frac{\left(V_{ref} + G_k \Delta v\right)}{V_{in}\left(a - b\left(V_{ref} + G_k \Delta v\right)\right)} - \frac{V_{ref}}{V_{in}\left(a - bV_{ref}\right)}\right) + \frac{G_c \Delta v}{V_{p\_static}}$$

$$\Delta d = A\Delta v + \frac{G_c \Delta v}{V_{p\_static}} \qquad A = \frac{aG_k(V_E + G_c \Delta v)}{T_s V_{in}\left(a - bV_{ref}\right)\left(a - bV_{ref} - bG_k \Delta v\right)}$$

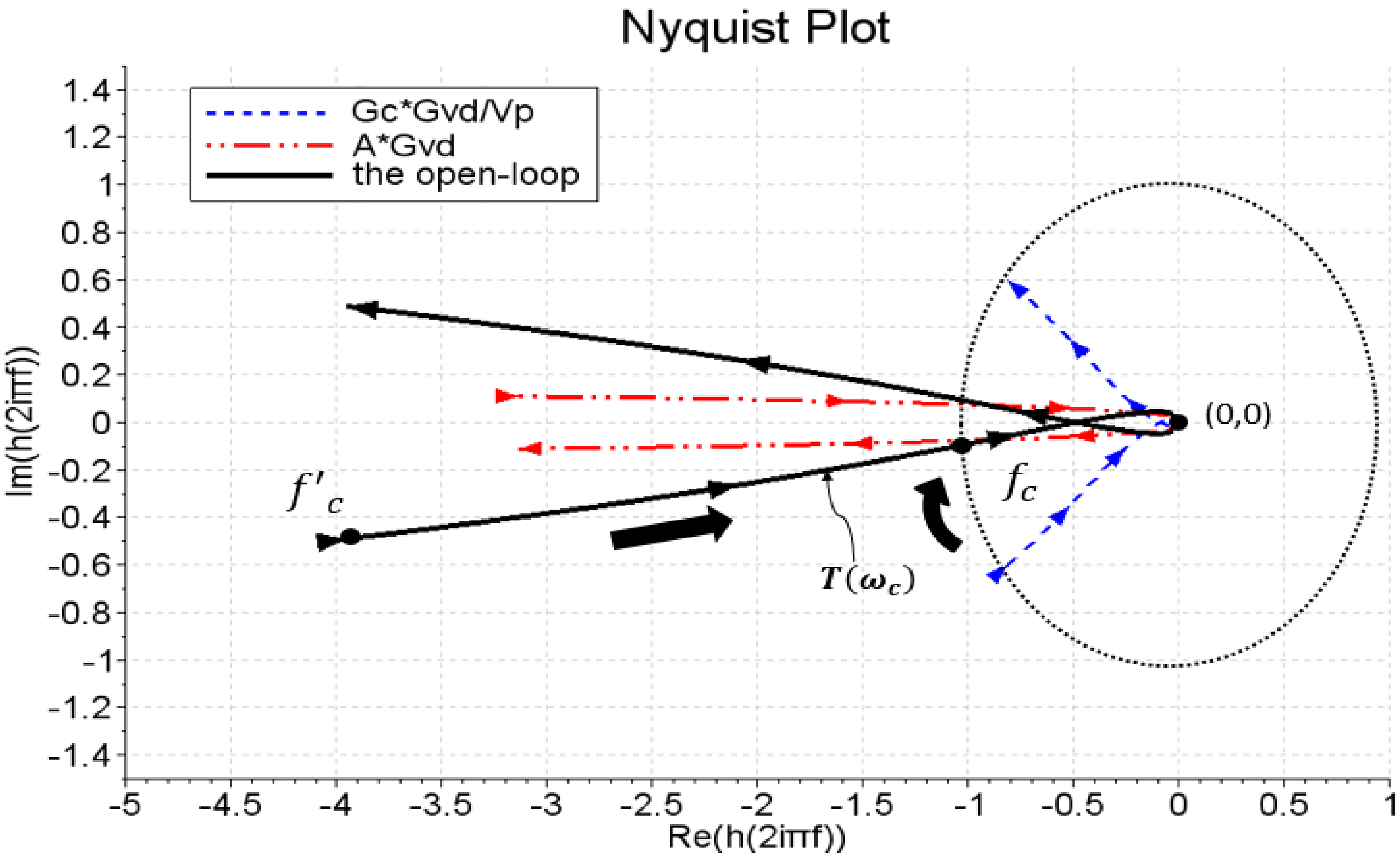
Large → Large → Enable fast transient response

Δv ⇒ A Non-linearly decrease

approach to 0 → approach to a constant → To ensure the loop stability

Appendix (3)

The Nyquist Plot



Q&A

- In page 9, the voltage controlled current source, why use Q1?

- A: Q1 is used to amplify the output current of op-amp 4. Limited supply voltage VDD causes a limited maximum current iCS, and if the iCS is big, transistor Q1 must be able to handle the maximum current.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