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Kobayashi
Laboratory

High-Frequency Low-Distortion Signal Generation Algorithm with AWG

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Objective

**Low-distortion sine wave generation
for ADC test**

Our Approach

DSP algorithm using AWG

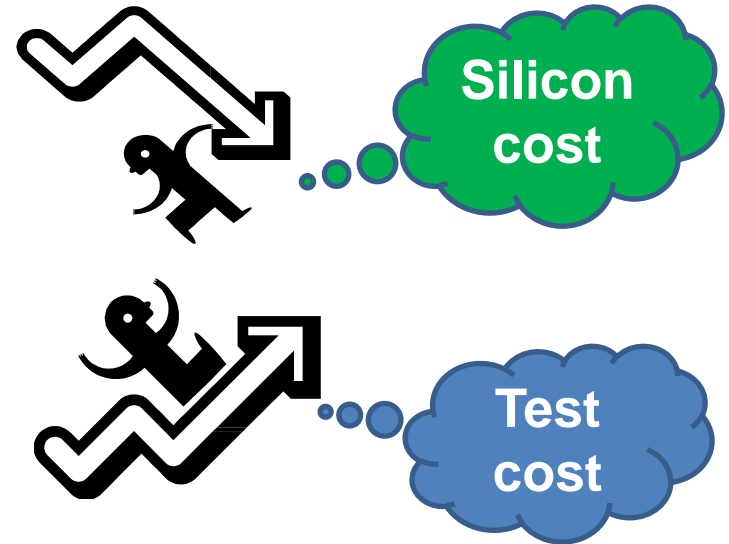
AWG : Arbitrary Waveform Generator

- **Research background**
- **Phase-switching algorithm**
- **Proposed solution**
- **Theoretical analysis**
- **Conclusion**

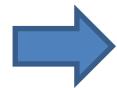
- **Research background**
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- Conclusion

Semiconductor industry

- **Silicon cost** ⇒ decreasing
- **Test cost** ⇒ increasing

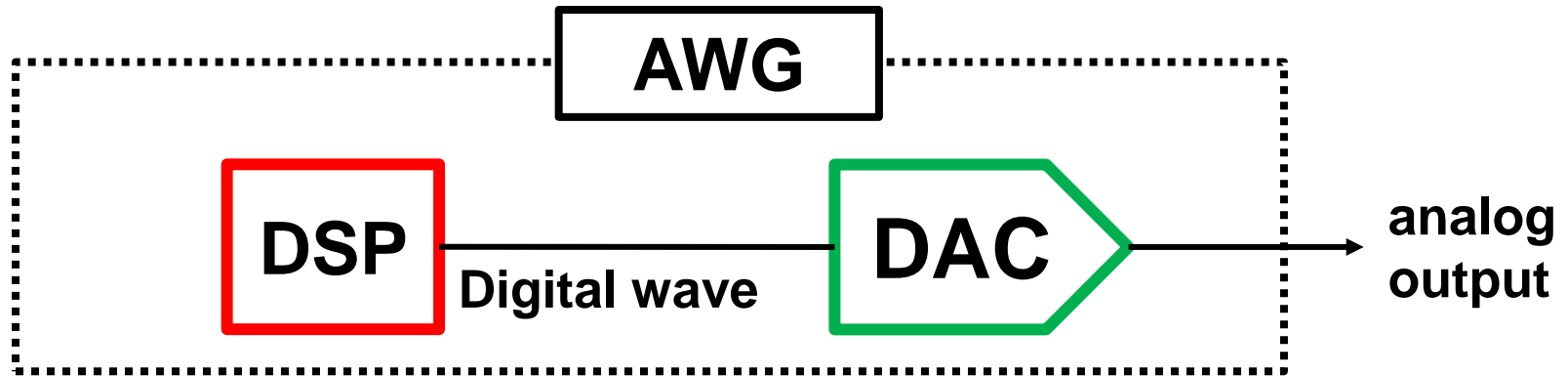


Low cost test

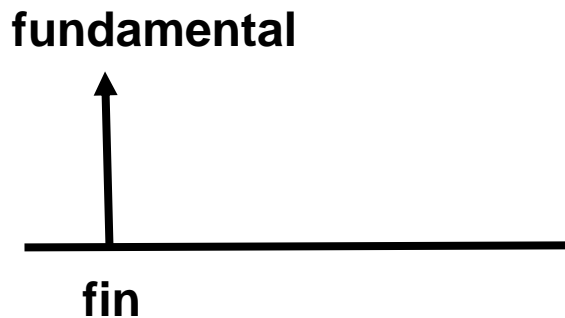


Low cost LSI production

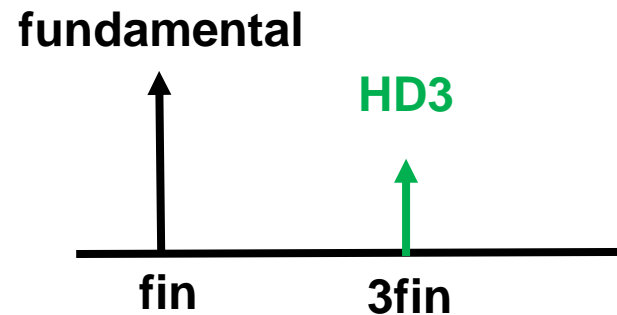
AWG : Arbitrary Waveform Generator



Ideal AWG output spectrum



Real AWG output spectrum (DAC has 3rd nonlinearity)



DAC nonlinearity



Harmonic distortion of AWG

AWG

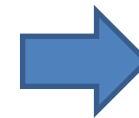


- AWG : **Expensive**
- **Long testing time**

Mass production



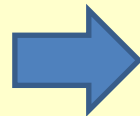
Test cost



high



Low cost test



Low cost AWG

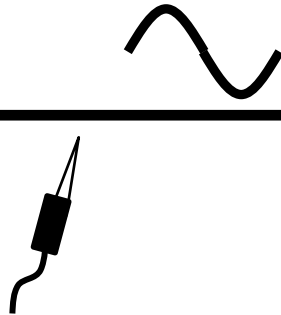


Test performance



Test signal

AWG



$$Z = b_1 Y + b_3 Y^3$$

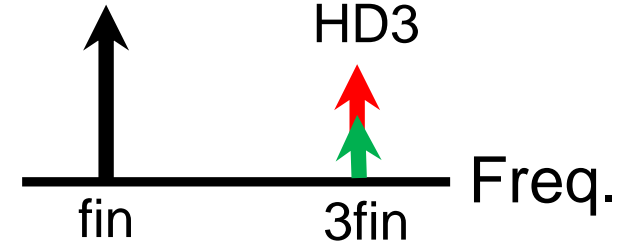
ADC

$$Y = a_1 D_{in} + a_3 D_{in}^3$$

AWG: Arbitrary Waveform Generator

ADC output spectrum

conventional



AWG HD3+ADC HD3

Inexpensive AWG output includes HD3

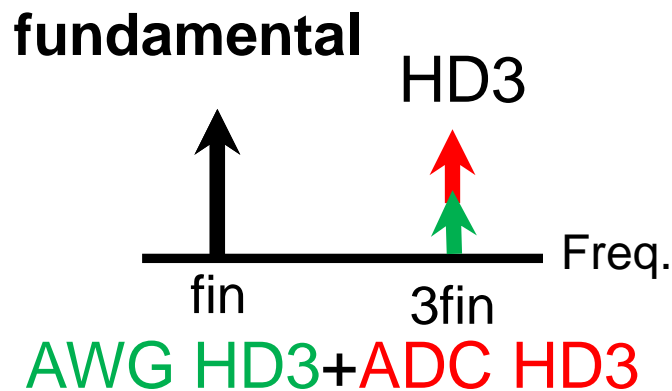
HD3 : 3rd order Harmonic Distortion

Conventional ADC nonlinearity test

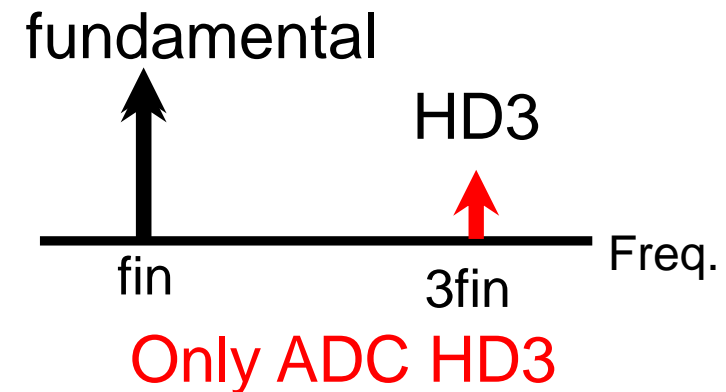


Over estimate of HD3

Conventional method



Proposed method



Accurate ADC linearity test with inexpensive AWG

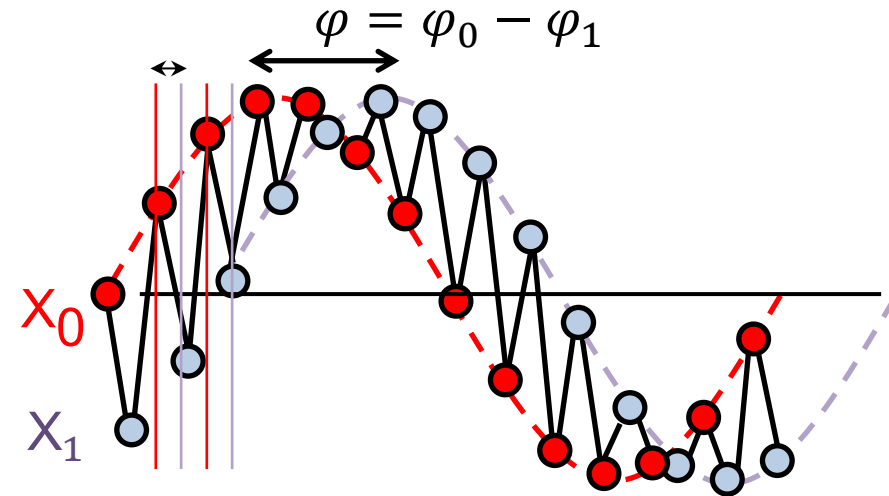
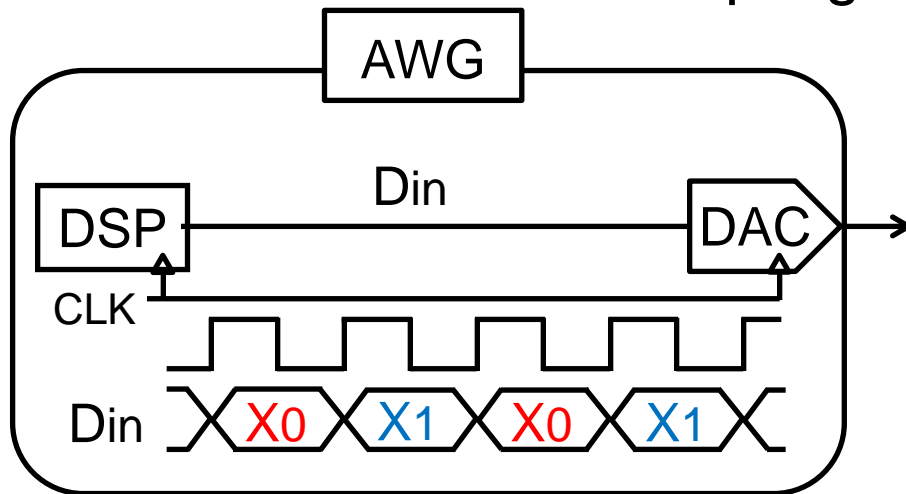
- Only DSP program change
- No hardware change
- No requirement for AWG nonlinearity identification

- Research background
- **Phase-switching algorithm**
- Proposed solution
- Theoretical Analysis
- Conclusion

Phase switching signal algorithm

Our previous proposal

Interleave sampling X_0 , X_1 every one clock



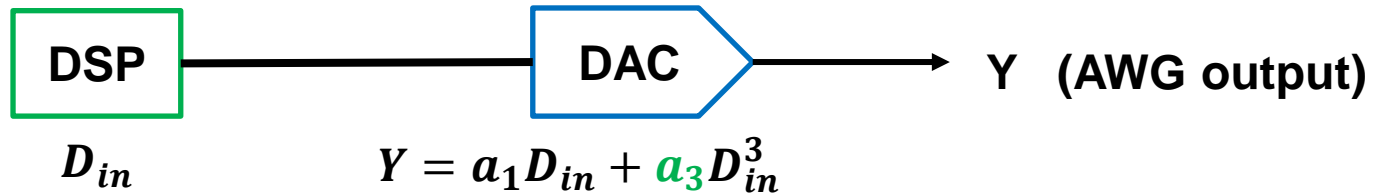
- $X_0 = A \cos(2\pi f_{in} n T_s + \varphi_0) \dots n: \text{even}$
- $X_1 = A \cos(2\pi f_{in} n T_s + \varphi_1) \dots n: \text{odd}$

$$\varphi = \varphi_0 - \varphi_1 = \pi/N$$

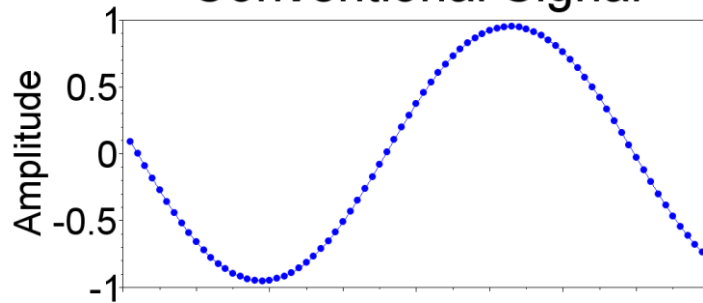


HD_N is cancelled.

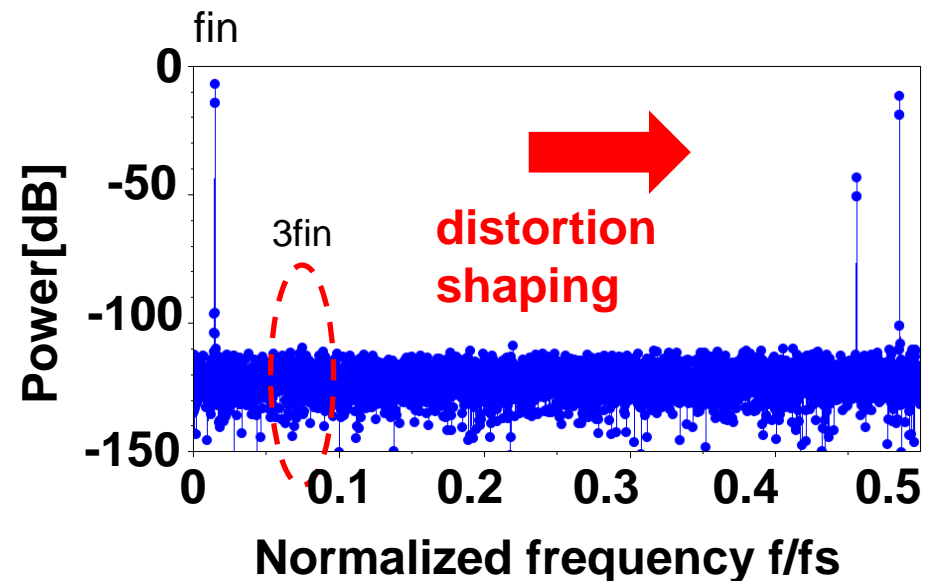
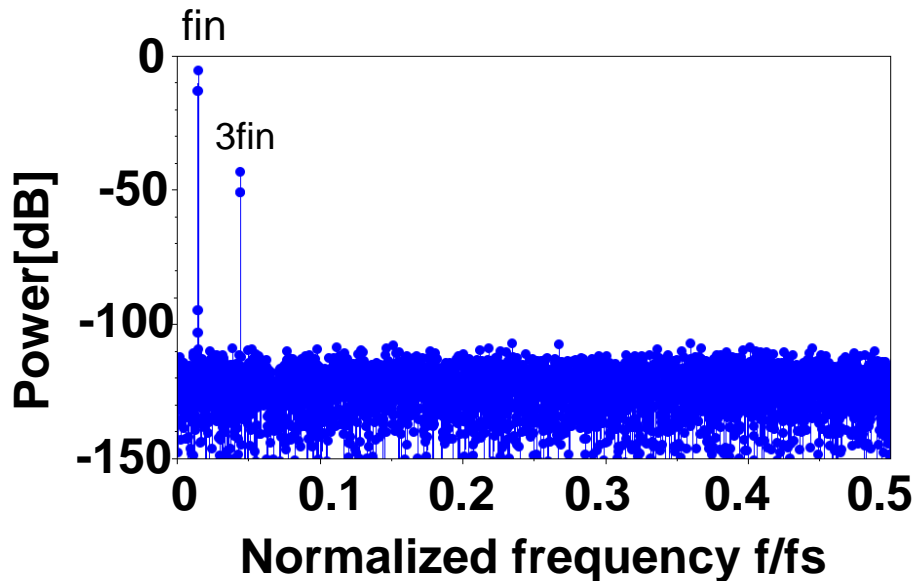
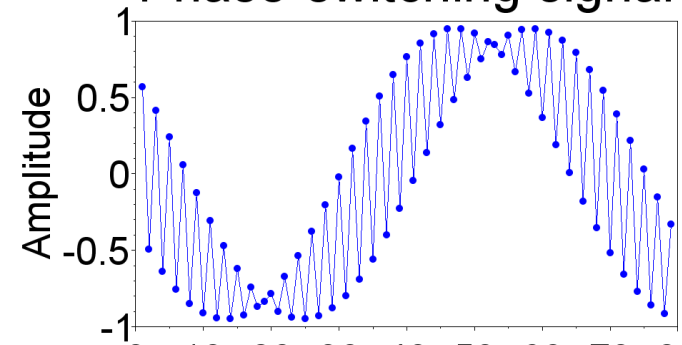
Simulation Result of Phase Switching Signal



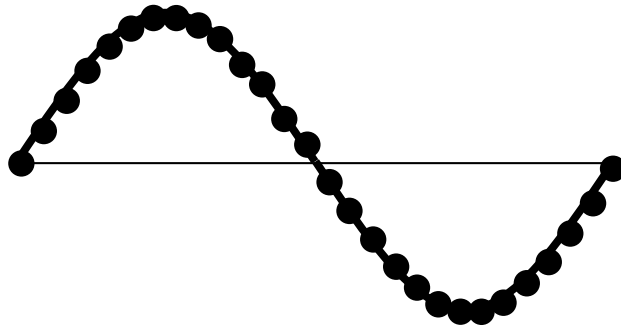
Conventional Signal



Phase-switching signal

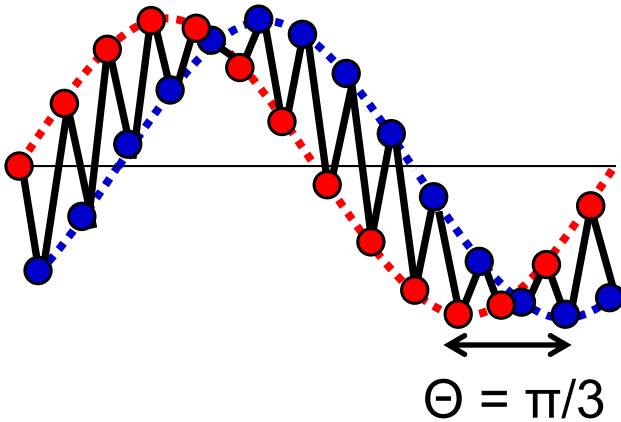


Conventional



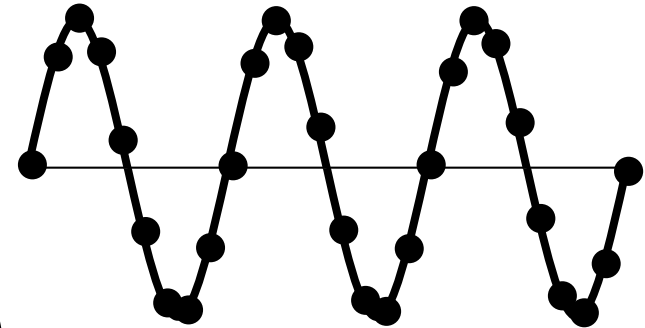
fundamental: f_{in}

Phase Switching

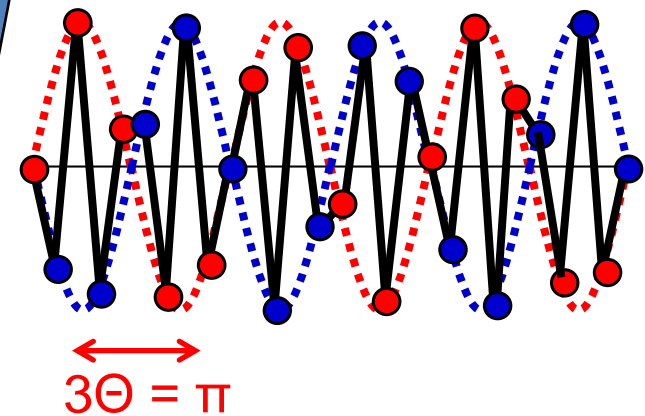


$$\Theta = \pi/3$$

3rd order non-linear system
Phase rotation by x3



3rd harmonics: $3 f_{in}$

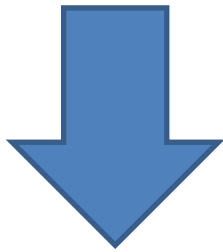


$$3\Theta = \pi$$

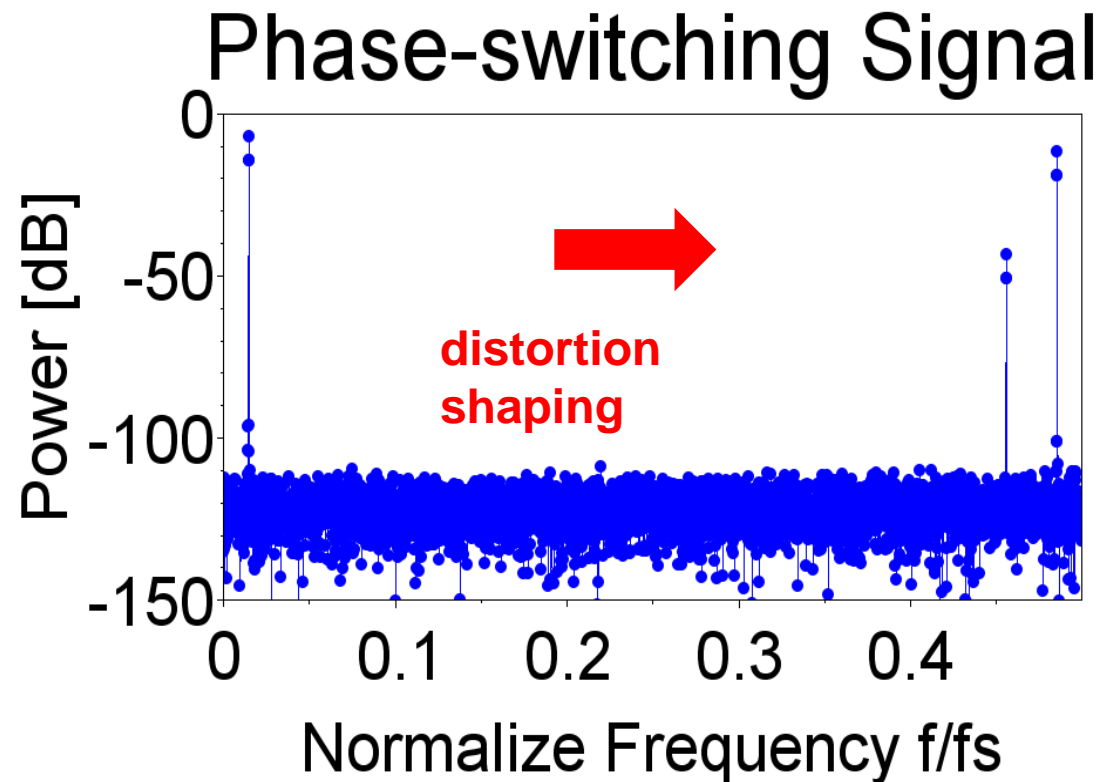
Two waves with phase difference π
are cancelled

- Research background
- Phase-switching algorithm
- **Proposed solution**
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“Distortion shaping” cancels HD3,
but spurious around $f_s/2$ appears.



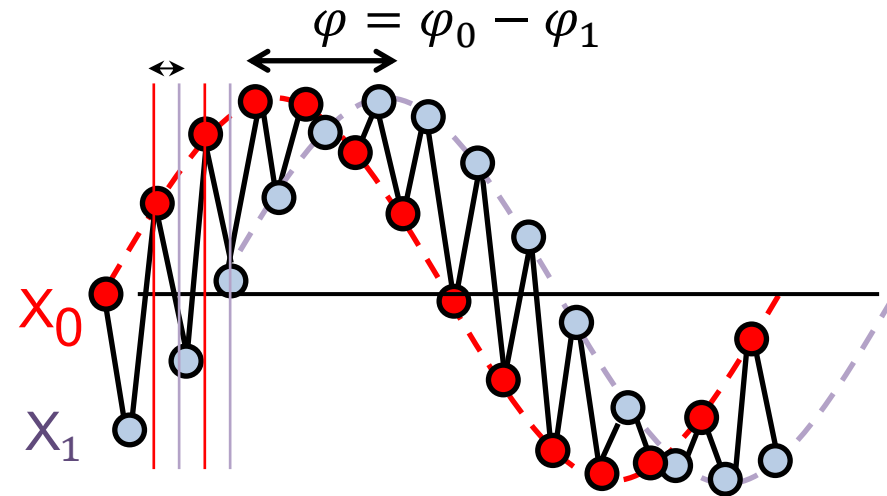
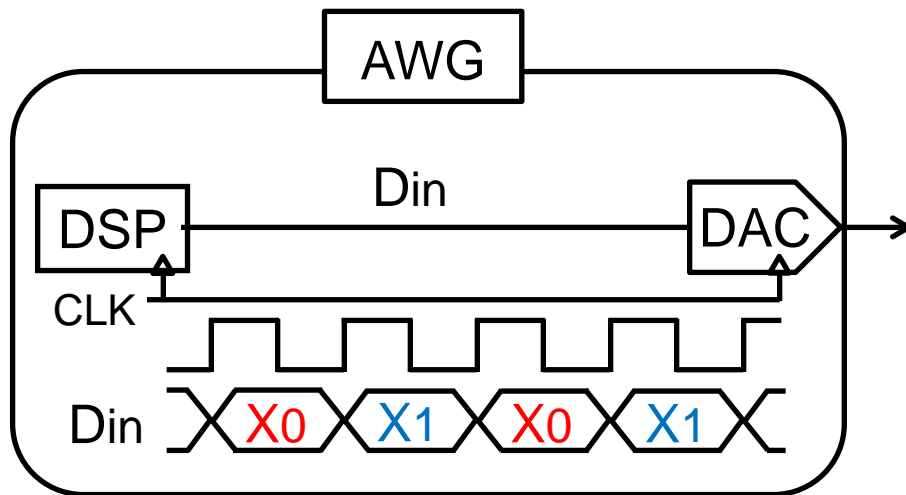
Phase switching signal
is applicable
only for low frequency
signal generation.



We propose phase switching method for high frequency

High frequency low distortion signal generation

Interleave sampling X_0 , X_1 every one clock



- $X_0 = A \cos(2\pi f_{in} n T_s + \varphi_0) \dots n: \text{even}$
- $X_1 = A \cos(2\pi f_{in} n T_s + \varphi_1) \dots n: \text{odd}$

$$\varphi = \varphi_0 - \varphi_1 = 2\pi/N \quad \rightarrow$$

N-th order image is cancelled



**Two sinusoidal
signals
(frequency : f_{in})**

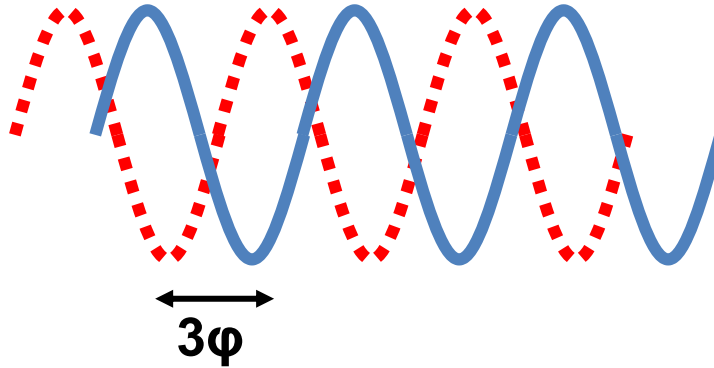
**Two 3rd order
harmonics
(frequency : $3f_{in}$)**

**Interleave sampling every one clock
(Sampling frequency : f_s)**

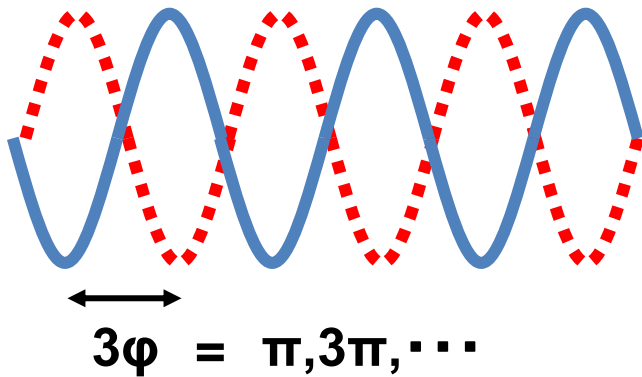
**Image signal
: $f_s/2 - f_{in}$**

**3rd order image
signal
: $f_s/2 - 3f_{in}$**

Two 3rd order harmonics

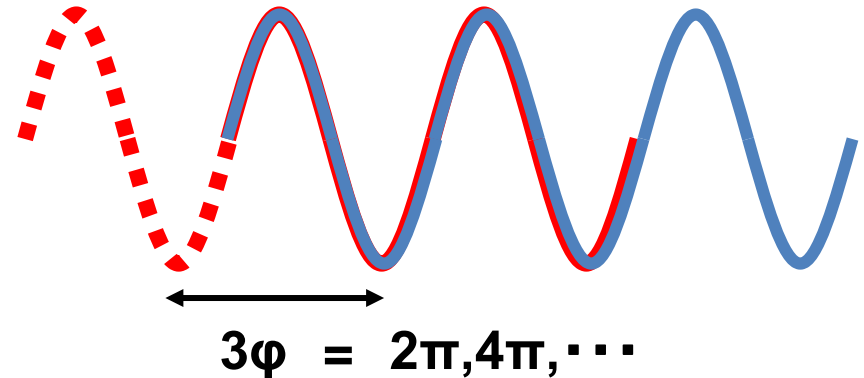


Reverse phase

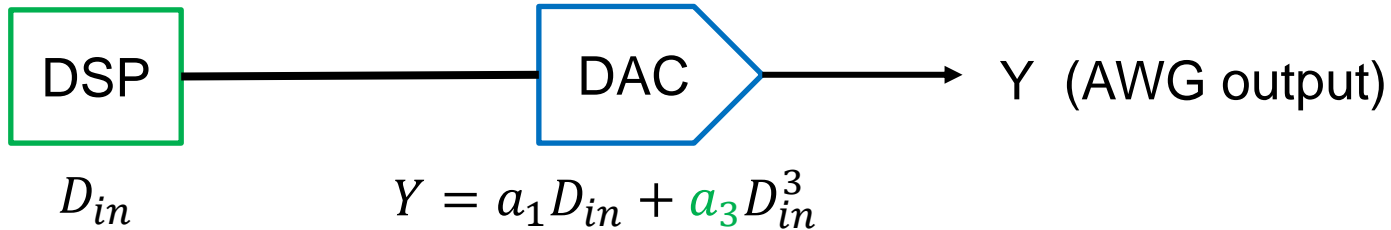


- **Cancelled HD3**

Same phase



- **Cancelled fs/2-3fin**

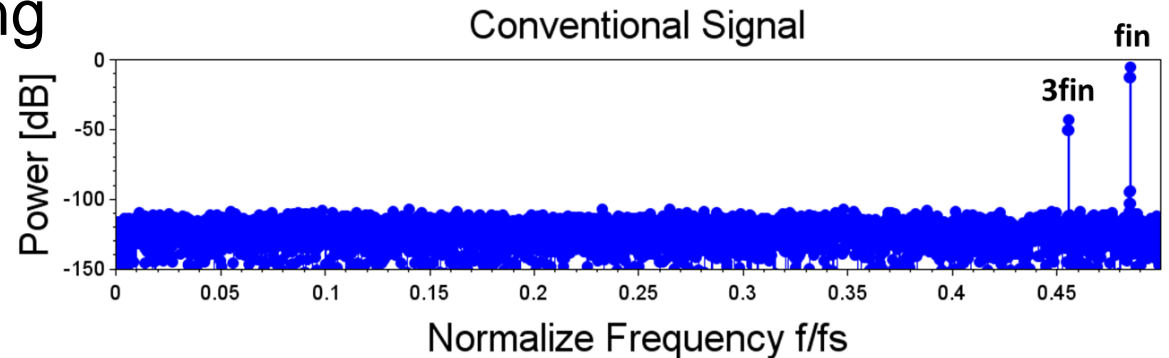
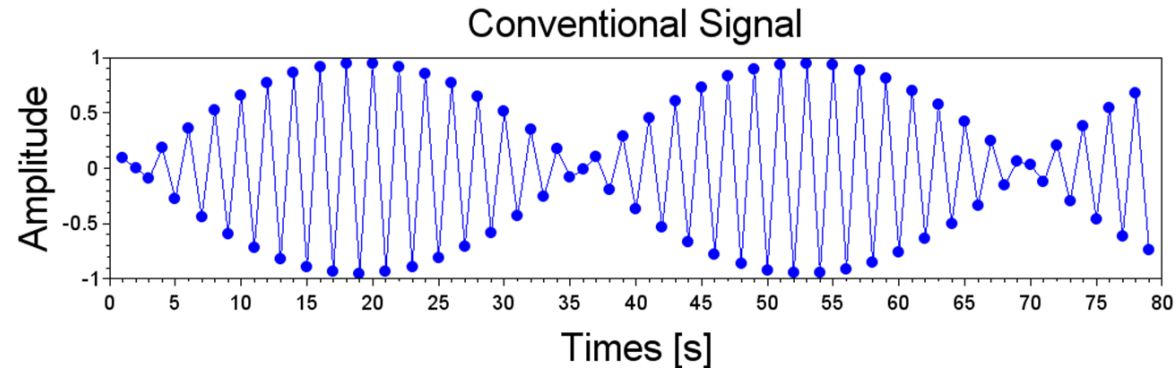


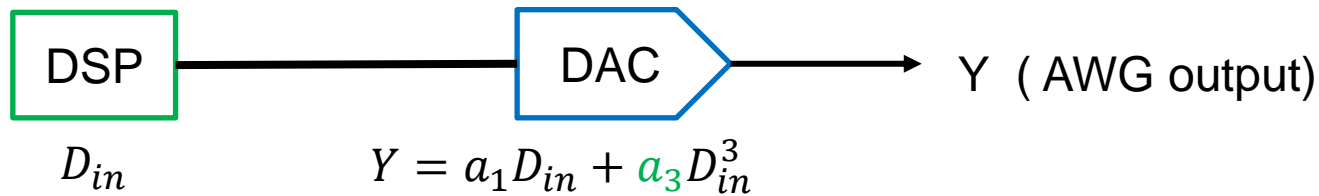
$$D_{in} = \sin(2\pi f_{in_conv} n T_s)$$

HD3 component ($3f_{in}$)



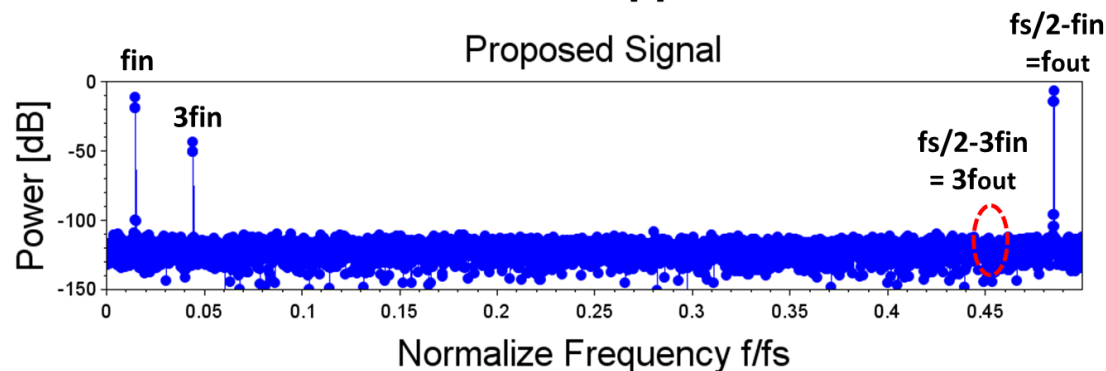
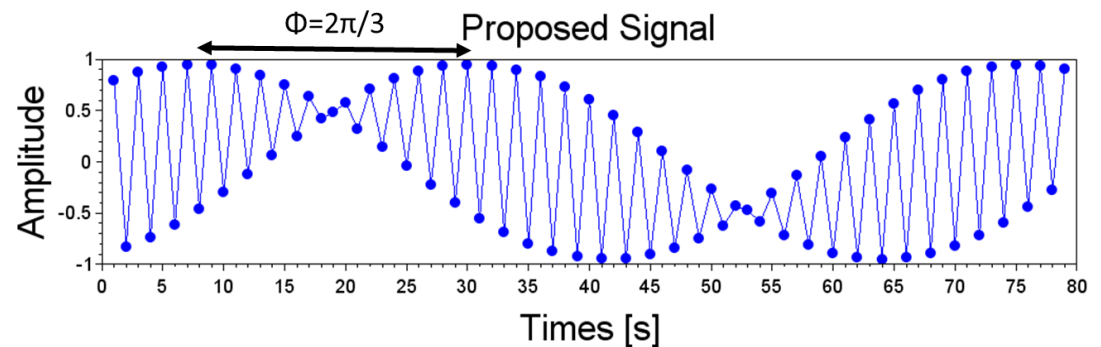
is folded back as aliasing



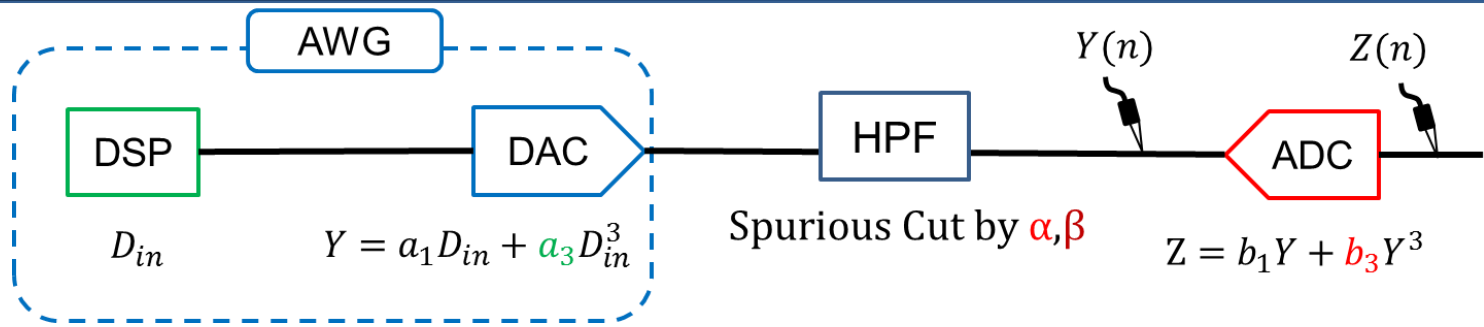


- $X_0 = A \cos(2\pi f_{in} n T_s + \pi/3) \dots n: \text{even}$
- $X_1 = A \cos(2\pi f_{in} n T_s - \pi/3) \dots n: \text{odd}$

**$3f_{out}$ component
is cancelled**



Low-Distortion High-Frequency Signal

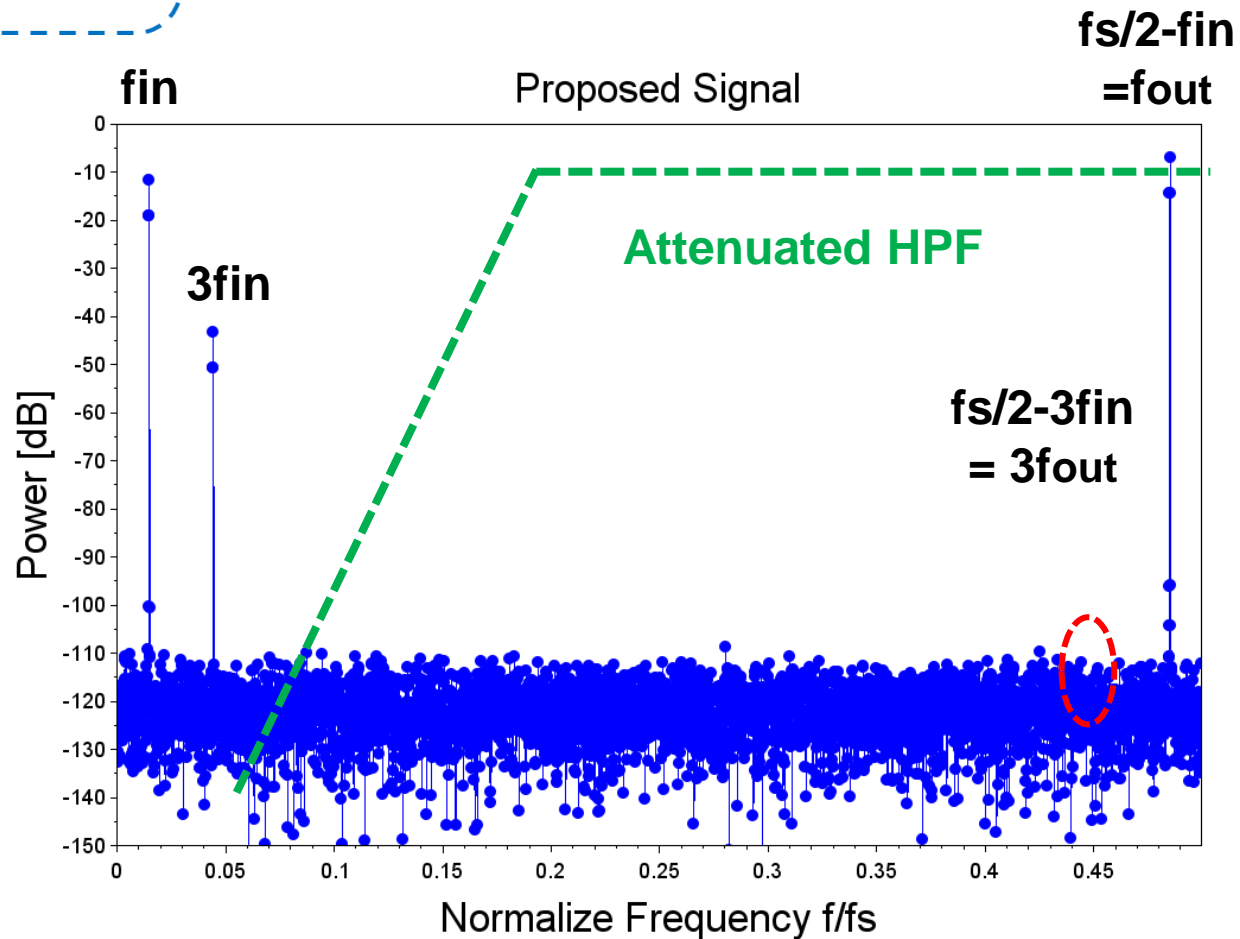


f_{in} , $3f_{in}$ components
reduction by HPF

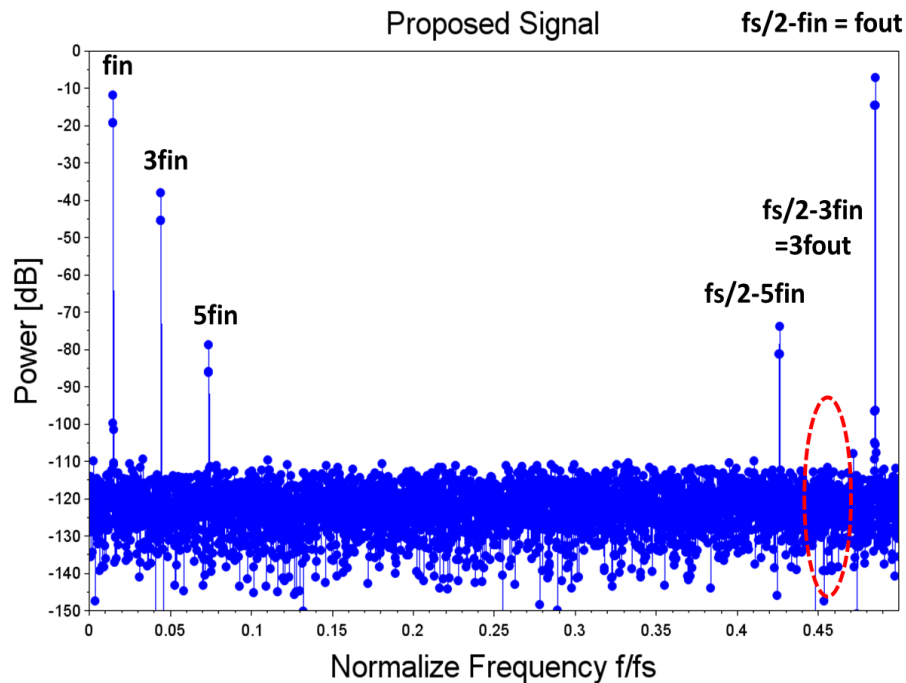


**Low distortion
sinusoidal signal**

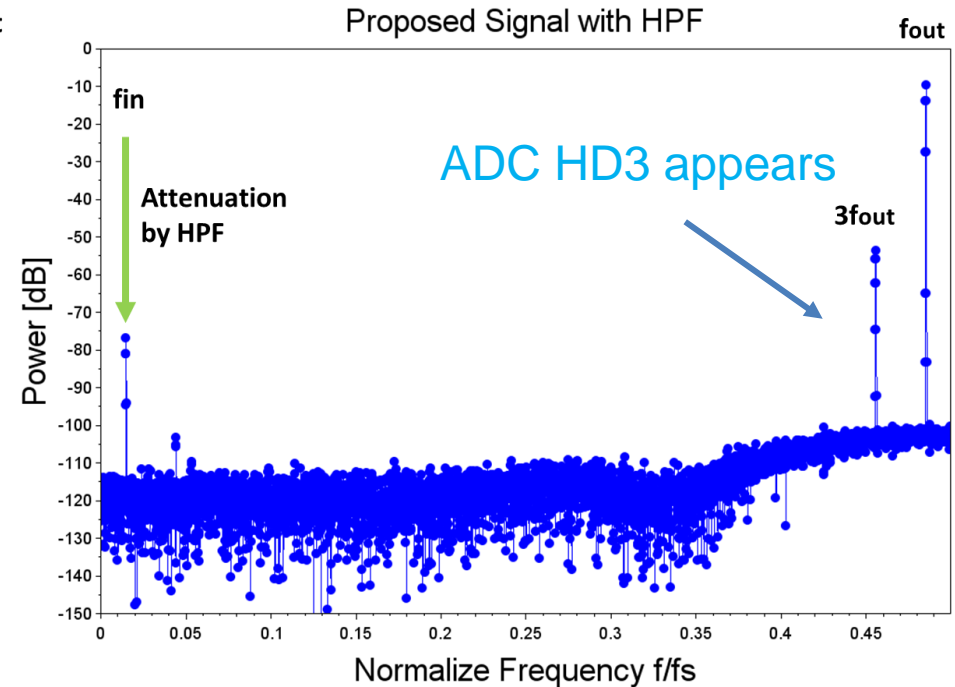
$$\left(f_{out} = \frac{f_s}{2} - f_{in} \right)$$



No attenuation of f_{in} component



Attenuation of f_{in} component with HPF



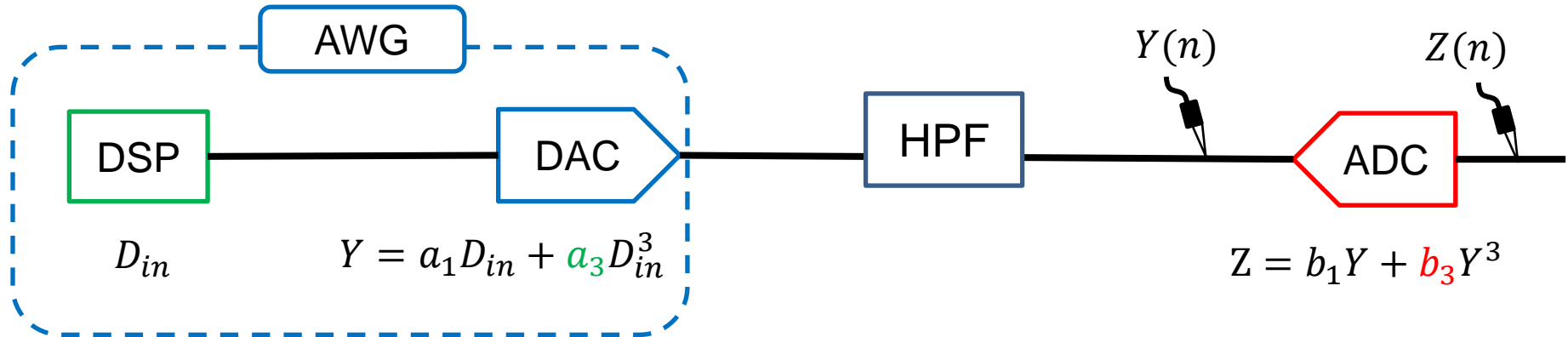
If f_{in} component is NOT reduced

➡ ADC HD3 component is cancelled
(ADC 3rd distortion cannot be measured)

If f_{in} component is reduced by HPF

➡ Accurate ADC HD3 measurement

- Research background
- Phase-switching algorithm
- Proposed solution
- **Theoretical Analysis**
- Conclusion



- AWG Input with Phase Switching

$$D_{in}(nT_s) = \begin{cases} A \cdot \sin\left(2\pi f_{in} nT_s - \frac{\pi}{3}\right) & n: \text{odd} \\ A \cdot \sin\left(2\pi f_{in} nT_s + \frac{\pi}{3}\right) & n: \text{even} \end{cases}$$

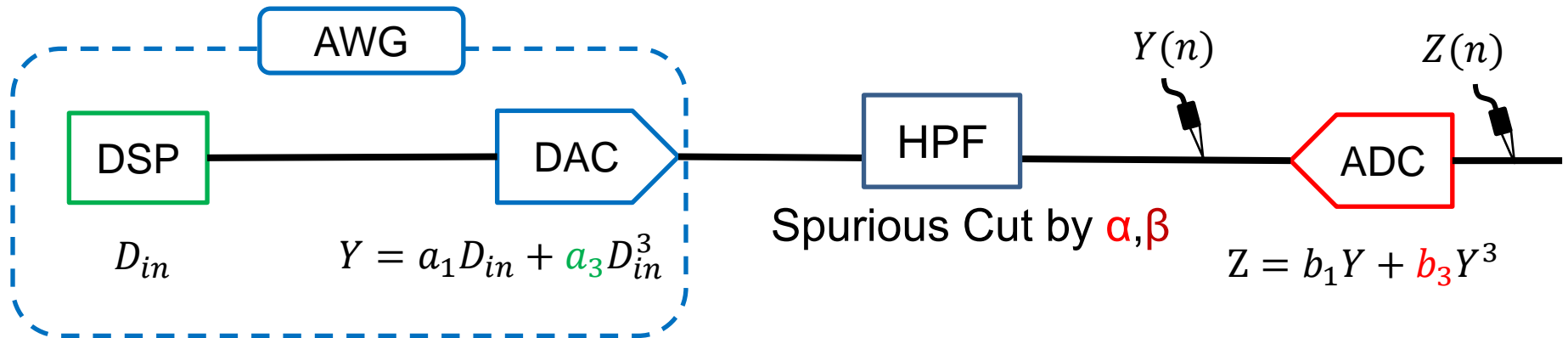
- AWG Nonlinearity Model

$$Y(nT_s) = a_1 D_{in}(n) + a_3 \{D_{in}(n)\}^3$$

- ADC Nonlinearity Model

$$Z(n) = b_1 Y(nT_s) + b_3 \{Y(nT_s)\}^3$$

For Simplicity
 $f_{s(\text{AWG})} = f_{s(\text{ADC})}$



$$\begin{aligned}
 Y = a_1 D_{in} + a_3 D_{in}^3 &= -\alpha \frac{1}{2} \left(a_1 A + \frac{3}{4} a_3 A^3 \right) \sin(2\pi f_{in} n T_s) \\
 &\quad -\beta \frac{1}{4} a_3 A^3 \sin(2\pi (3f_{in}) n T_s) \\
 &\quad + \frac{\sqrt{3}}{2} \left(a_1 A + \frac{3}{4} a_3 A^3 \right) \cos \left(2\pi \left(\frac{f_s}{2} - f_{in} \right) n T_s \right)
 \end{aligned}$$

filter
 $0 \leq \alpha, \beta \leq 1$

Proposed method uses this component

f_{in} : input frequency

f_s : sampling frequency

ADC output

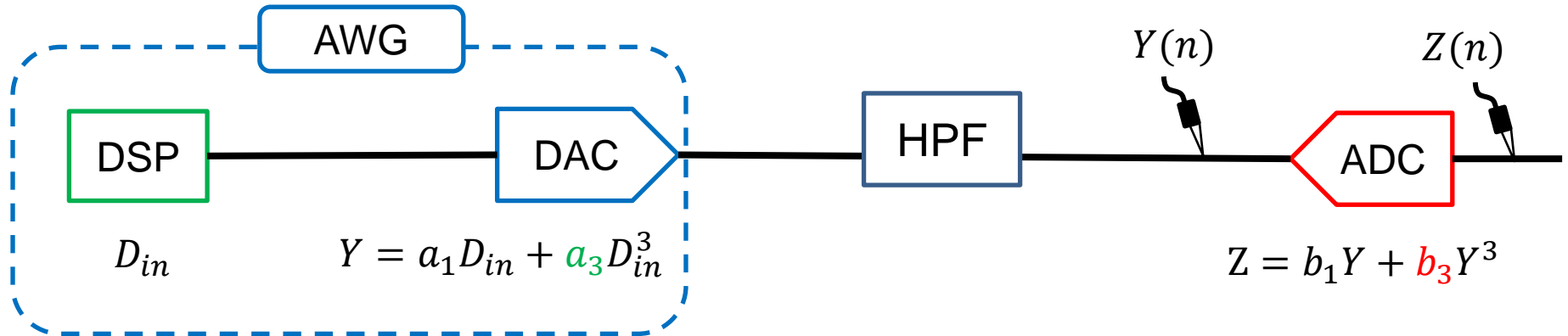
$$\begin{aligned}
 Z(nT_s) &= b_1 Y + b_3 Y^3 \\
 &= \left\{ b_1 R + \frac{3}{4} b_3 R (R^2 + 2\alpha\beta PQ + 2\beta^2 Q) \right\} \cos\left(2\pi \left(\frac{f_s}{2} - f_{in}\right) nT_s\right) \\
 &\quad + \left\{ \frac{1}{4} b_3 R (R^2 - 3\alpha^2 P^2) \right\} \cos\left\{2\pi \left(\frac{f_s}{2} - 3f_{in}\right) nT_s\right\}
 \end{aligned}$$

+ ...



$$\left\{ \frac{1}{4} b_3 R (R^2 - 3\alpha^2 P^2) \right\} = -\frac{3\sqrt{3}}{32} b_3 A^2 \left(a_1 A + \frac{3}{4} a_3 A^3 \right) (\alpha^2 - 1)$$

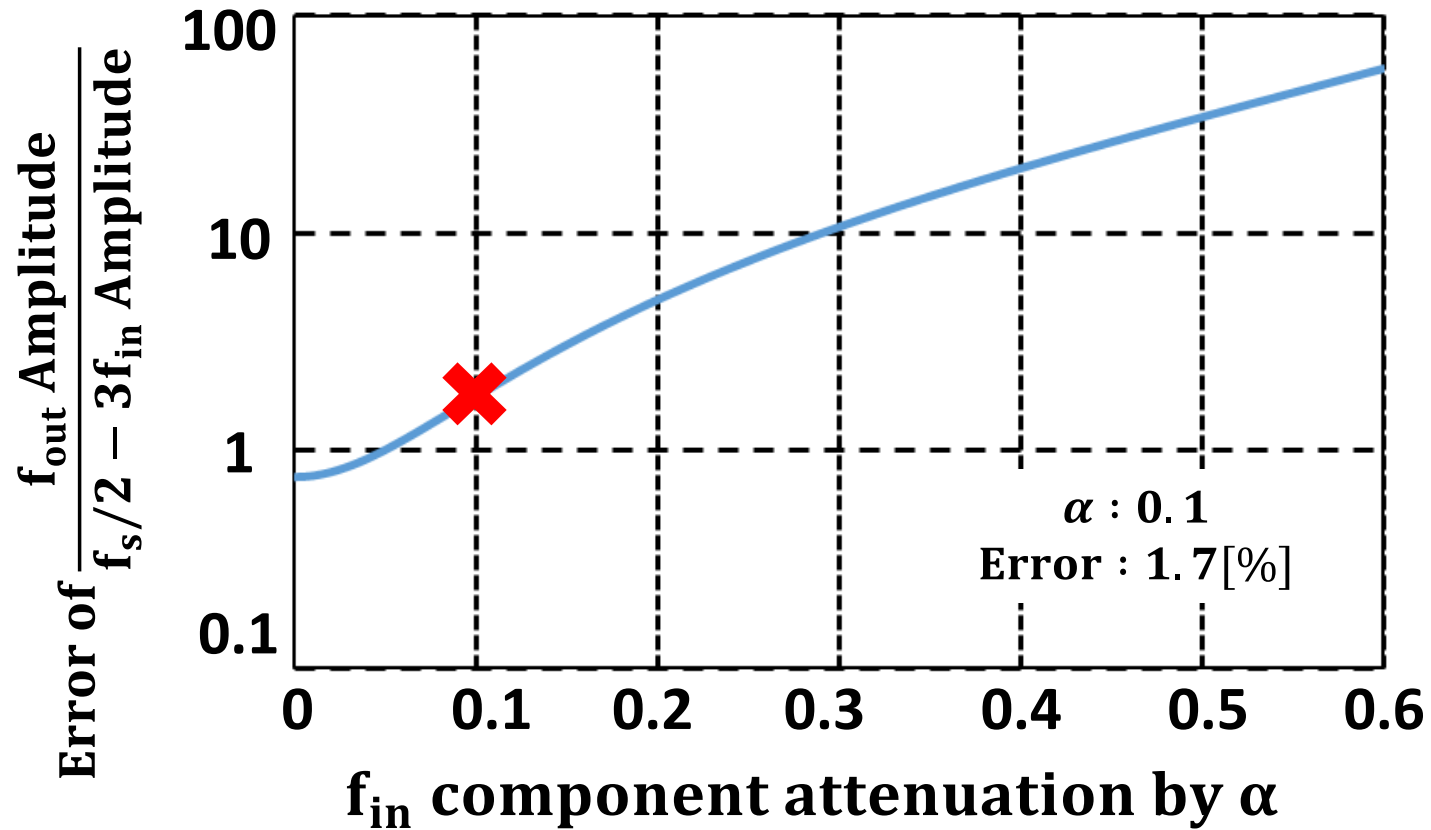
Coefficient of $\cos\left(2\pi \left(\frac{f_s}{2} - 3f_{in}\right) nT_s\right)$



Coefficient of ADC HD3

$$= -\frac{3\sqrt{3}}{32} b_3 A^2 \left(a_1 A + \frac{3}{4} a_3 A^3 \right) (\alpha^2 - 1)$$

- When filter $\alpha = 1$, \longrightarrow ADC HD3 Cancelled
- When filter $\alpha \neq 1$, \longrightarrow Accurate measurement of ADC HD3



Attenuation by a factor of 1/10
with HPF is easy

- Reserch background
- Phase-switching algorithm
- Proposed solution
- Theoretical Analysis
- **Conclusion**

- We have proposed high-frequency low-distortion signal generation algorithm with AWG.
- Needs only a simple analog HPF.
- No need for AWG nonlinearity identification
- Simulation shows that measurement error of ADC HD3 is as low as 1.7%.

Thank you for your kind attention!



**Accurate measurement
has been very important
from thousands years ago.**

度量衡 統一 by 始皇帝

