

Mar. 8 2018 (Thu)

## Automatic Notch Frequency Tracking Method with EMI Noise Reduction of Pulse Coding Controlled Switching Converter for Communication Devices

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# OUTLINE

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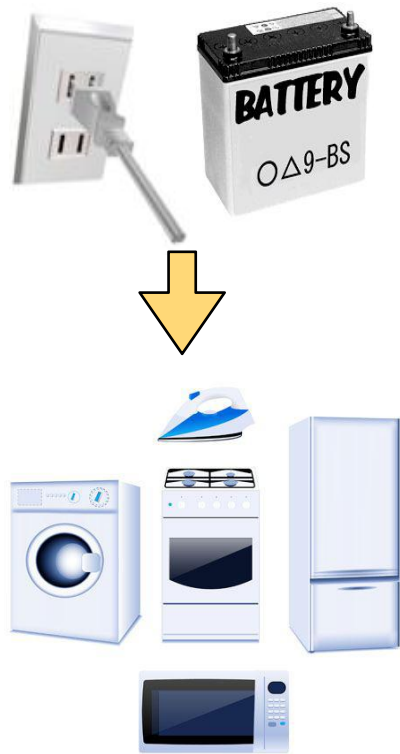
- Introduction & Objective
- Conventional Switching Converters
- Pulse Coding Method in Switching Converter
- Automatic PWC Control
  - Relationship with the Clock frequency and the Notch frequency
  - Direct generation of clock pulse from input frequency
  - Simulated Noise Spectrum of PWM Signal
- Automatic PWPC Control
- Conclusion and future work

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# Research Background



**Switching converters**  
Supply many kinds of voltage by switching power



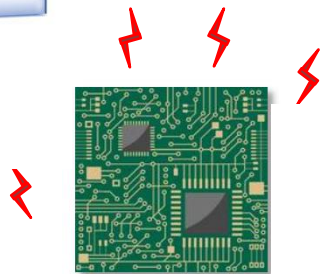
Power of switching converter  
has become large



Switching noise has strongly spread  
in wide frequency range



Important to reduce switching noise  
by decreasing main spectrum level



**EMI**

EMI:Electro-Magnetic Interference

# Research Objective

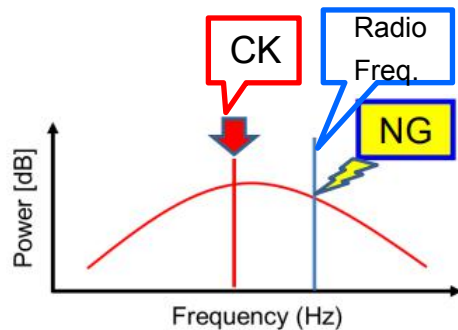
Reduce clock noise by spread spectrum  
with shaking clock phase



Trouble



Noise of clock frequency is spread



Some electronic would not like to be  
affected at special frequency noise



Research Objective



Radio receiver

Spread spectrum with both **EMI<sup>[1]</sup> reduction** and  
**control the diffusion of noise**

[1]EMI: Electro-Magnetic Interference

# Research Summary

## Proposed method

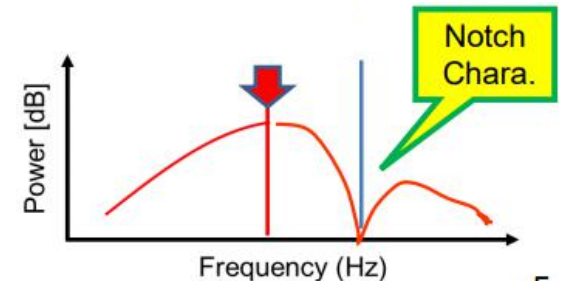
Spread spectrum method using pulse coding



Design modulation circuit  
in order to generate notch frequency automatically

## Achievement

- ① Reduction of EMI generated from clock
- ② **Noise removal** at specific frequency
- ③ **Automatic generation** of notch frequency



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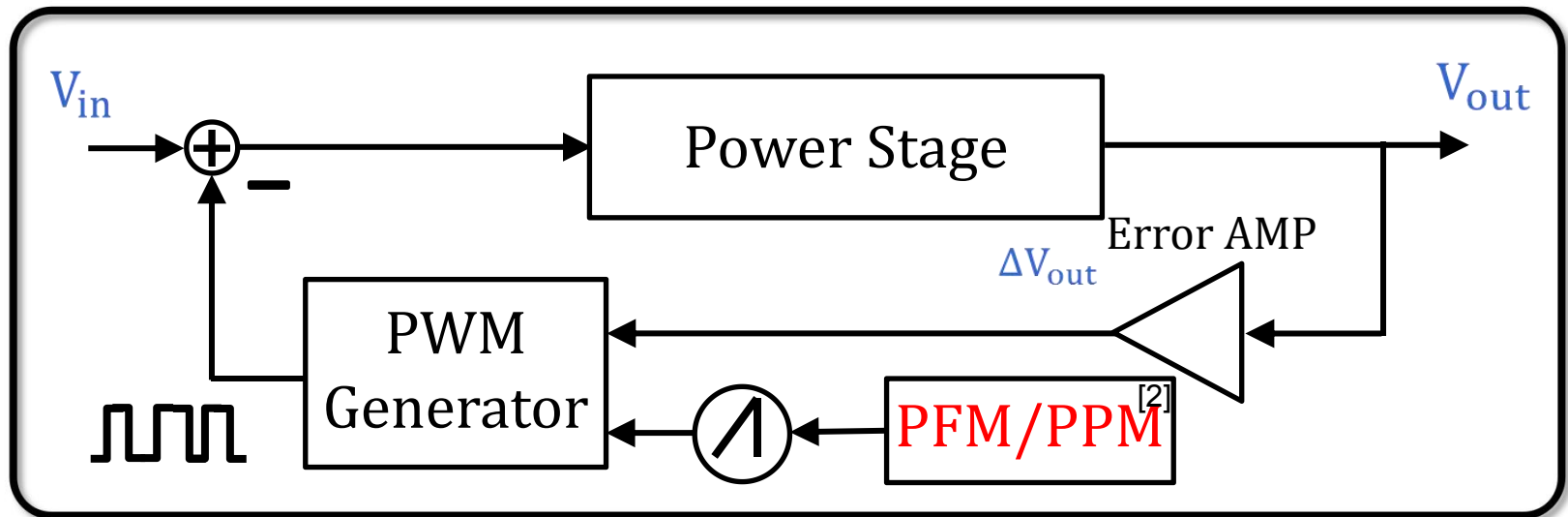
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# Conventional Switching Converter with Spread Spectrum

## Spread Spectrum

Continuous modulation of periodic clock

⇒ Reduction of EMI concentrating on  
fundamental frequency



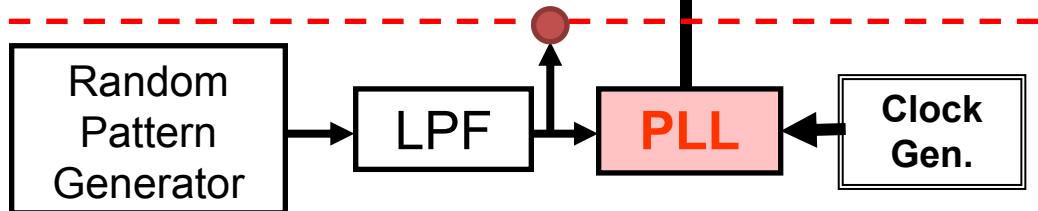
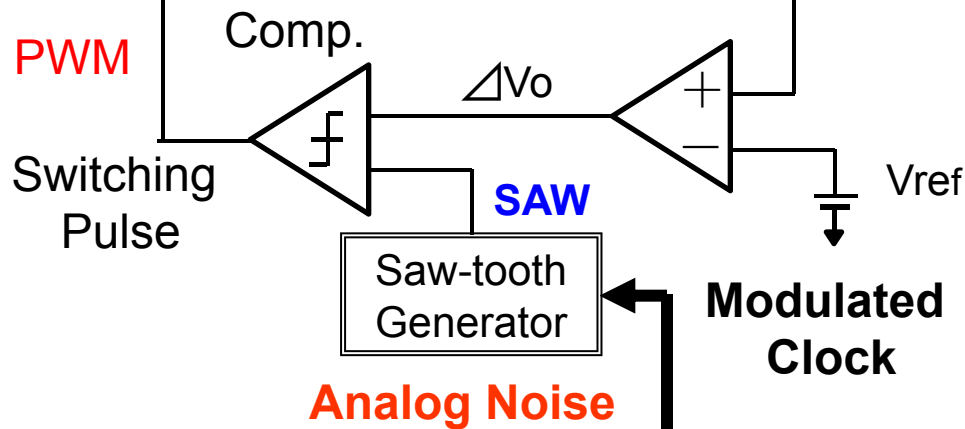
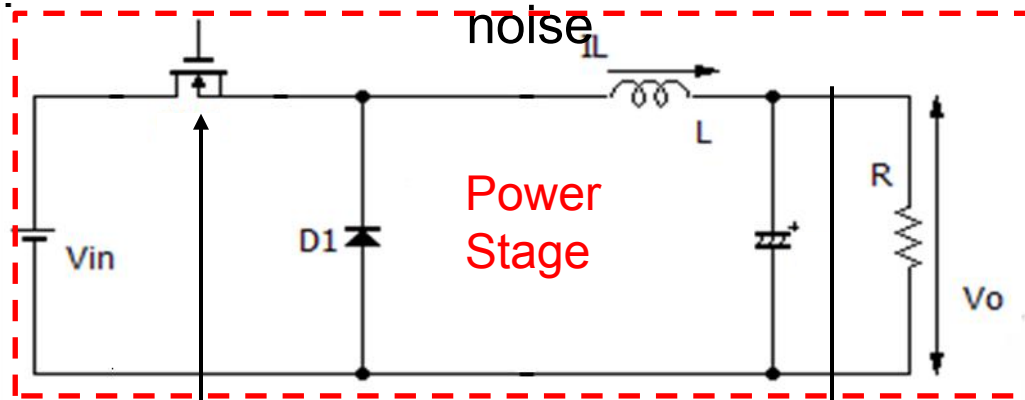
Switching Power

[2] PFM: Pulse Frequency Modulation PPM: Pulse Phase Modulation



# Spread Spectrum for EMI Reduction

Spread spectrum using pseudo **analog** noise

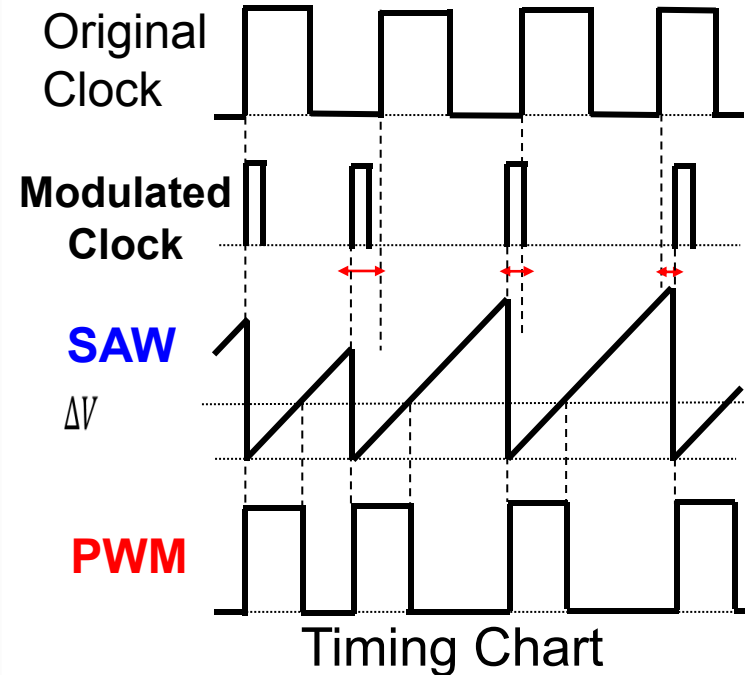


Buck converter with modulated clock

To reduce EMI noise, clock pulse is modulated



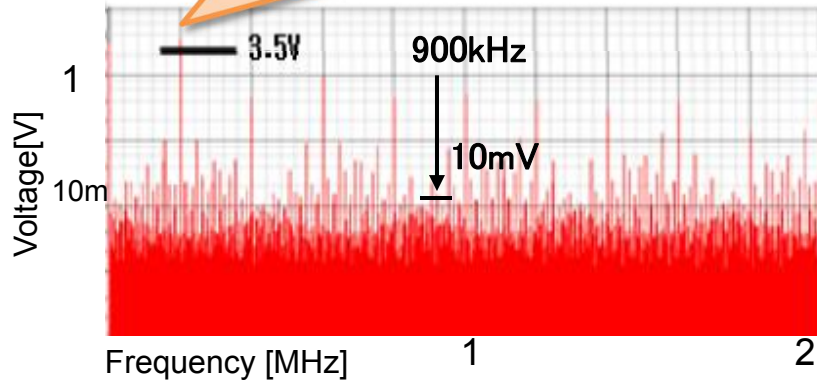
\* Clock to SAW is modulated by shaking phase using analog noise & PLL<sup>[3]</sup>



[3] PLL: Phase Locked Loop

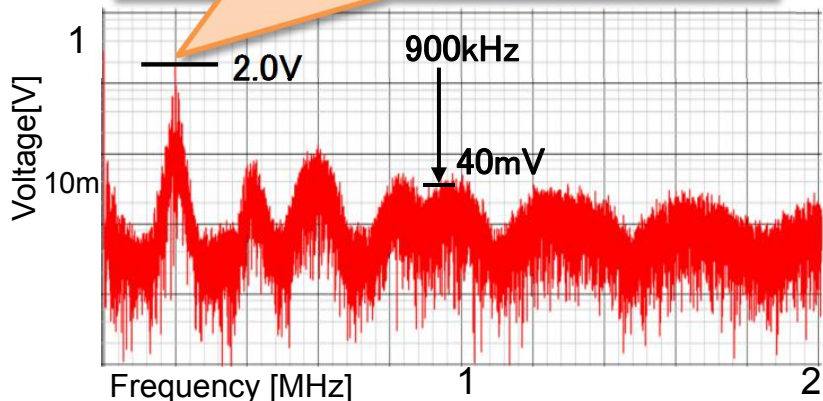
# Spread spectrum for EMI Reduction

Maximum noise **3.5V**



PWM signal spectrum without EMI reduction

Maximum noise **2.0V**



PWM signal spectrum with EMI reduction

◎ Simulation conditions

Input : 12V

Output : 6V

Clock frequency: **200kHz**

Without EMI reduction

- Noise is concentrated in basic and harmonic frequencies

**With EMI reduction**

- **Peak level** of clock frequency is reduced a lot



Noise is concentrated by diffusion



Bottom levels are increased

**NG**

# OUTLINE

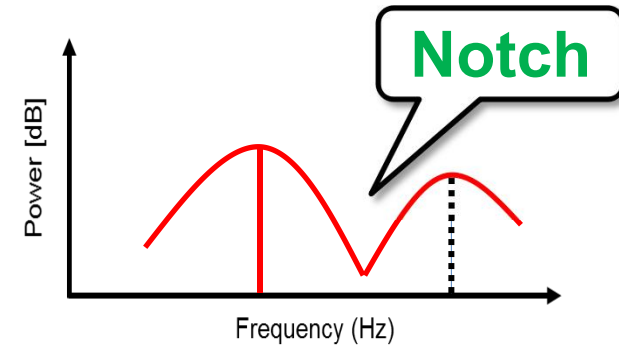
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# Diffuse Noise to Specific Frequency

## Problem

Noise diffusing uniformly  
(using analog modulation)



Using digital modulation

Noise diffuses to specific frequency



Frequency band where  
noise does not spread

**Notch band** created in important frequency band



- EMI Reduction
- Control of diffused noise

# Coding Method

## Single coding method

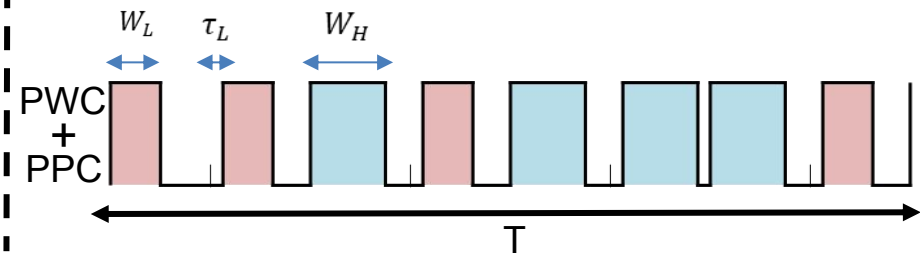
Pulse width · period · position  
select **one** to modulation

- PWC(Pulse Width coding)method
- PCC(Pulse Cycle coding) method
- PPC(Pulse Phase coding) method

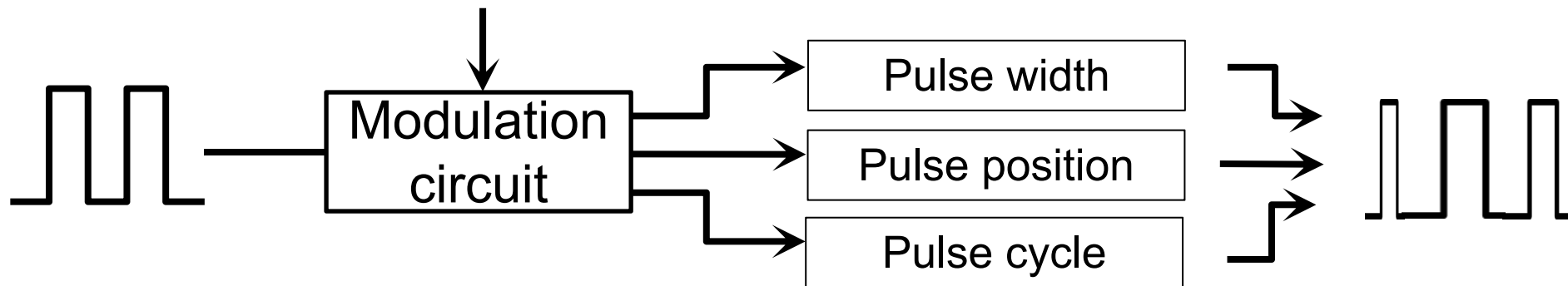
## Complex coding method

Pulse width · period · position  
select **two** to modulation

- PWPC (PWC+PPC) method

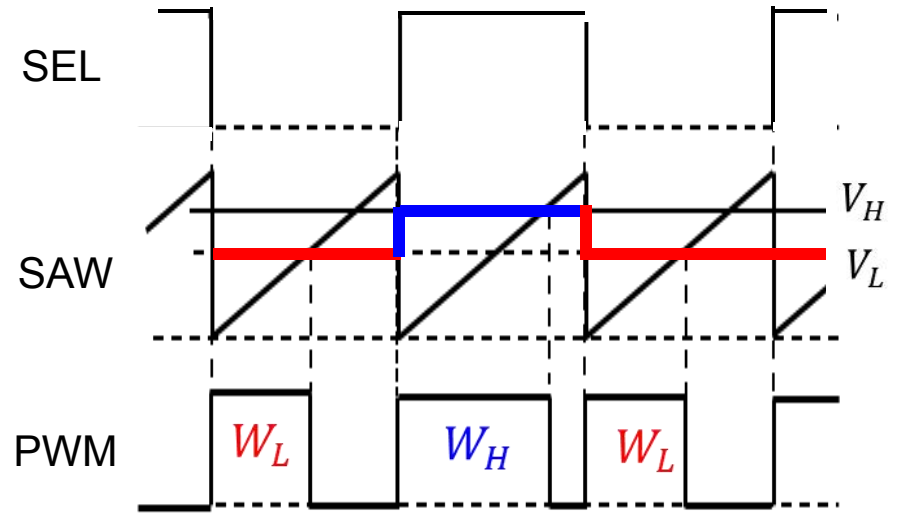
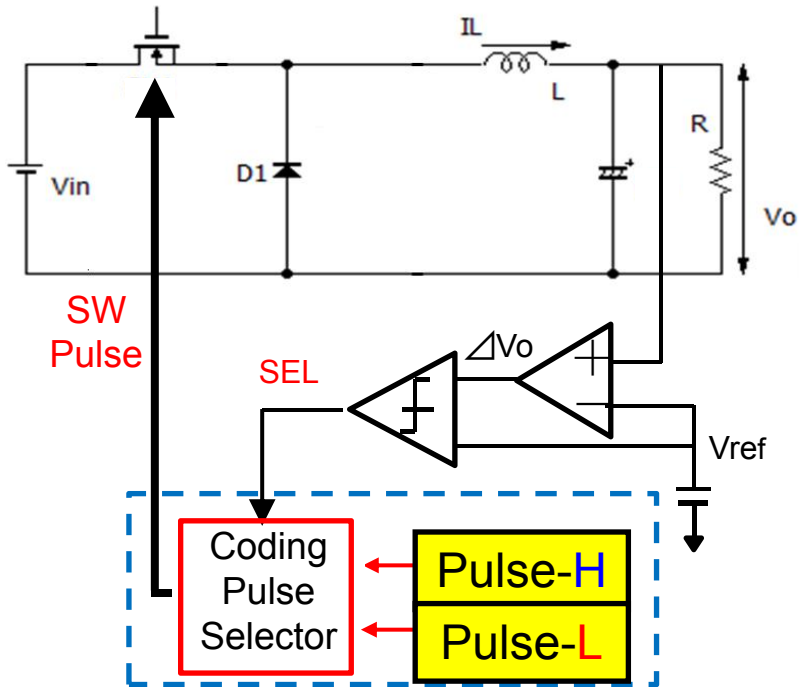


0/1 Signal



Complex coding method

# Pulse Width Modulation in Switching Converter



Input **High**

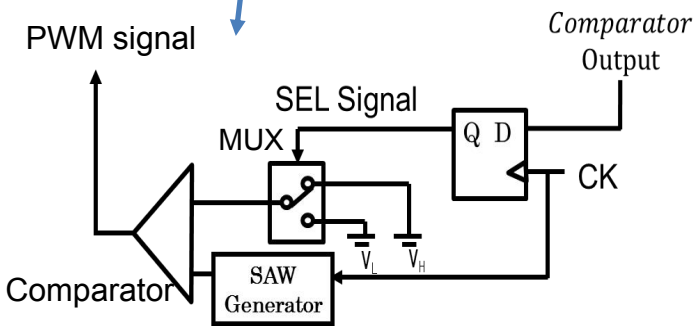
- ① SEL: **High**
- ② MUX select  $V_H$
- ③ Generate pulse with **long width** in comparator

Input **Low**

- ① SEL: **Low**
- ② MUX select  $V_L$
- ③ Generate pulse with **short width** in comparator

$$\star D_H > D_O > D_L$$

$$D_O = V_O / V_{in}$$



**★ manually set  $W_L$  and  $W_H$**

# Simulation Result with PWC Control

## ◎ Condition

Buck DC-DC converter

$V_{in}$  : 10V

$V_{out}$  : 5V

$L$  : 200  $\mu$  H

$C$  : 470  $\mu$  F

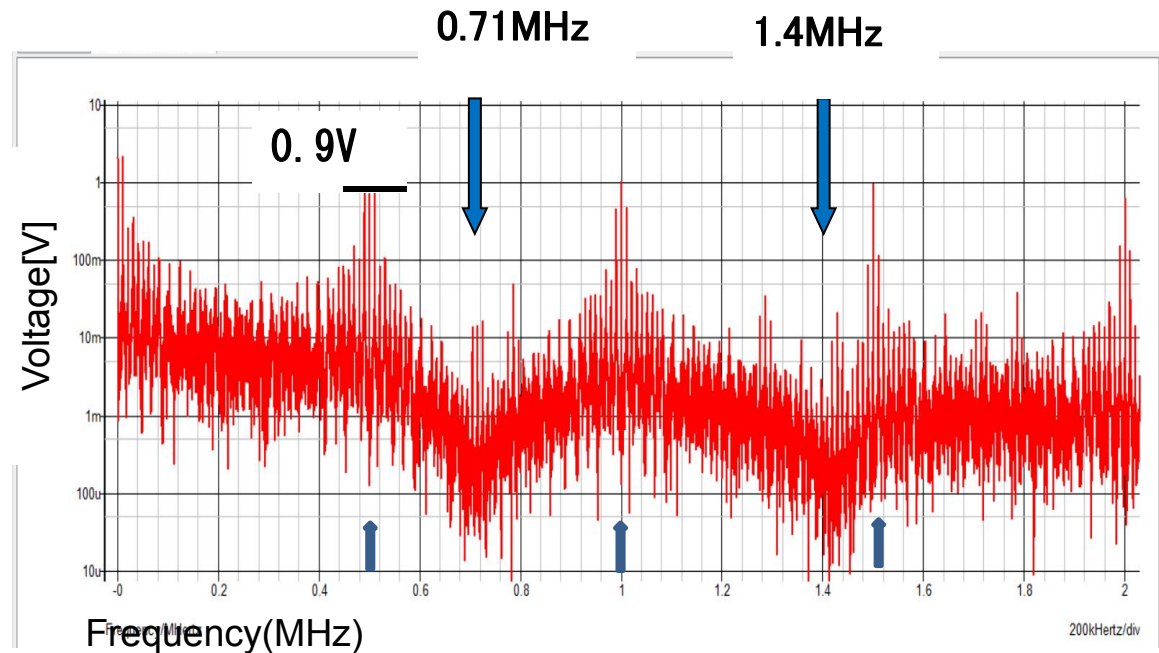
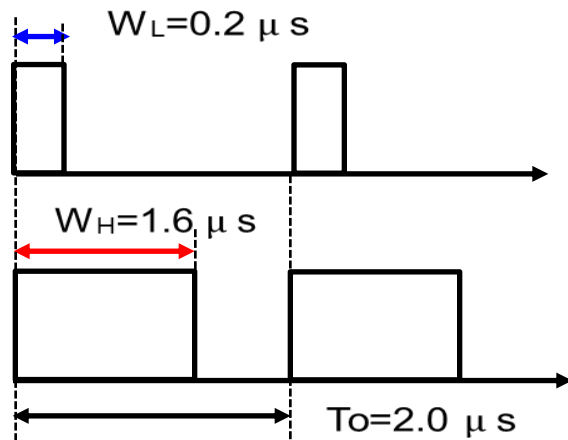
$I_{out}$  : 0.25A

$f_{ck}$  : 500kHz

Design clock pulse to determine the notch frequency

$$f_n \cong N \times \frac{1}{(W_H - W_L)} \quad [N = 1, 2, 3, \dots, n]$$

$$= N \times \frac{1}{1.6\mu s - 0.2\mu s} = 0.71 \text{ MHz}$$



Pulse widths of the coding pulses

PWM signal spectrum using PWC control

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# Automatic PWC Control

Set frequency of radio reception



Auto corresponding to  $F_{in}$  change is necessary



Notch frequency

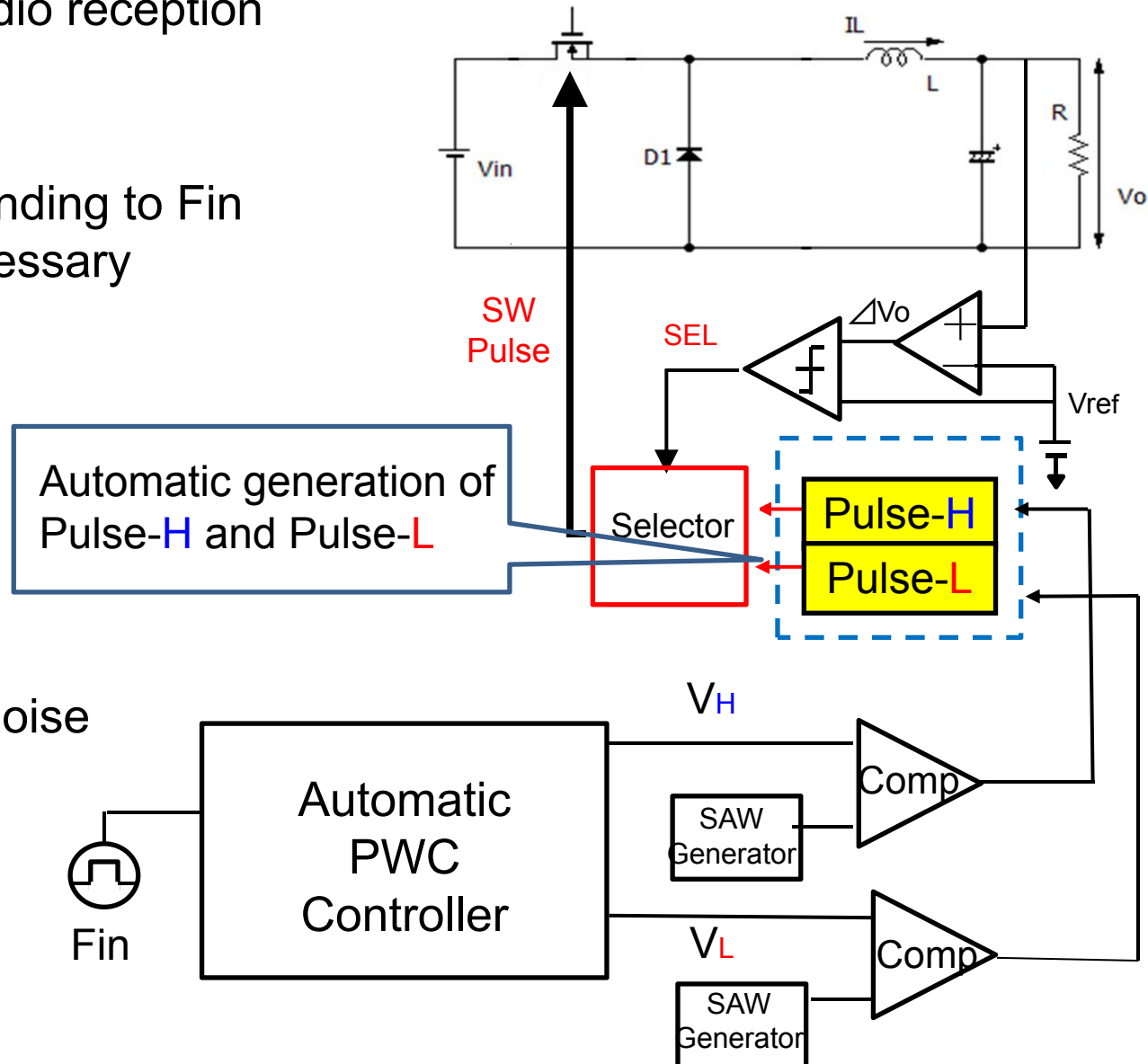


Research objective

Control of diffused noise



Radio receiver

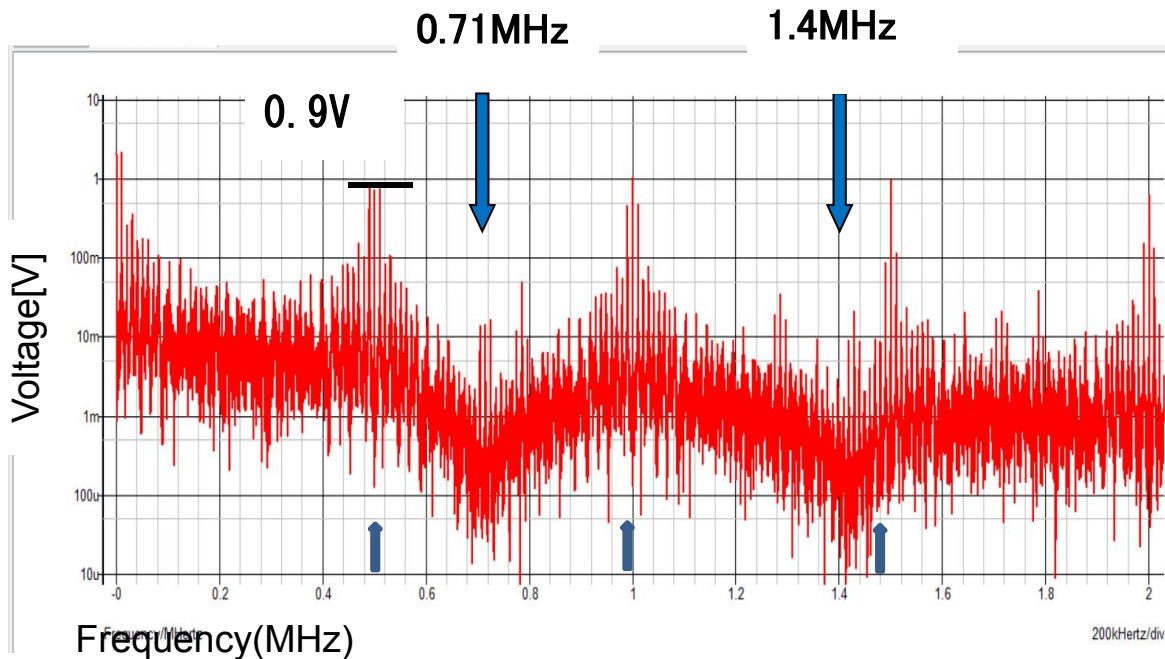


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# Relationship with Clock and Notch

$F_{ck} : 500\text{kHz}$



PWM signal spectrum using PWC control

Better to generate  $F_n$  at  
middle of  $F_{ck}$

$$F_{ck} < F_n < 2F_{ck}$$

$$NF_{ck} < F_n < (N + 1)F_{ck}$$

Optimal

$$F_n = (N + 0.5)F_{ck}$$

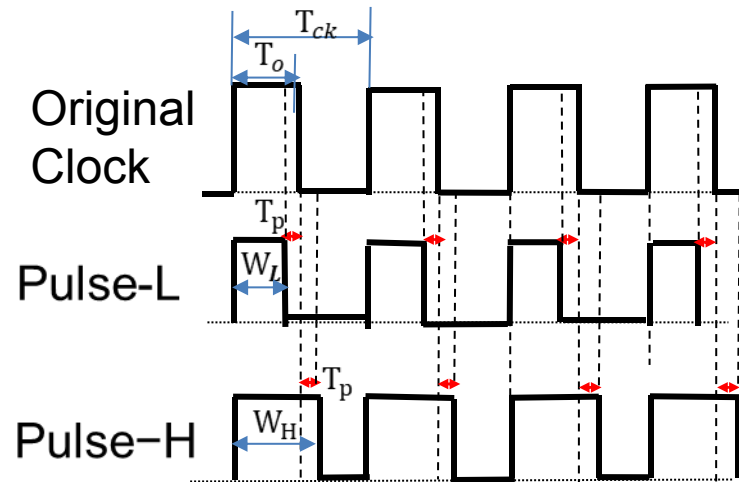
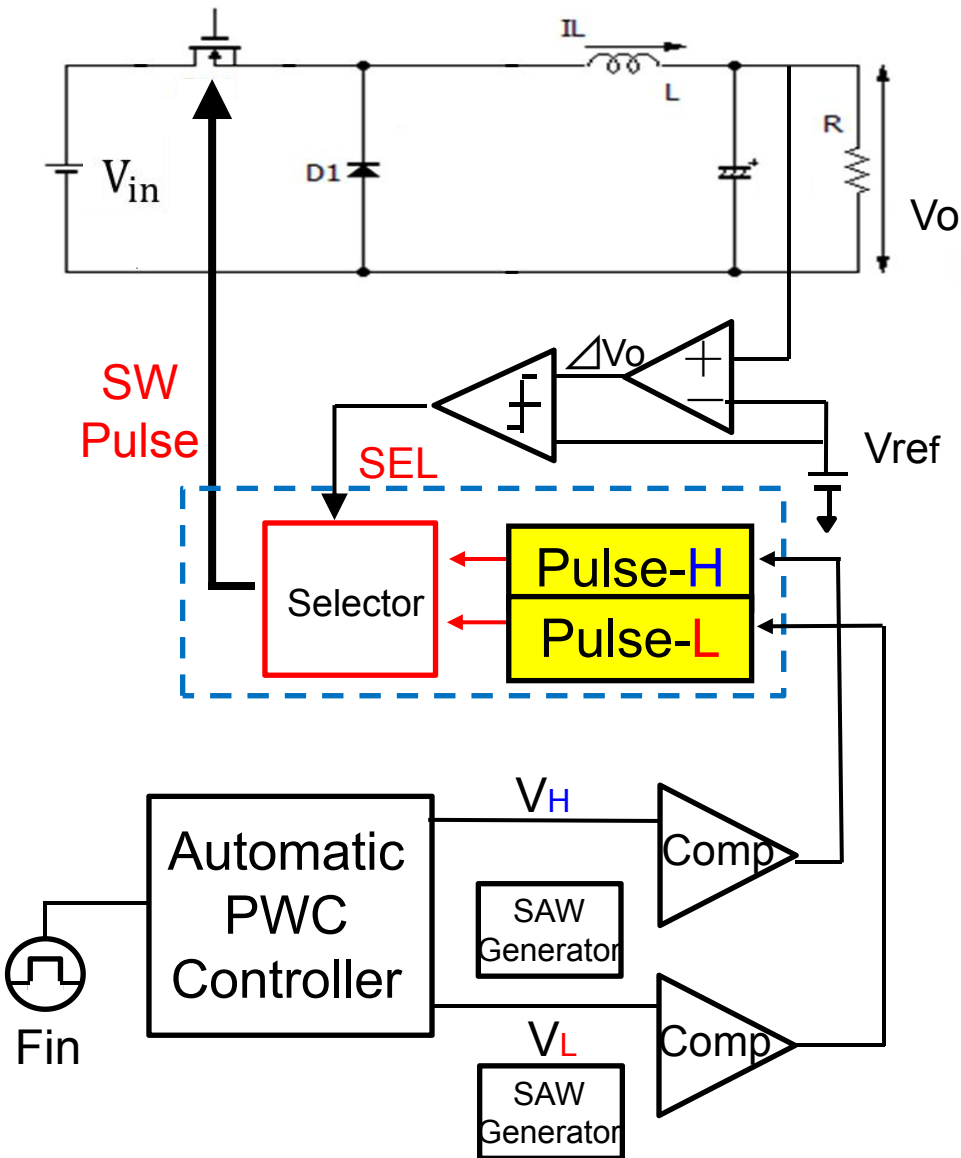
When  $N=1$

Optimal

$$F_n = 1.5F_{ck}$$

$$\frac{F_n}{3} = \frac{F_{ck}}{2}$$

# Relationship between Pulse-H and Pulse-L



Timing Chart

$$T_o = D_o \times T_{ck} = \frac{V_o}{V_{in}} \times T_{ck}$$

$$W_L = T_o - T_p$$

$$W_H = T_o + T_p$$

$$T_n = W_H - W_L = 2 \times T_p$$

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# Generating Tck using Direct Calculation

Generate Tck from Tin using:

$$F_{in} = (N + 0.5) \cdot F_{ck}$$

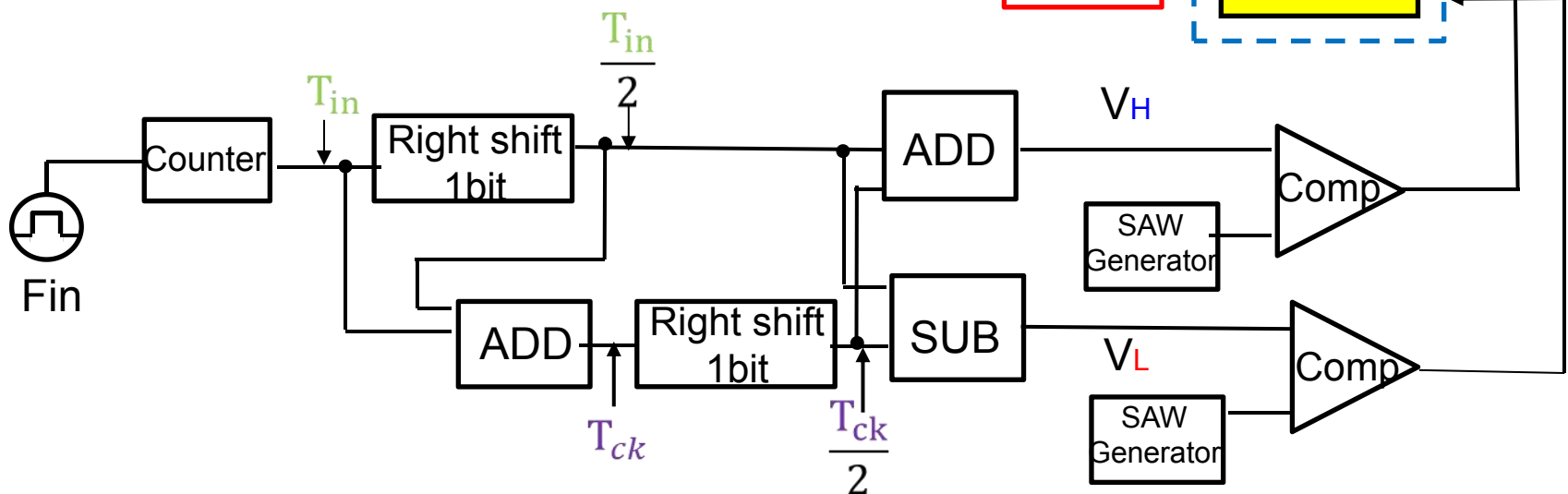


$$T_{ck} = (N + 0.5) \cdot T_{in} \quad N=1 \quad D_o=0.5$$

$$W_L = T_o - T_p = D_o \times T_{ck} + \frac{1}{2} T_{in}$$

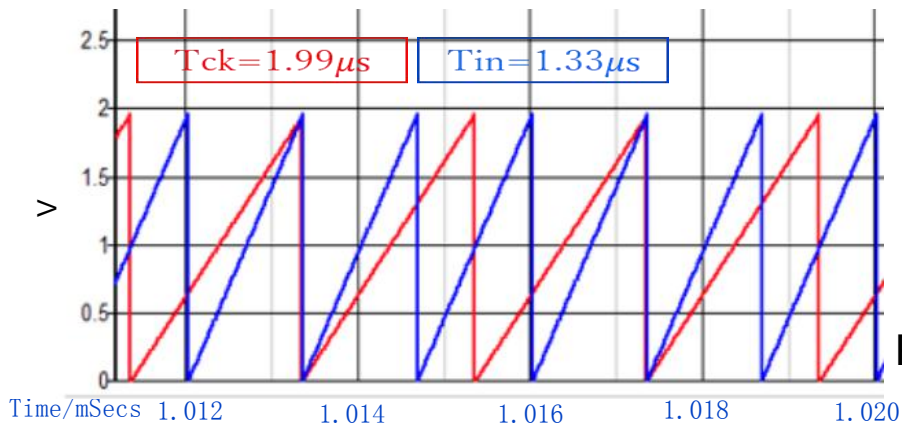
$$W_H = T_o + T_p = D_o \times T_{ck} - \frac{1}{2} T_{in}$$

$$T_n = 2 \times T_p$$



# Simulation Waveforms of $W_H$ , $W_L$ Generation

We set  $F_{in} = 750kHz$   $\rightarrow$  Automatic generated  $F_{ck} = 500kHz$



Simulation waveform of Tck and Tin

$$T_{ck} = (N + 0.5)T_{in} = 1.5T_{in}$$

Theoretical formula

$$W_H = 1.66\mu s$$

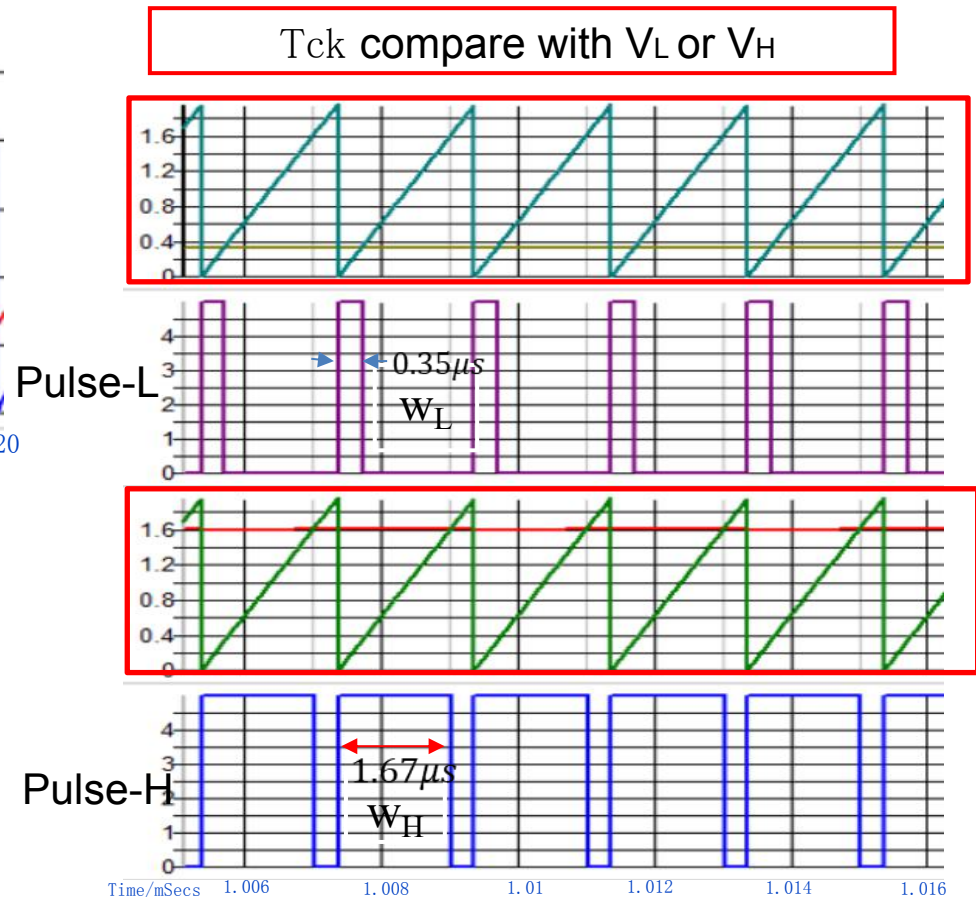
$$W_L = 0.38\mu s$$

Simulation result

$$W_H = 1.67\mu s$$

$$W_L = 0.35\mu s$$

Well  
matched



Simulation waveform of  $W_H$  and  $W_L$

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# Simulated Noise Spectrum of PWM Signal Case 1

According to

$$F_{in} = (N + 0.5)F_{ck}$$

Case 1 :  $F_{in}=750\text{kHz}$ ,  $N=1 \Rightarrow F_{ck}=500\text{kHz}$ ,  $W_H=1.66\mu\text{s}$ ,  $W_L=0.38\mu\text{s}$

**Result:**  $F_n=750\text{ kHz}$ ,  $F_{ck}=500\text{ kHz}$ ,  $F_{ck} < F_n < 2F_{ck}$

## © Condition

Buck DC-DC converter

$V_{in} : 10\text{V}$

$V_{out} : 5\text{V}$

$L : 200\ \mu\text{H}$

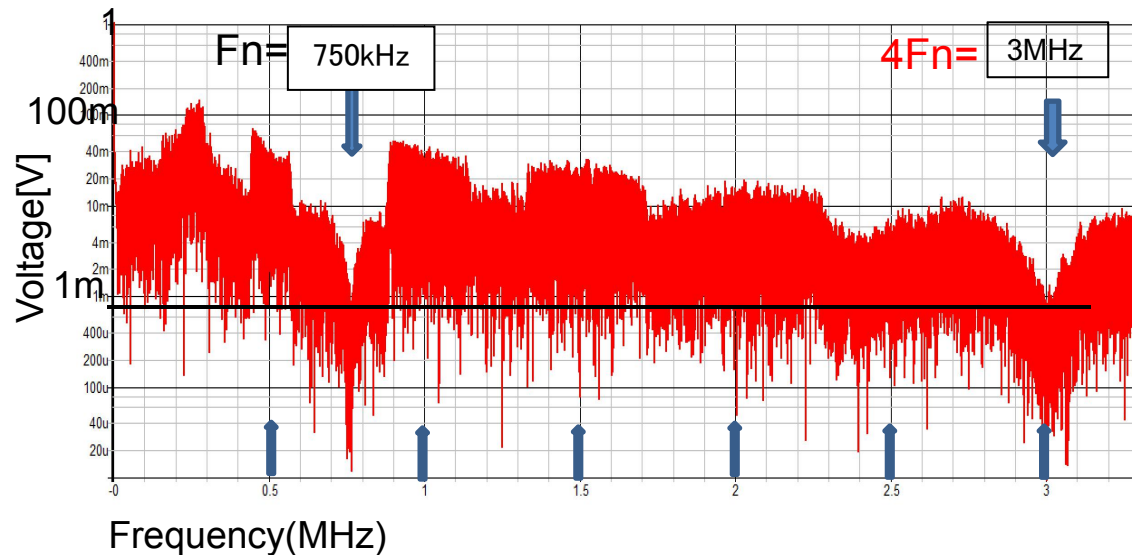
$C : 470\ \mu\text{F}$

$I_{out} : 0.25\text{A}$

## © Result

$F_n=750\text{kHz}$

$4 \cdot F_n=3.0\text{MHz}$



Simulated spectrum with EMI reduction

Assume to suppress influence on AM radio in 750kHz  
 $\Rightarrow$  A notch was generated around **750kHz**

# Simulated Noise Spectrum of PWM Signal Case 2<sup>26/38</sup>

Case 2:  $F_{in}=1.25\text{MHz}$ ,  $N=2 \Rightarrow F_{ck}=500\text{kHz}$ ,  $W_H=1.40\mu\text{s}$ ,  $W_L=0.60\mu\text{s}$

Result:  $F_n=1.27\text{MHz}$ ,  $F_{ck}=500\text{kHz}$ ,  $2F_{ck} < F_n < 3F_{ck}$

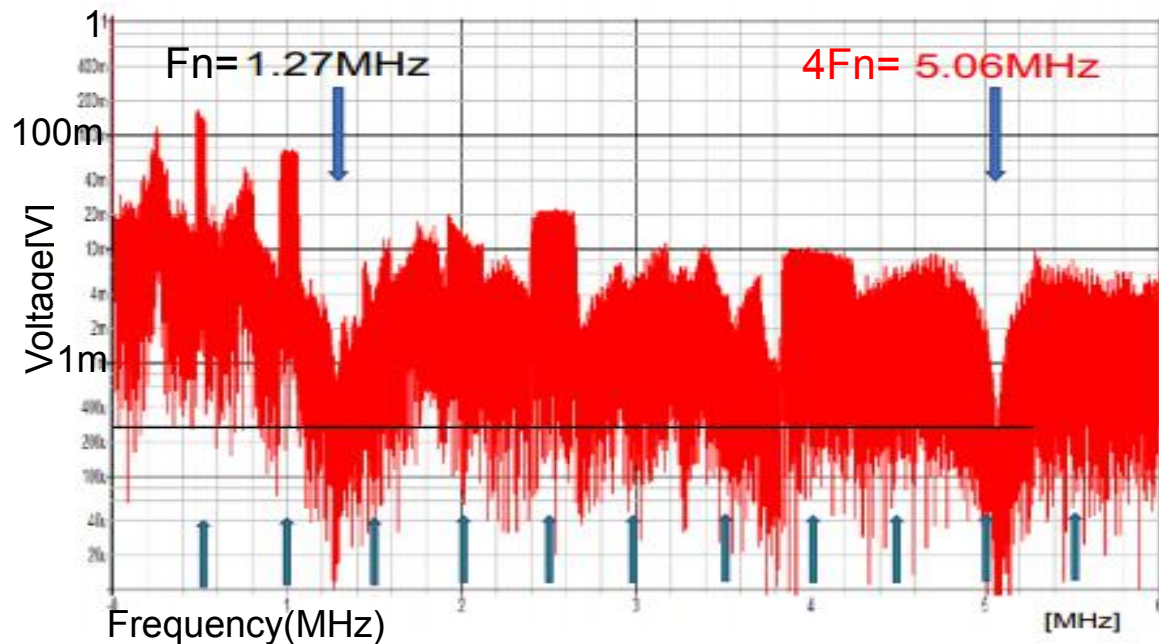
## © Simulation Result

$F_n=1.27\text{MHz}$

$4F_n=5.05\text{MHz}$

\* Compare bottom levels

$4F_n$  is deeper than  $F_n$



© Condition : same

Simulated spectrum with EMI reduction

# Transient Response with $F_{in}$ Change in Case 2

## ◎ Condition (N= 2 )

$$F_{in} = 1.25\text{MHz} \rightarrow F_{in} = 1\text{MHz}$$

$$F_{in} = 1.25\text{MHz} \rightarrow F_{in} = 750\text{kHz}$$

Settling Time  $\approx 0\mu\text{s}$

## ◎ Output stability

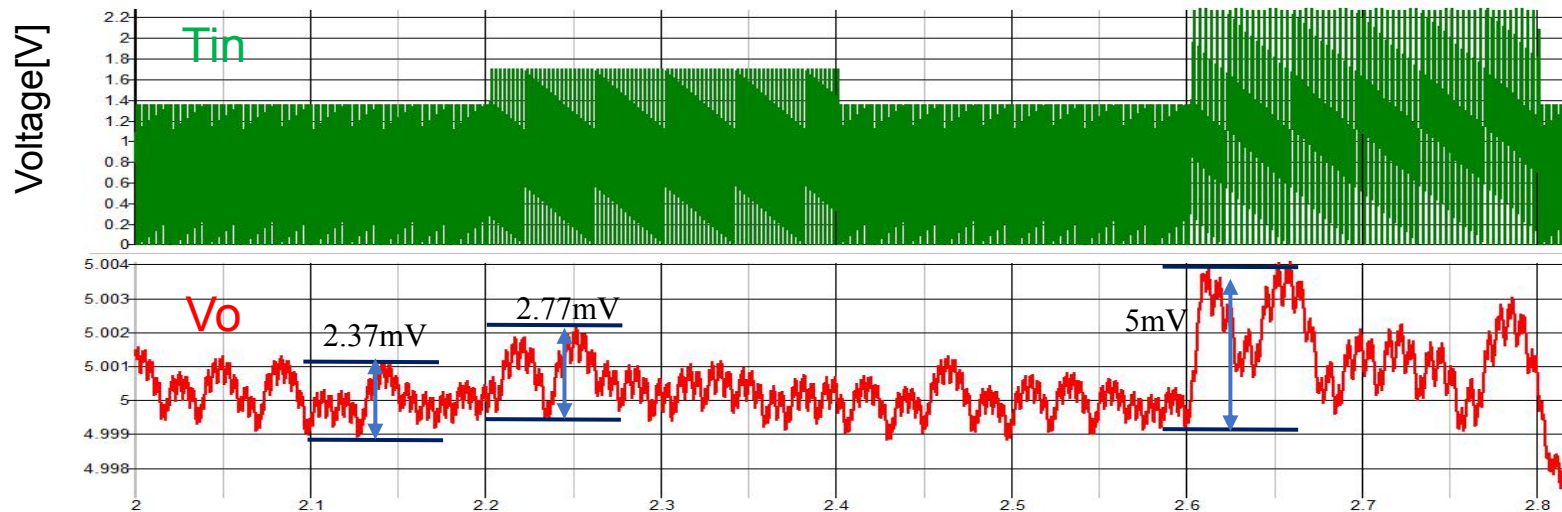
Ripple:  $2.37\text{mV}_{pp}$  at  $F_{in} = 1.25\text{MHz}$

$2.77\text{mV}_{pp}$  at  $F_{in} = 1\text{MHz}$

$5\text{mV}_{pp}$  at  $F_{in} = 750\text{kHz}$

Static ripple is about 0.1% of the output voltage  $V_o$

stable



Transient response with  $F_{in}$  change

Response speed is important when tuning or switching communication channels

# Simulated Noise Spectrum of PWM Signal Case 3 <sup>28/38</sup>

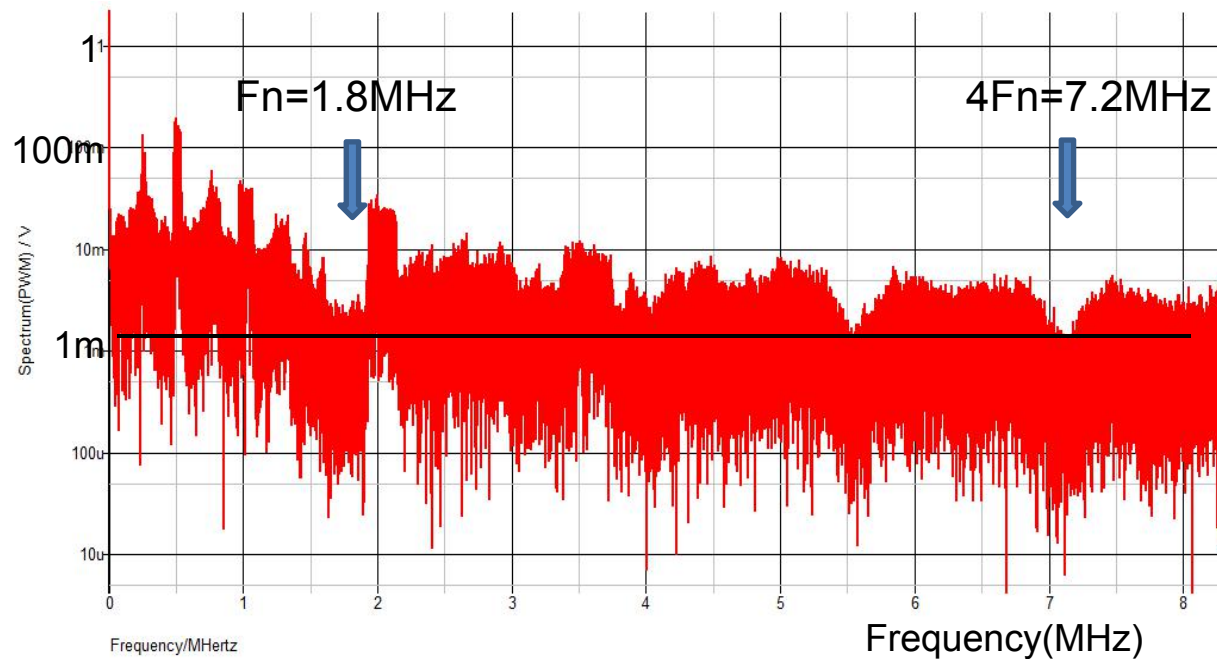
Case3 :  $F_{in}=1.75\text{MHz}$ ,  $N=3 \Rightarrow F_{ck}=500\text{kHz}$ ,  $W_H=1.29\mu\text{s}$ ,  $W_L=0.72\mu\text{s}$

Result:  $F_n=1.8\text{ MHz}$ ,  $F_{ck}=500\text{ kHz}$ ,  $3F_{ck} < F_n < 4F_{ck}$

## © Simulation Result

$F_n=1.8\text{ MHz}$   
 $4F_n=7.2\text{ MHz}$

\* Compare bottom levels  
Almost equal

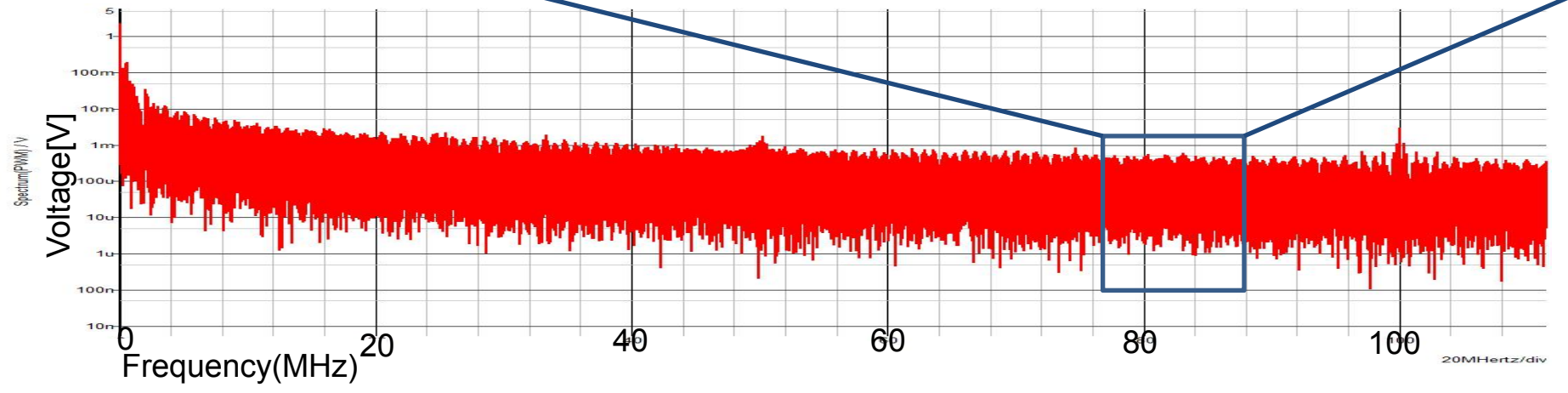
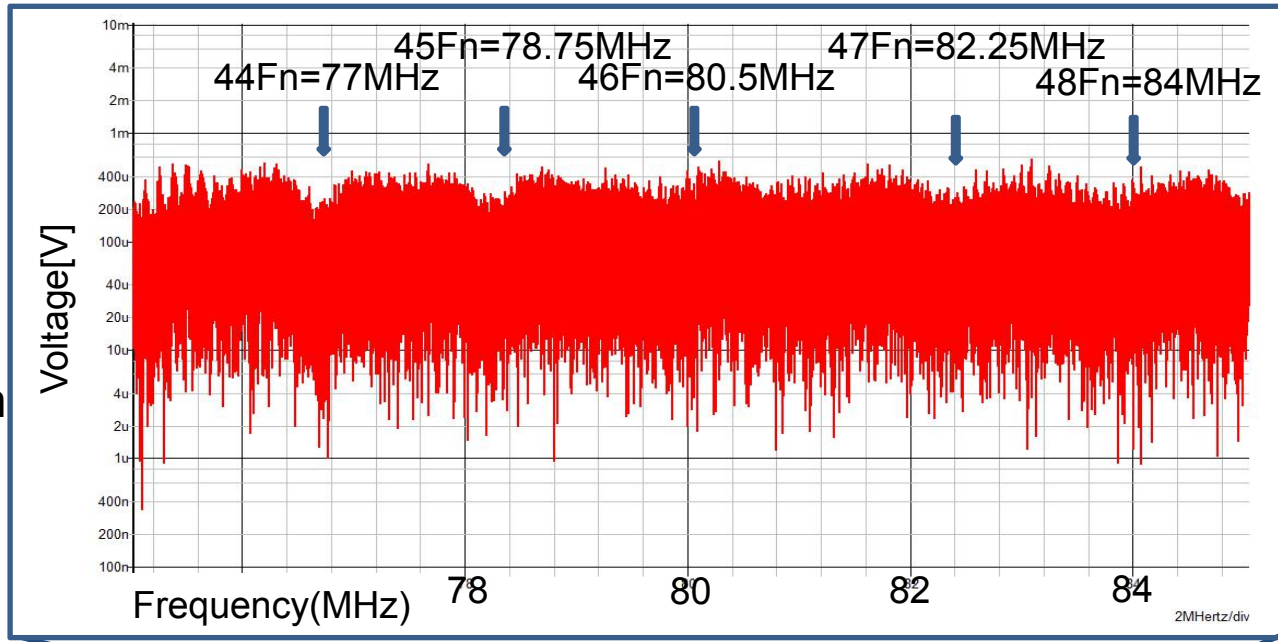


© Condition: same

Simulated spectrum with EMI reduction

# Simulated Noise Spectrum of PWM Signal Case 3

- \* High frequency harmonics is not clear!
- \* But it is good for AM radio receiver. (< 2MHz)
- It needs to generate Notch at higher than 80MHz (FM)



# OUTLINE

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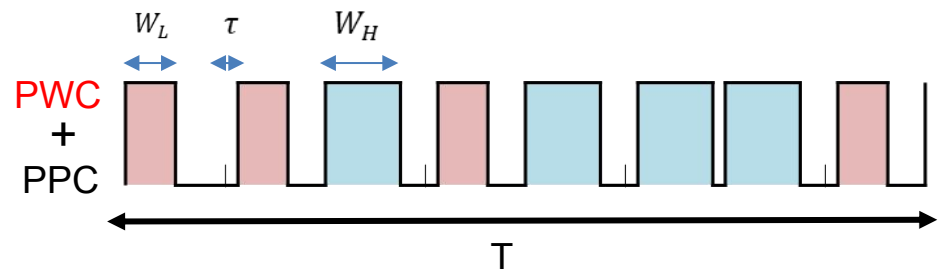
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# PWPC Method

## Complex coding method

PWPC (**P**ulse **w**idth **c**oding + **P**ulse **p**hase **c**oding) method

PPC \ PWC	$W_L$	$W_H$
$\phi_L$ (= 0)		
$\phi_H$		

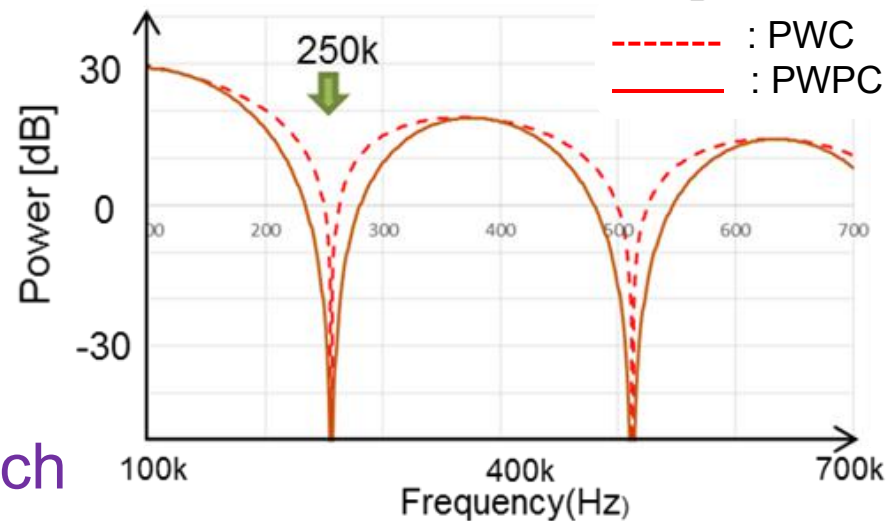


Expect

Condition:

$$W_H = 7\mu s$$

$$W_L = 3\mu s$$



Theoretical formula

$$f_{notch1} = \frac{n}{(W_H - W_L)}$$

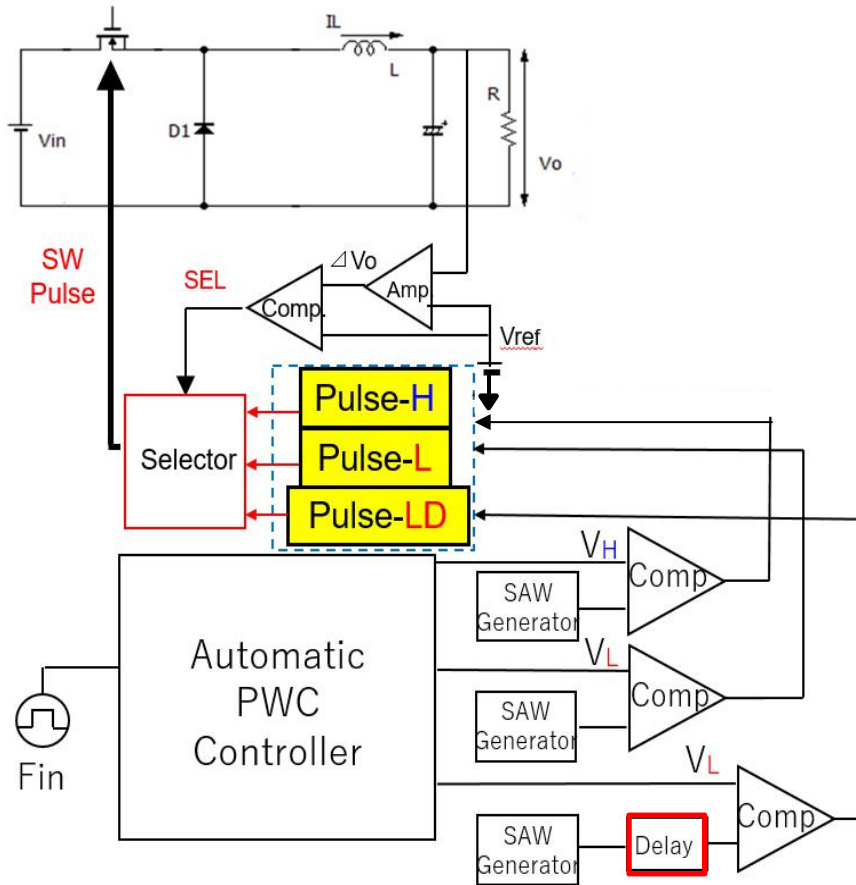
$$f_{notch2} = \frac{n}{2|\tau_H - \tau_L|}$$

Set  $f_{notch1} = f_{notch2}$

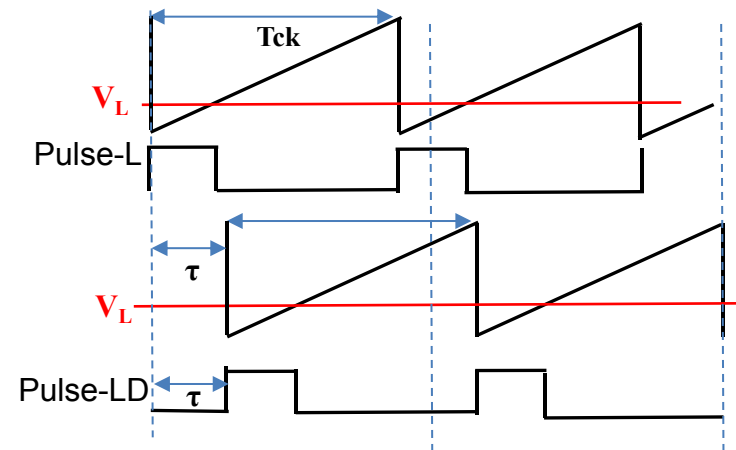
➡ Big Notch

# Automatic Generation of Notch Frequency with PWPC Control

## Automatic pulse generation



Pulse coding of PWPC method



Design timing in PWPC method

$$W_H = T_o + T_p = D_o \times T_{ck} + 0.5T_{in}$$

$$W_L = T_o - T_p = D_o \times T_{ck} - 0.5T_{in}$$

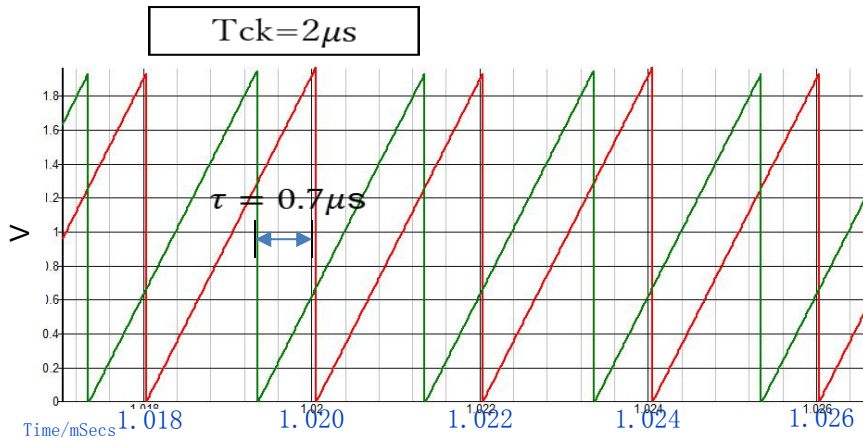
$$\tau = (W_H - W_L) / 2 = 0.5 \times T_{in}$$



# Simulation Waveforms of $W_H$ , $W_L$ Generation

We set  $F_{in} = 750kHz$   $\Rightarrow$  Automatic generated  $F_{ck} = 500kHz$

$$f_{notch1} = f_{notch2} \Rightarrow \frac{n}{(W_H - W_L)} = \frac{n}{2|\tau_H - \tau_L|} \Rightarrow \tau_H - \tau_L = \tau = \frac{W_H - W_L}{2} = \frac{T_{in}}{2}$$



Simulation waveform of Tck and delay Tck

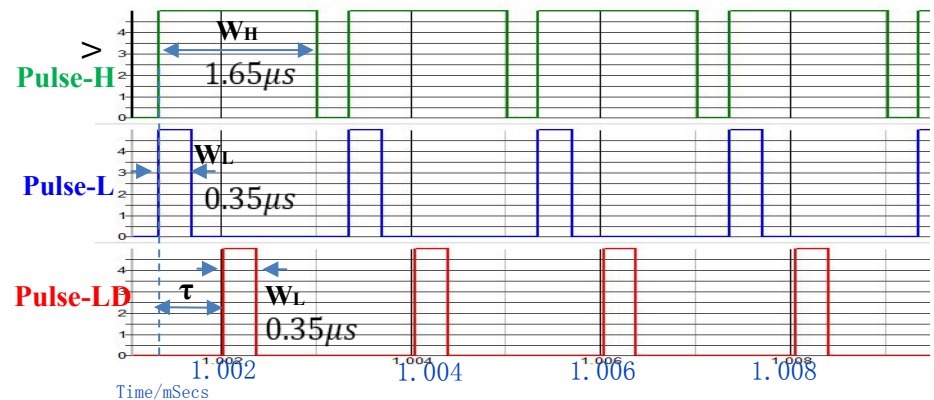
Theoretical formula result

$$W_H = 1.67 \mu$$

$$W_L = 0.33 \mu$$

$$\tau = 0.67 \mu$$

Well  
matched



Simulation waveform of Pulse-H,  
Pulse-L and delay Pulse-L

Simulation result

$$W_H = 1.66 \mu$$

$$W_L = 0.38 \mu$$

$$\tau = 0.70 \mu$$

# Simulated Noise Spectrum of PWPC Control

According to  $F_{in} = (N + 0.5)F_{ck}$

$F_{in}=750\text{kHz}$  ,  $N=1 \Rightarrow F_{ck}=500\text{kHz}, W_H=1.67\mu\text{s}, W_L=0.33\mu\text{s}$

$F_n=750\text{ kHz}$ ,  $F_{ck}=500\text{ kHz}$ ,  $F_{ck} < F_n < 2F_{ck}$

## © Condition

Buck DC-DC converter

$V_{in}$ : 10V

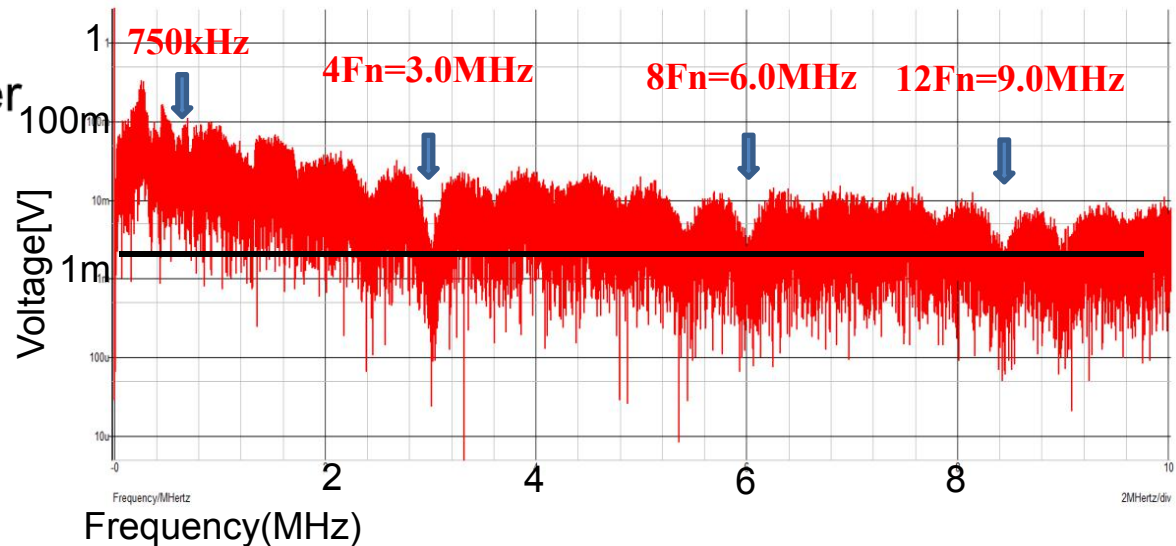
$V_{out}$ : 5V

L: 200  $\mu\text{H}$

C: 470  $\mu\text{F}$

$I_{out}$ : 0.25A

$F_{in}$ : 750kHz



Simulated spectrum with EMI reduction

PWPC characteristic: There are many harmonics of  $4NF_n$

( $N = 1, 2, 3, \dots$ )

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- **Conclusion and future work**

# Conclusion

- Developed pulse coding control in order to generate notch characteristics at desired frequency
- Analyze **spread spectrum** with notch characteristics
- **Automatic generate the notch frequency from  $F_{in}$**

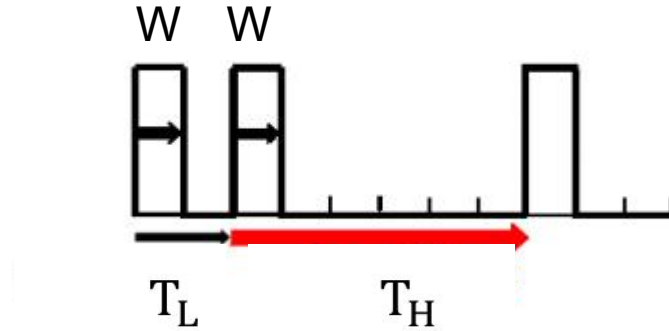


Using  $F_{in} = (N + 0.5)F_{ck}$ , discussion on direct generation of notch in  $N=1,2,3$  situation using PWC control

Automatic generating of notch frequency with PWPC control

# Future Work

- Notch generation using PCC(Pulse Cycle Coding) method



- Investigate why the large notch at  $4F_n$  appear.
- Extend  $4F_n$  in order to high frequency notch generation using PWPC method

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Thank you for Listening

# Q and A

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Q1: Is there any way to get broad notch? Get the width and depth of notch, is it available?

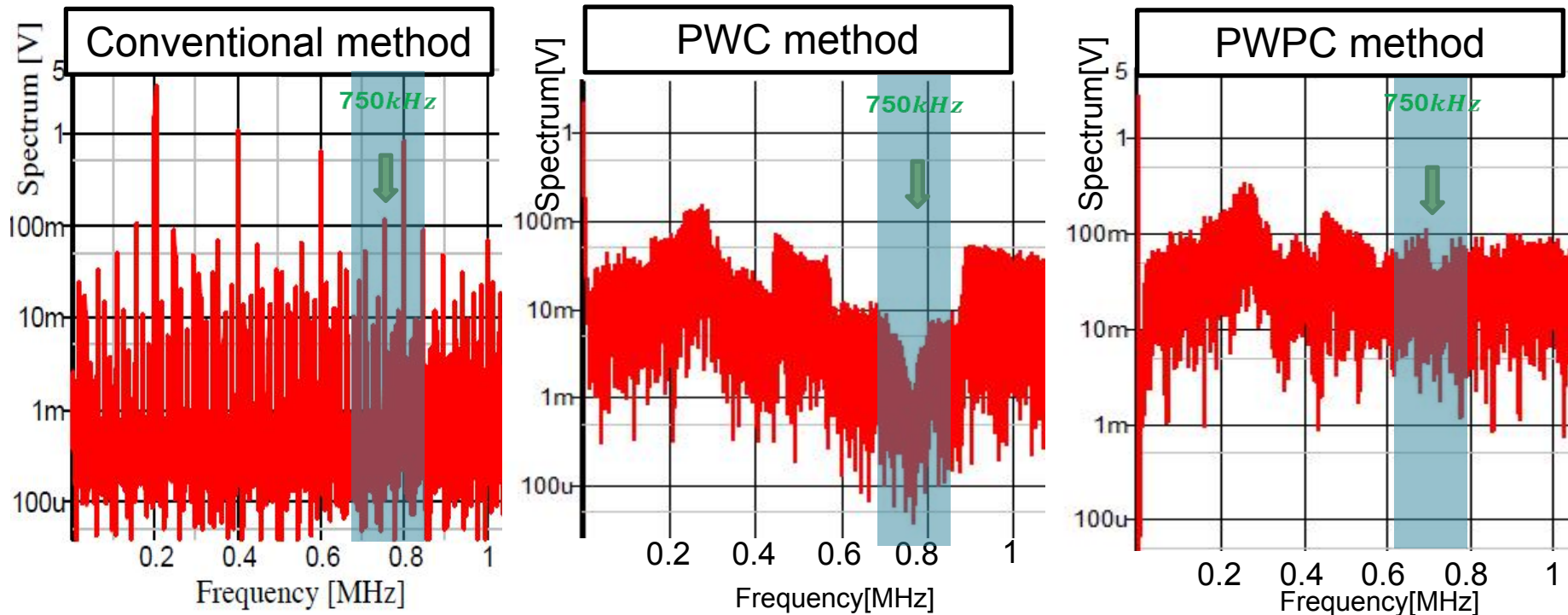
A: In order to get the notch more deep, we come up with PWC, PWPC method, compared with there two method, we found in low frequency, PWC method is better to create deep notch. Also want to consider the PCC method to expect deep notch. I have not consider about to expand the width of notch, I will consider about it in the later.

Q2: Can you tell me the effect of notch frequency depending on the current load change?

A: In the communication devices, there are many changes of the receiving signal and the input frequency, Response speed is important when tuning or switching communication channels. If let the current load change, the change of output voltage is small, it means the system is stable.

# Spectrum Comparison with Proposed Method

- Assumed to suppress the influence on AM radio  
 $\Rightarrow$  A notch is generated around 750 kHz
- Compared with PWC, PWPC and conventional method



$$f_{clock} = 500kHz$$

$$f_{notch} = 750kHz$$

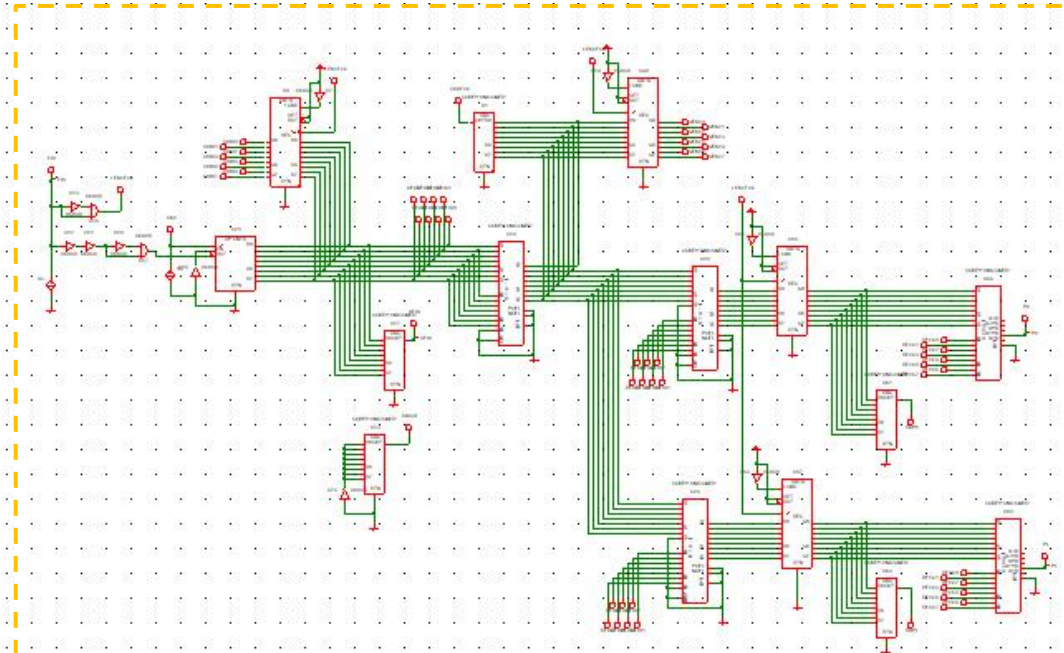
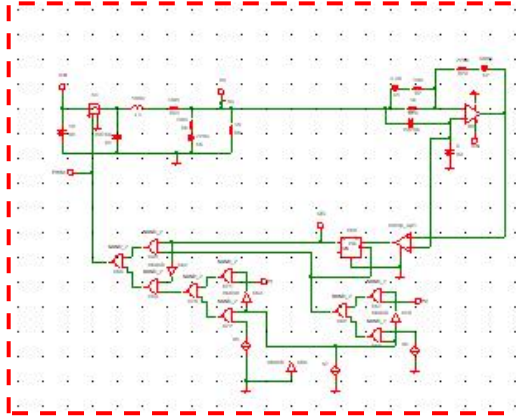
**Spectrum reduced compared with the conventional method!!**



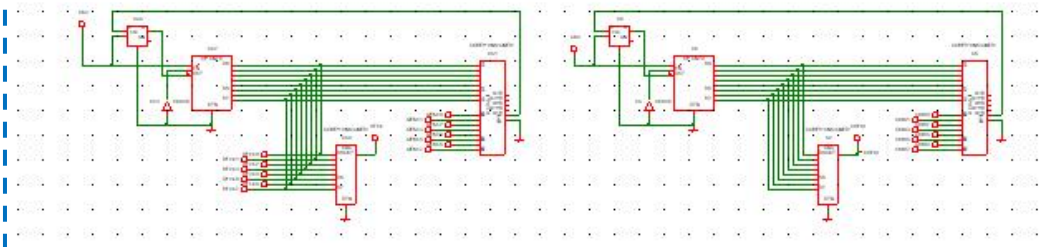
# Automatic Notch Generation using Direct method (N=1)

Direct generation of  $W_H$  and  $W_L$

Buck converter



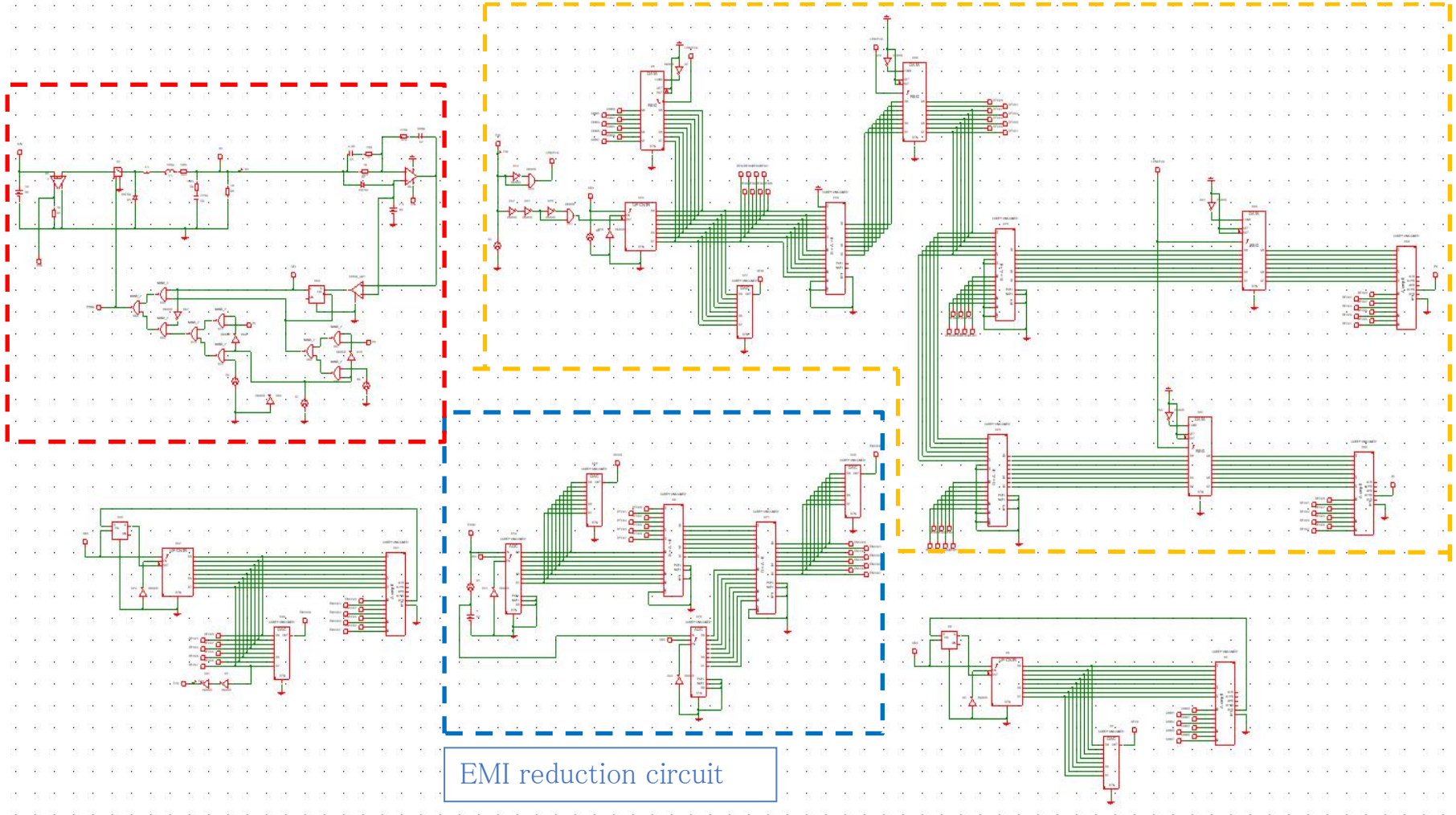
Saw-tooth generator



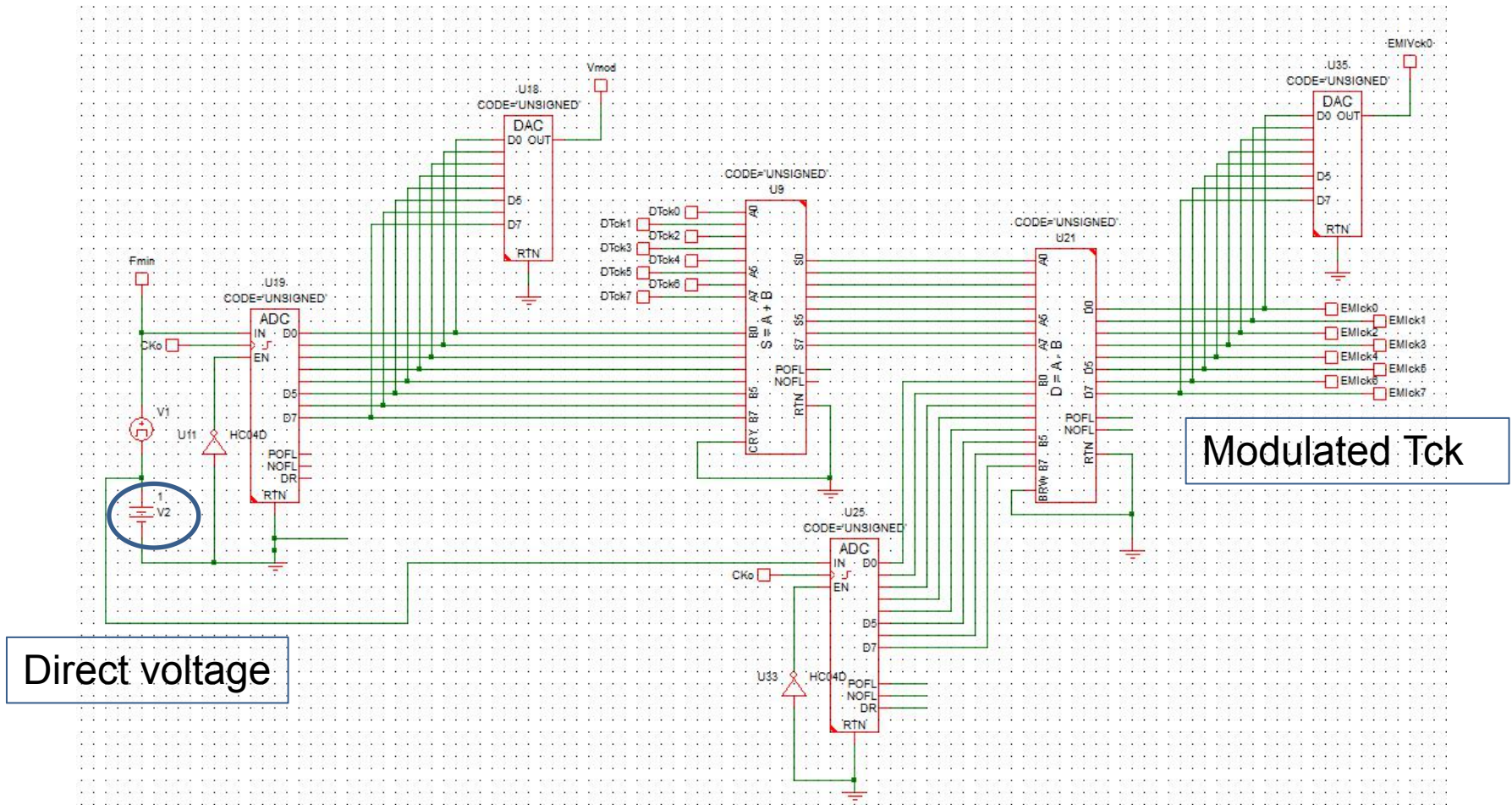
No CPU!

# Automatic Notch Generation using Direct method with EMI Reduction (N=2)

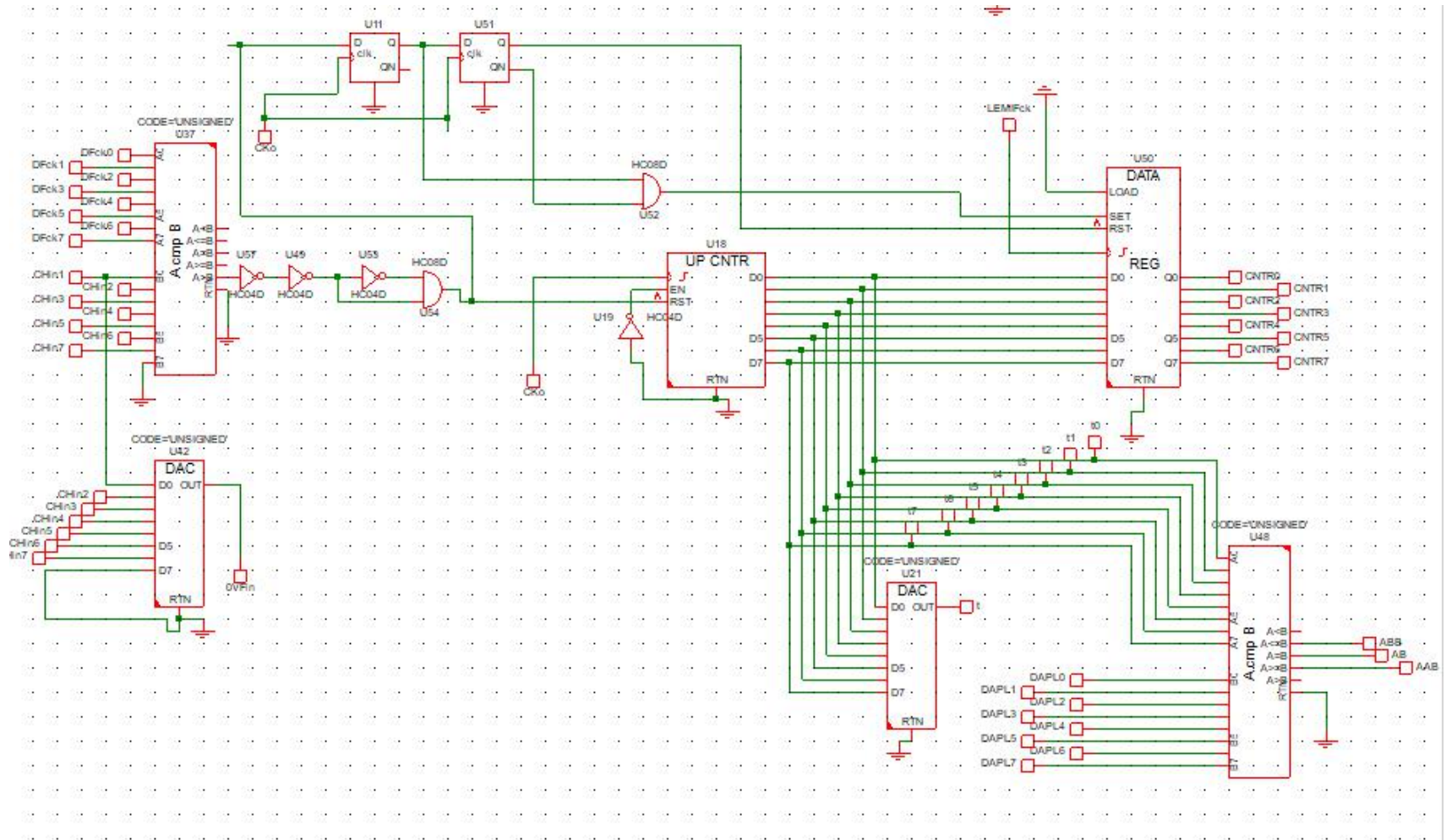
Direct generation of  $W_H$  and  $W_L$



# EMI Reduction



# Produce the delay of Tck



# Application of Automatic Generation of the Notch Frequency



Switching frequency and harmonics used in in-vehicle DC-DC converter must not overlap reception frequency bands of AM, FM of radio

**demand**

Reception frequency from radio receiver

$\approx$  Notch frequency

Frequency band where noise does not spread

**Goal**

**Automatic** generation of notch frequency



DC-DC converter

It is possible to greatly reduce influence on other electronic devices

Set frequency of radio reception

**Auto** correspond to Fin change is necessary



**Radio receiver**

# Transient Response with $F_{in}$ Change in Case 3

## © Condition

$$F_{in} = 1.75\text{MHz} \rightarrow F_{in} = 1.5\text{MHz}$$

## © Output stability

$$\text{Ripple: } 1.69\text{mV}_{pp} \text{ at } F_{in} = 1.75\text{MHz}$$

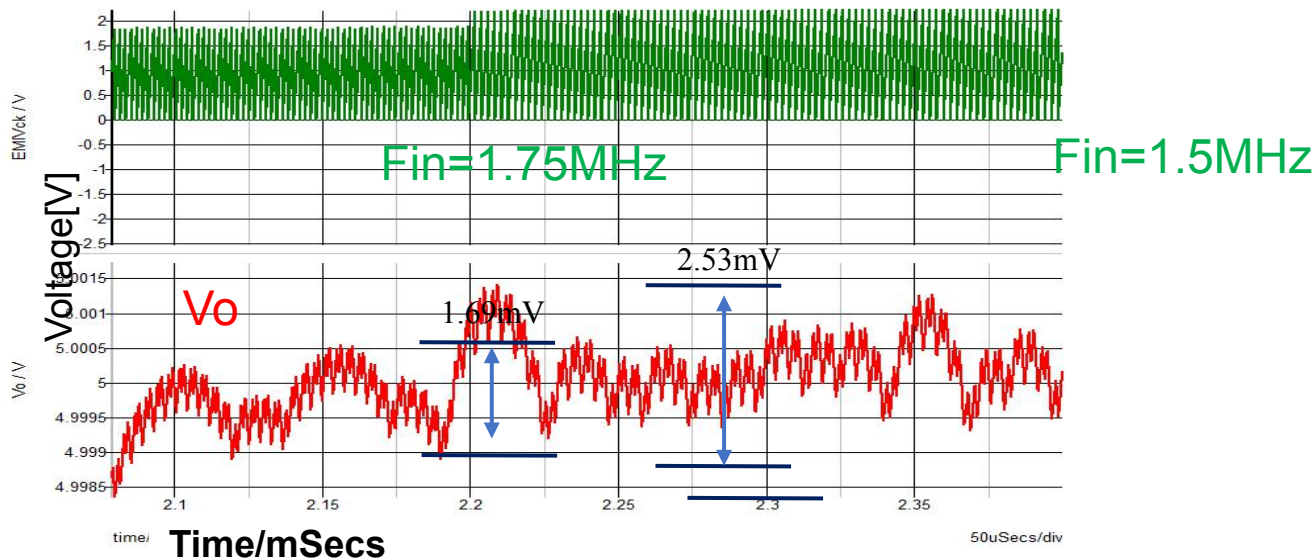
$$2.53\text{mV}_{pp} \text{ at } F_{in} = 1.5\text{MHz}$$

$$\text{Static ripple: } 2.53\text{mV}_{pp}$$

$$V_o : 5.0\text{V}$$

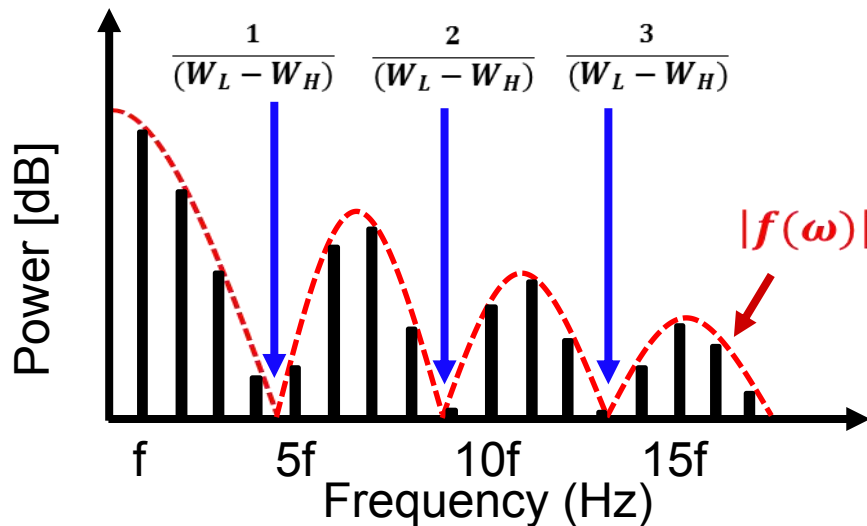
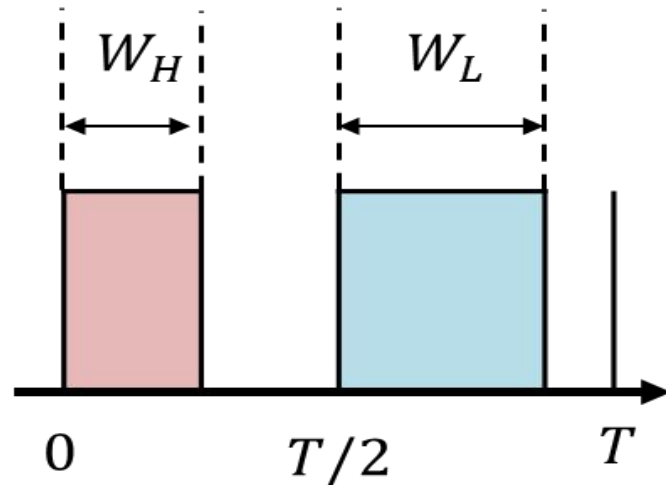
Static ripple is about 0.05% of the output voltage  $V_o$

stable



Transient response with  $F_{in}$  change in  $N=3$  situation

# Expression Analysis of Coding Waveform



$$\begin{aligned}
 f(\omega) &= \int_{-\infty}^{\infty} f(t)e^{-j\omega t} dt \\
 &= \int_0^{W_H} e^{-j\omega t} dt + \int_{T/2}^{W_L+T/2} e^{-j\omega t} dt \\
 &= -\frac{1}{j\omega} \{ \cos(\omega W_H) - j\sin(\omega W_H) \\
 &\quad - \cos(\omega W_L) + j\sin(\omega W_L) \}
 \end{aligned}$$


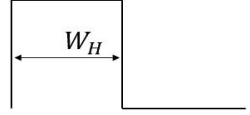
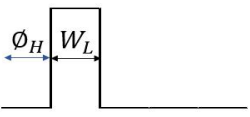
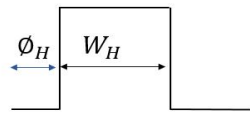
$$|f(\omega)| = \frac{1}{\omega} \sqrt{2 - 2\cos(\omega W_H - \omega W_L)}$$

↓ From the double theorem

$$\begin{aligned}
 &= \frac{1}{\omega} \sqrt{4\sin^2\{(\omega W_L - \omega W_H)/2\}} \\
 &= \frac{(W_L - W_H) \left| \sin\left\{\frac{\omega}{2}(W_L - W_H)\right\} \right|}{\frac{\omega}{2}(W_L - W_H)} \\
 &= (W_L - W_H) \left| \text{sinc}\left\{\frac{\omega}{2}(W_L - W_H)\right\} \right|
 \end{aligned}$$

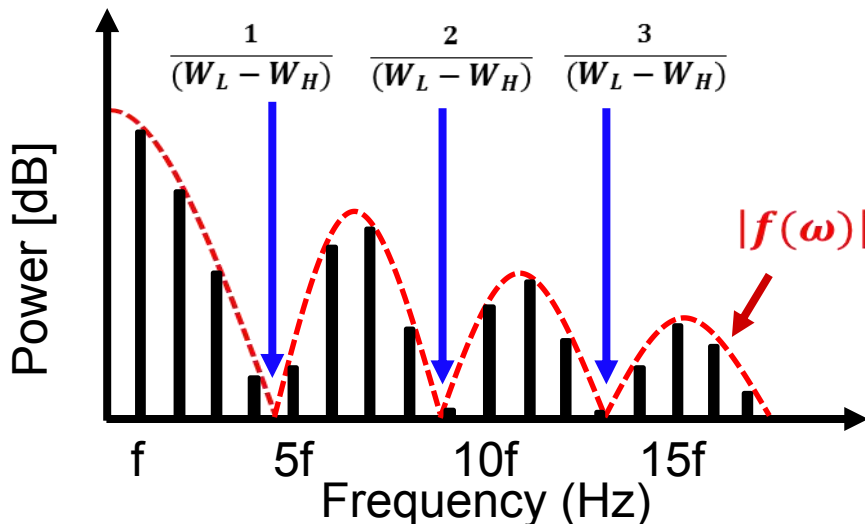
$$f_{notch} \cong N \times \frac{1}{(W_H - W_L)}$$

# Expression Analysis of Coding Waveform

PPC \ PWC	$W_L$	$W_H$
$\phi_L$ (= 0)		
$\phi_H$		

$$\begin{aligned}
 f(\omega) &= \int_{-\infty}^{\infty} f(t) e^{-j\omega t} dt \\
 &= \frac{1}{\omega} \{ j\cos(\omega(\tau_H - \tau_L)) + \sin(\omega(\tau_H - \tau_L)) \\
 &\quad - j\cos(\omega(\tau_H - \tau_L - W)) - \sin(\omega(\tau_H - \tau_L - W)) \\
 &\quad - j\cos(\omega(\tau_L - \tau_H)) - \sin(\omega(\tau_L - \tau_H)) \\
 &\quad + j\cos(\omega(\tau_L - \tau_H - W)) + \sin(\omega(\tau_L - \tau_H - W)) \}
 \end{aligned}$$

$$|f(\omega)| = 2|\tau_L - \tau_H| \left| \text{sinc} \left\{ (2|\tau_L - \tau_H|) \frac{\omega}{2} \right\} \right| \left| \text{sin} \left\{ W \frac{\omega}{2} \right\} \right|$$



$$f_{notch} \cong N \times \frac{1}{2|\tau_H - \tau_L|}$$



# PWPC Method

## Expression analysis of PWPC method

$$|f(\omega)| = (2|\tau_L - \tau_H|) \left| \text{sinc} \left\{ (2|\tau_L - \tau_H|) \frac{\omega}{2} \right\} \right| \left| \sin \left\{ (W_L - W_H) \frac{\omega}{2} \right\} \right|$$

Let  $W_2 - W_1 = 2|\tau_L - \tau_H|$

$$|f(\omega)| = \frac{\sin^2 \left( \frac{\omega}{2} (W_L - W_H) \right)}{\omega/2}$$

The square of *sin*

©Condition

$$W_L = 7\mu\text{s}$$

$$W_H = 3\mu\text{s}$$

