

# Automatic Correction of Current Imbalance due to Element Variations in Multi-Phase Ripple Controlled Converter

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# Research Objective

## Objective

- Development of power supply with
- Automatic correction of current imbalance  
Due to element variations(L or C)
  - Fast response
  - Low output voltage ripple control

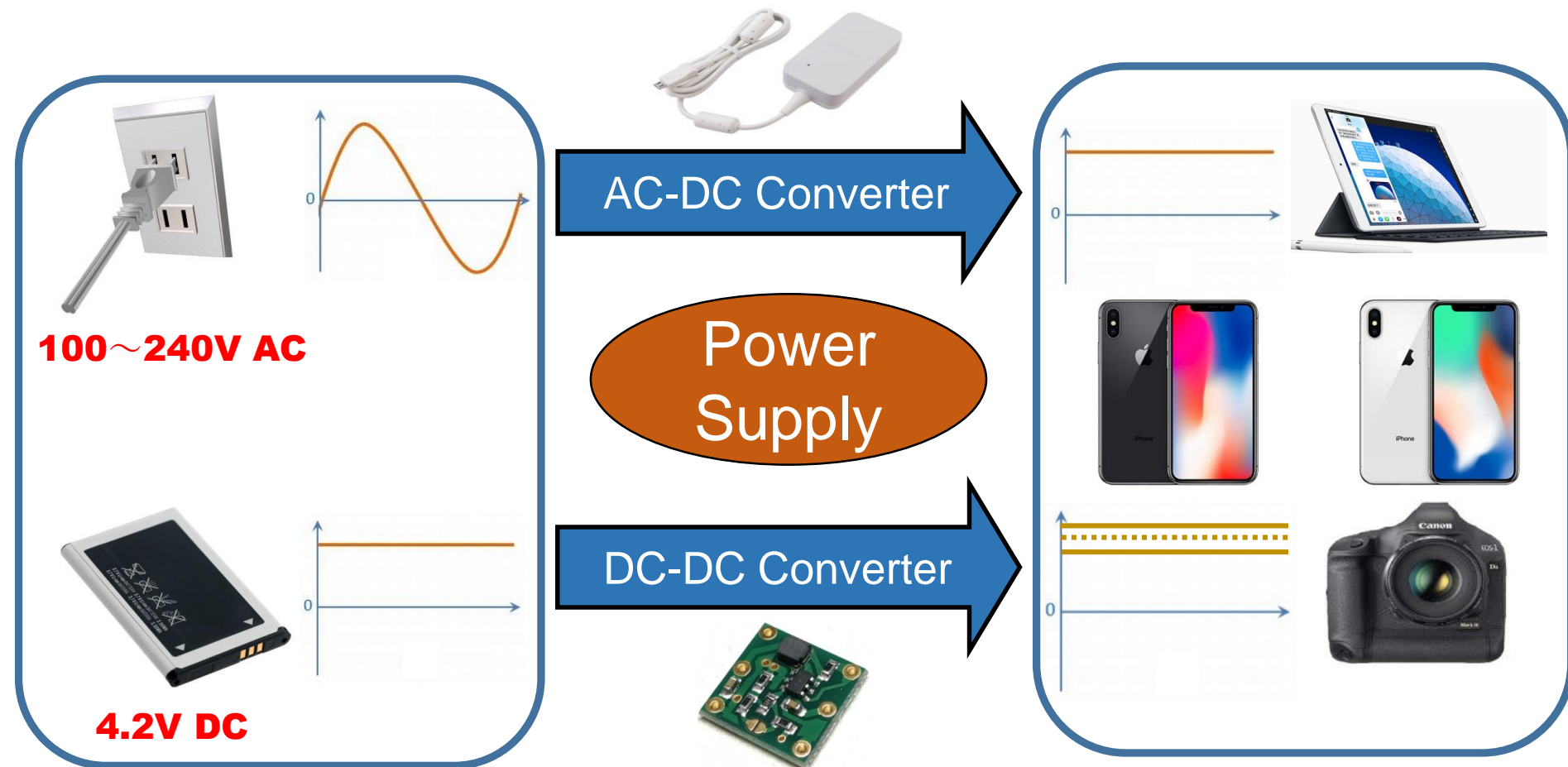
## Approach

- Constant on-time control method
- Multi-phase converter

- Research background
- Constant on-time control
- Four-phase converter solution  
via saw-tooth wave circuit
- Simulation results
- Automatic correction technology  
for balance of element variation
- Conclusion

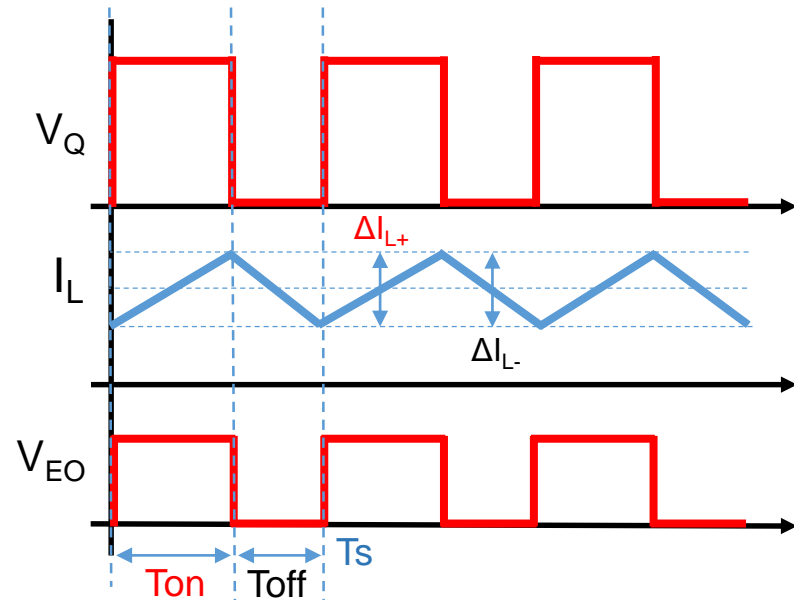
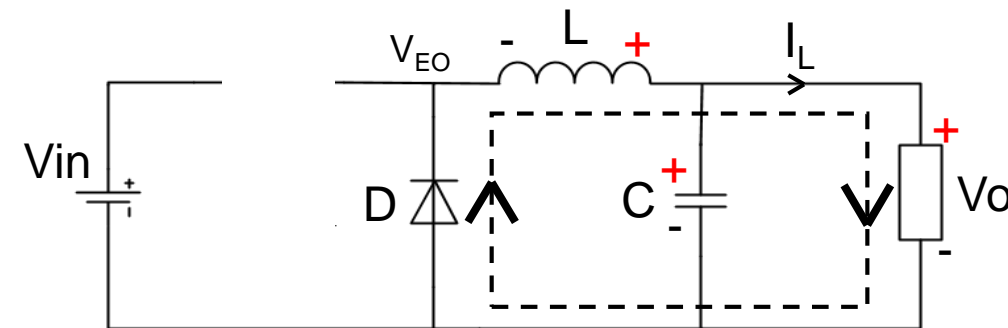
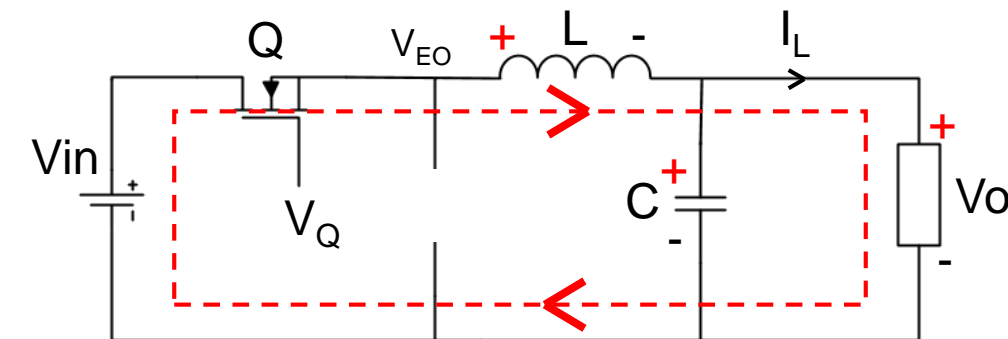
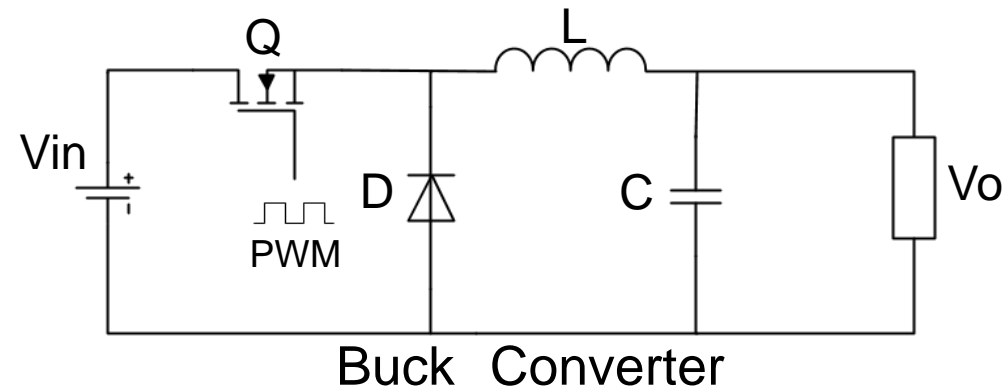
- **Research background**
- Constant on-time control
- Four-phase converter solution via saw-tooth wave circuit
- Simulation result
- Automatic correction technology for balance of element variation
- Conclusion

# Power Supplies Prevail Everywhere



Power supply → demanded everywhere  
to provide appropriate voltage for electronic device

# Operation of Buck Converter



**On State**

$$V_{L\text{on}} = V_{\text{in}} - V_{\text{o}} = L \cdot (\Delta i_{L+} / \Delta t_{\text{on}})$$

**Off State**

$$V_{L\text{off}} = -V_{\text{o}} = L \cdot (\Delta i_{L-} / \Delta t_{\text{off}})$$

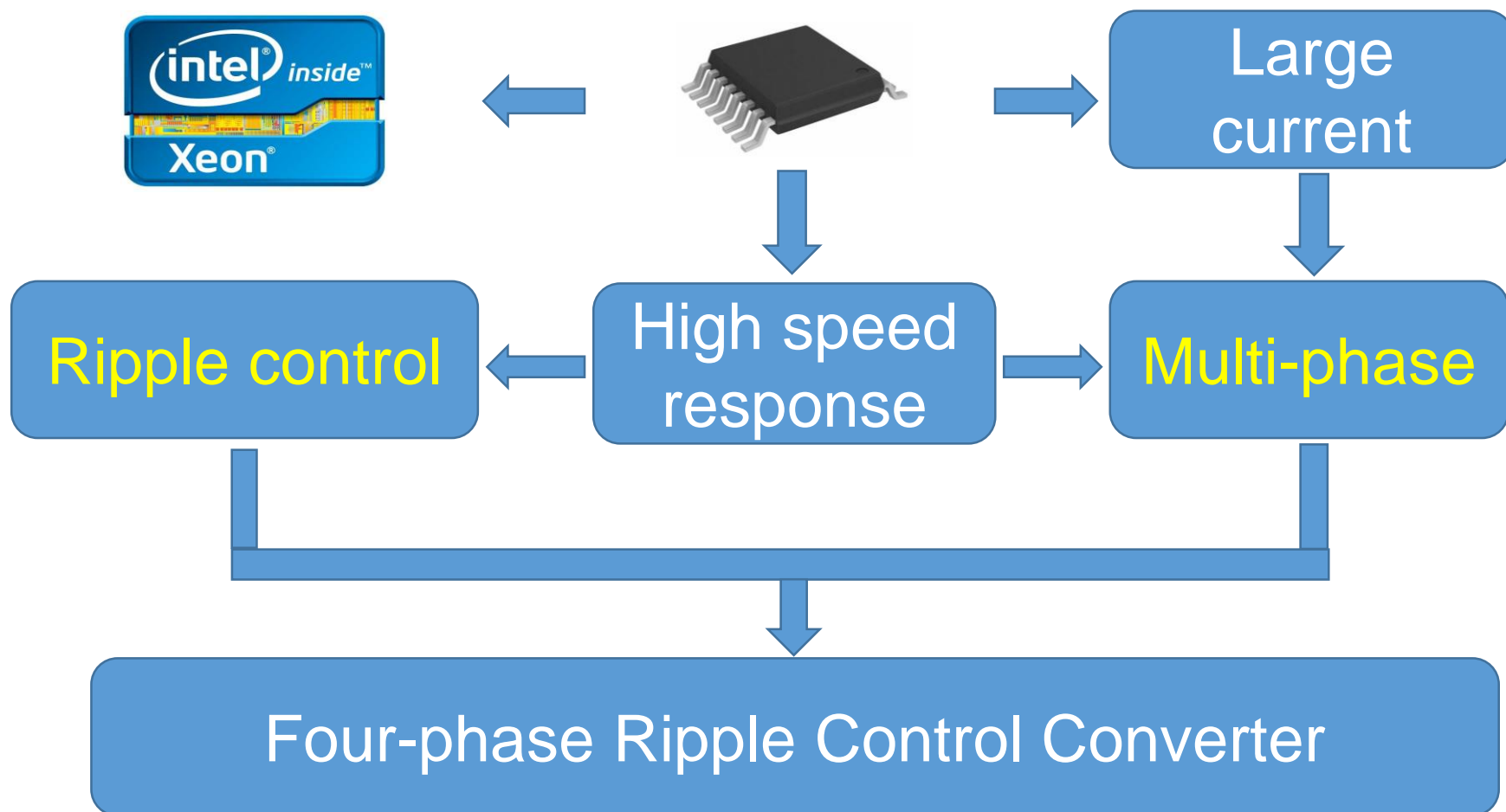
**Volt-second  
balance**

$$\Delta i_{L+} = \Delta i_{L-}$$

$$V_{\text{o}} = V_{\text{in}} \frac{T_{\text{on}}}{T_{\text{s}}}$$

# Demand for Power Supply of Process

DC input	DC output	Max. output current	Max. output current step	Max. output current slew rate
12V	1.5V	120A	100A/us	930A/us

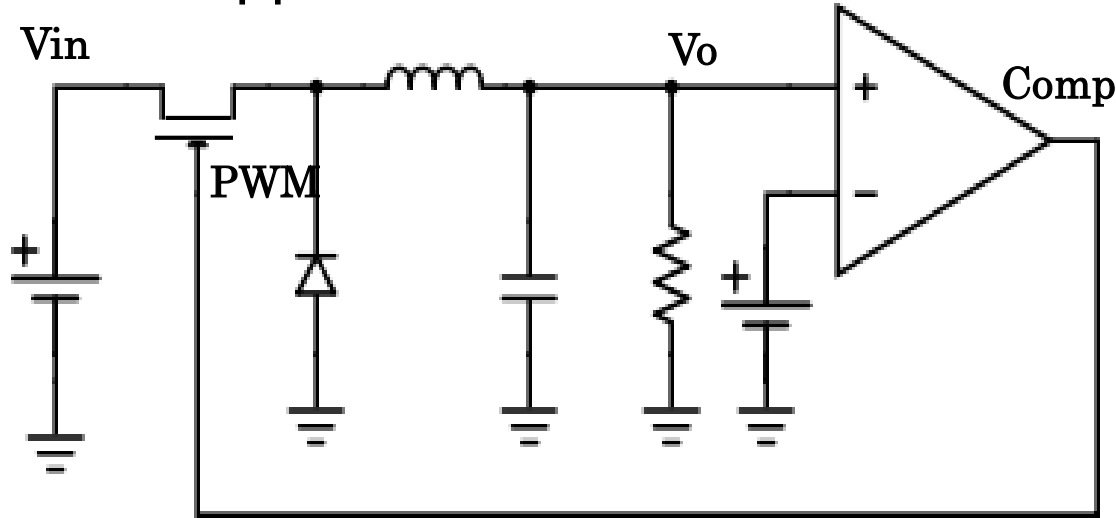


- Research background
- **Constant on-time control**
- Four-phase converter solution
  - via saw-tooth wave circuit
- Simulation result
- Automatic correction technology
  - for balance of element variation
- Conclusion



# Ripple Control Converter

## Basic Ripple Control Converter



No fixed  
clock signal



### Merit:

- ① High-speed response
- ② Easy to obtain high frequency
- ③ No Op-Amp



### Demerit:

- ① Operation frequency is changed by the load current transient.
- ② Large noise



$F_{op} \doteq \text{constant}$

Low frequency

Stable operating frequency



Constant on-time  
control method

# Ripple Control with Constant on-time Method

## Ripple Control

Hysteresis window control

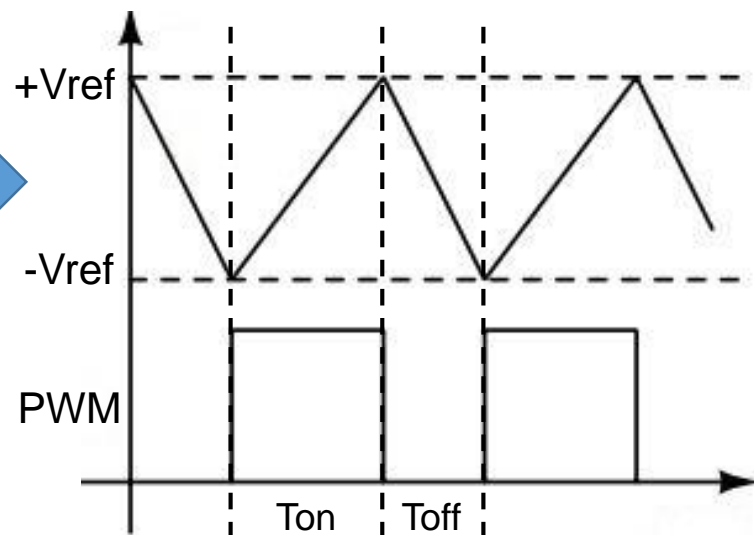
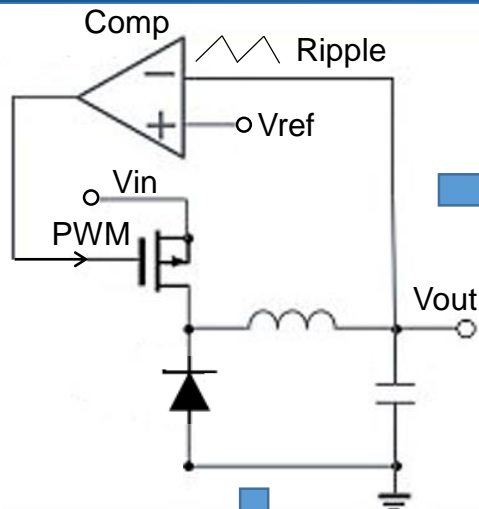


Extreme fast response



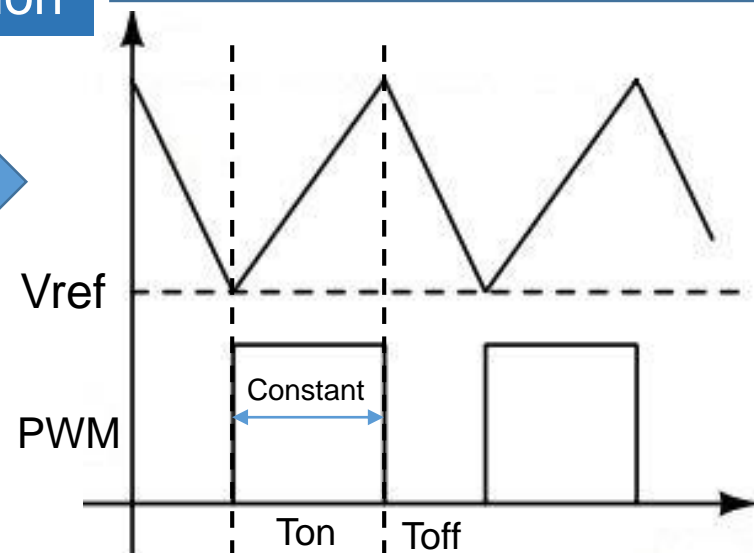
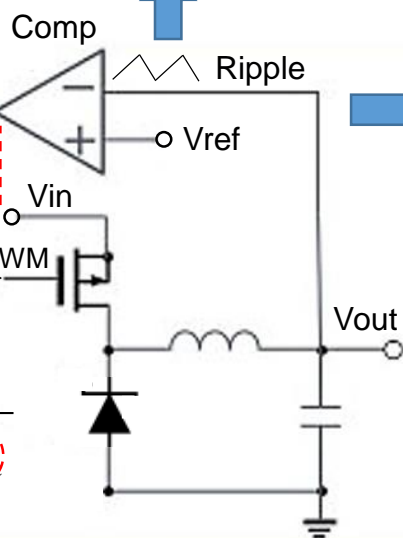
Constant on-time control

$$V_{out} = V_{in} \frac{T_{on}}{T_s}$$
$$f_s = \frac{1}{T_s} \Rightarrow f_s = \frac{V_{out}}{V_{in} \cdot T_{on}}$$



Frequency swings usually

No phase compensation

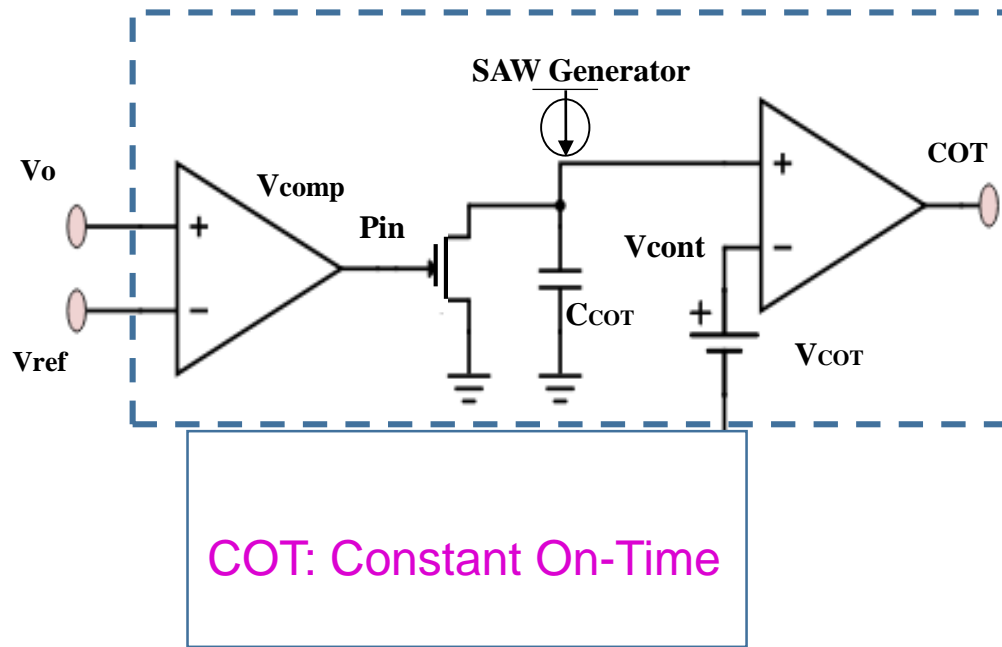


Frequency keeps stable

# Operation of Proposed COT Generator

## Proposed COT Converter

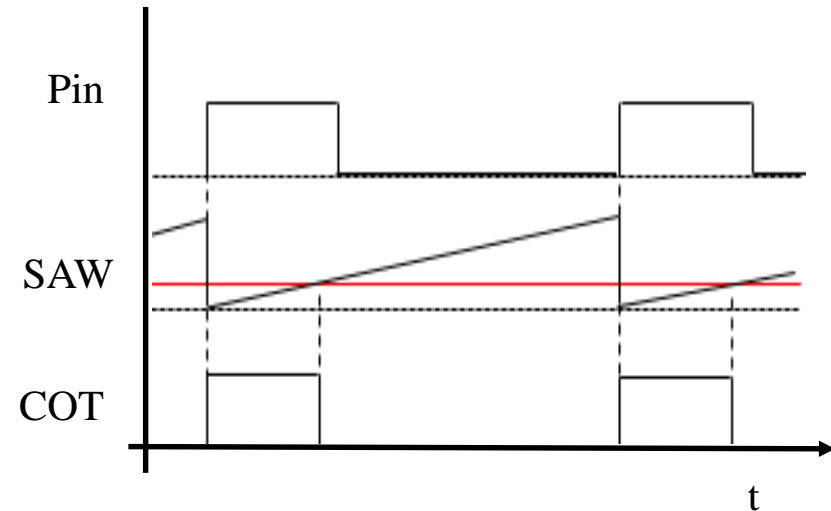
COT Generator of sub-converter



COT: Constant On-Time

No External Clock

Operation waveform



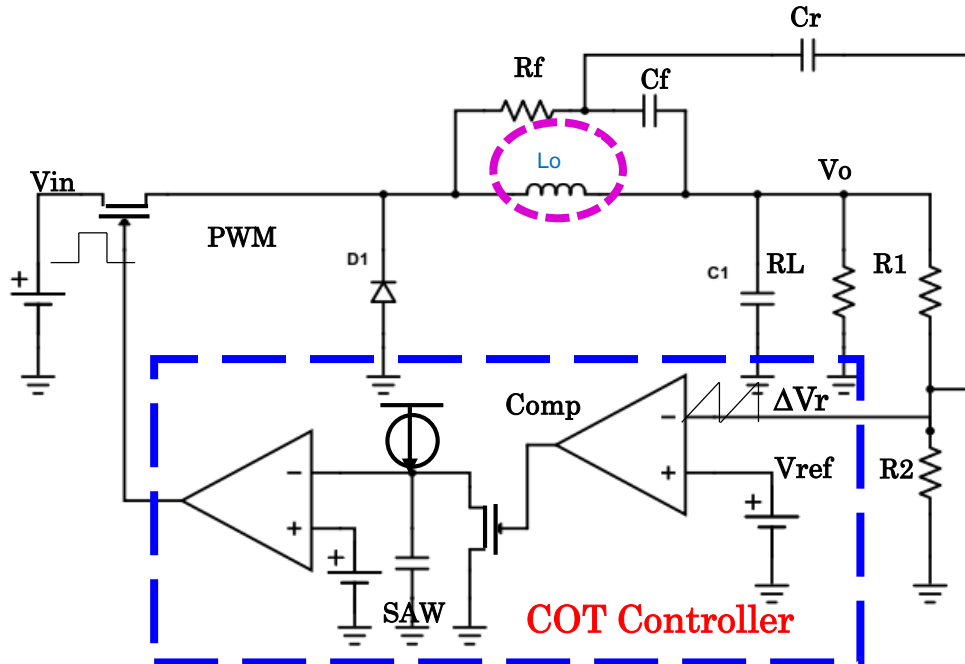
SAW signal generator with  $V_{cont}$

- ①  $P_{in}$  is supplied from the comparator
- ② Positive edge resets and restarts SAW generator
- ③ Gradient is decided with  $I_o$  and  $C_{COT}$
- ④ COT pulse is generated by comparing SAW signal and  $V_{cont}$ .

- Research background
- Constant on-time control
- **Four-phase converter solution  
via saw-tooth wave circuit**
- Simulation result
- Transfer function characteristics
- EMI reduction via pulse phase modulation
- Conclusion

# Single-Phase Converter

## Ripple injection method

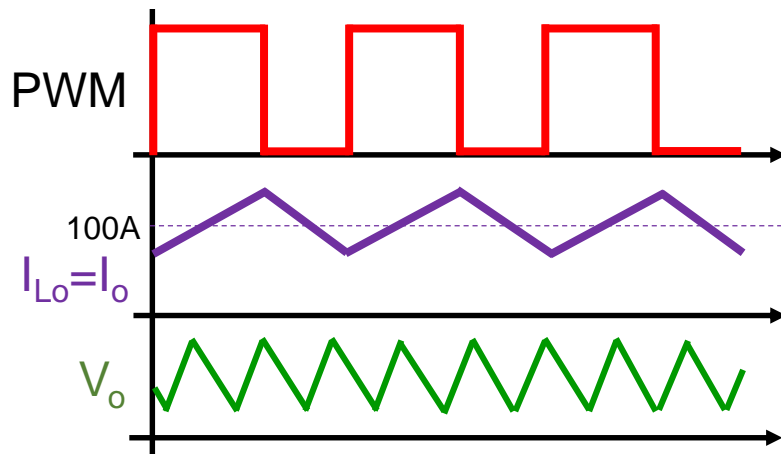


$I_o$  flows  
only through inductor  $L_o$



$L_o$  large

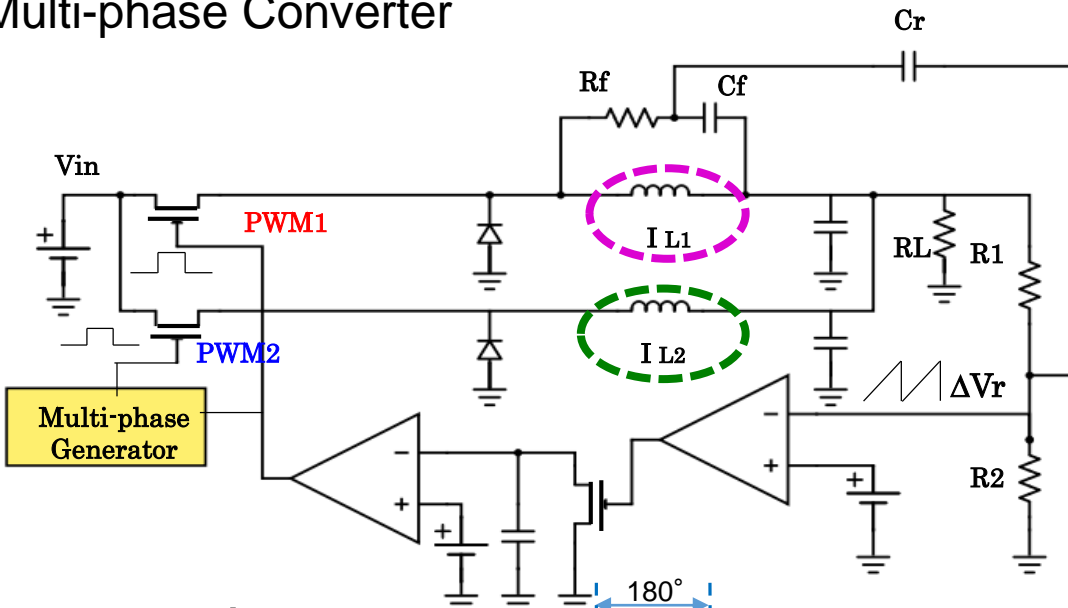
body of coil is large



Large load  
on inductor  $L_o$

# Merit of Multi-Phase Converter

## Multi-phase Converter

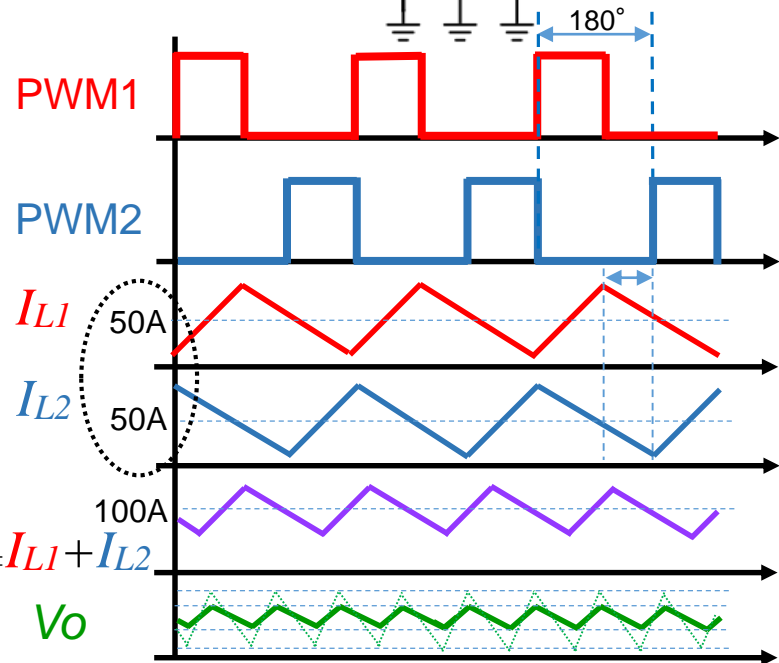


Tracking PWM2 with PWM1 without clock demand

Inductor L1 and L2 will go shares with Io



L1 and L2 small



180° phase difference

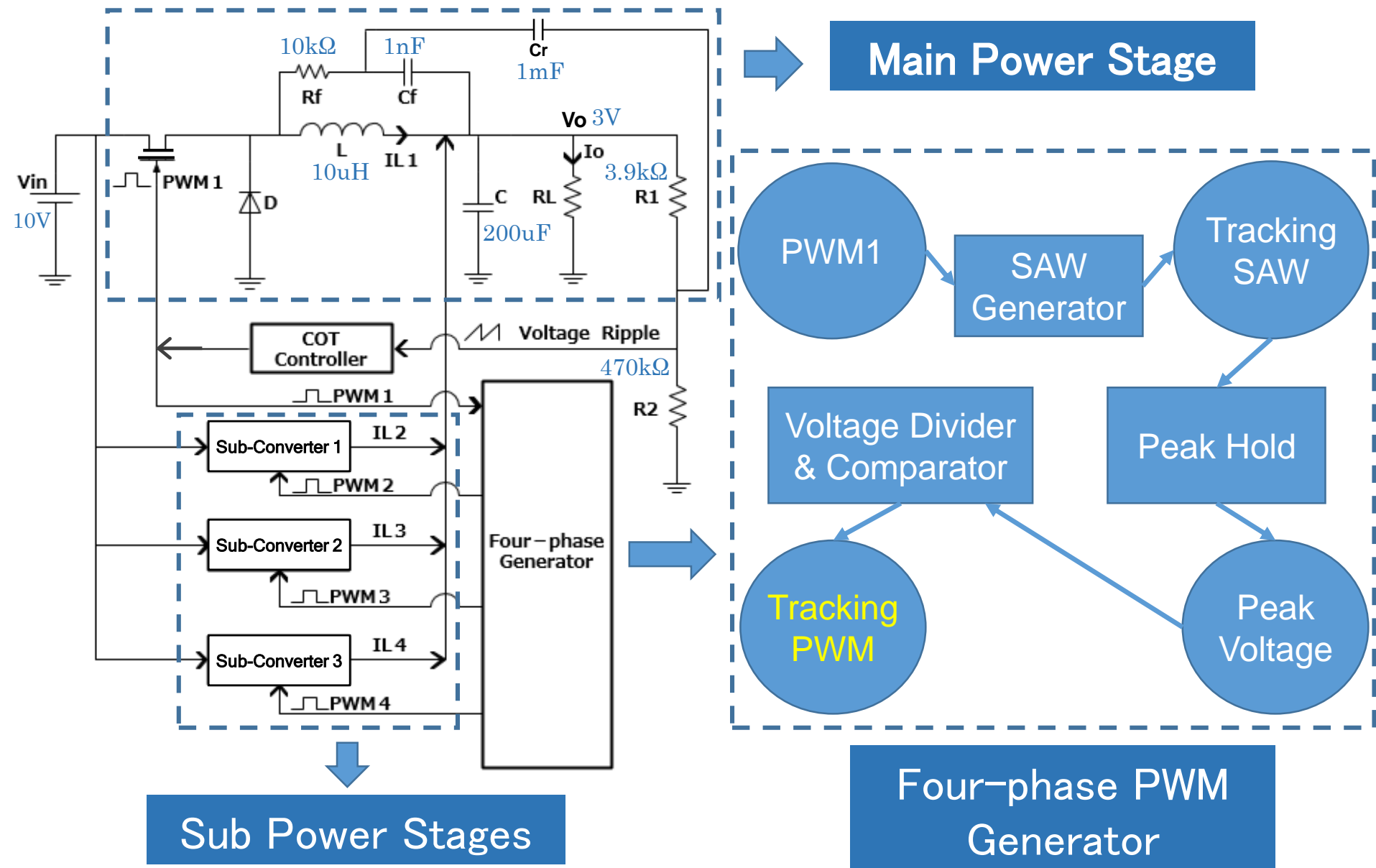
Load of each phase's inductor halved

Simulative frequency multiplication

Low ripple by shifted two-phase peak current

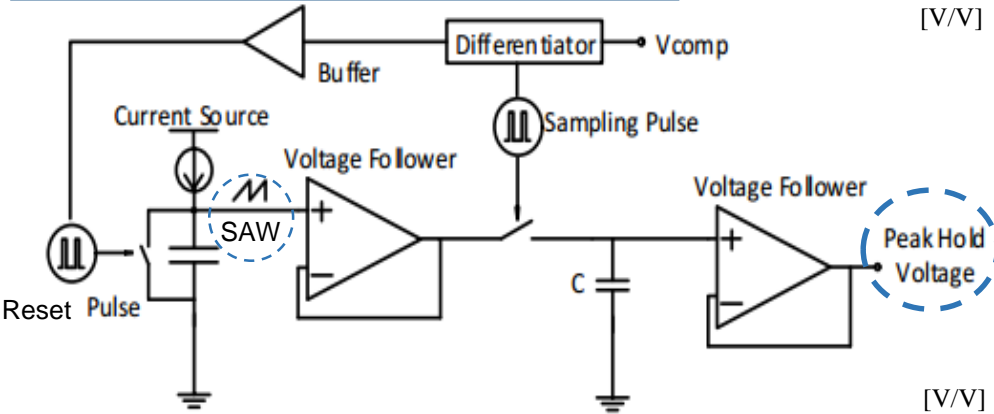
- \* Small body size, L1, L2
- \* High speed response
- \* Smaller output ripple

# Proposed Four-Phase Converter Solution

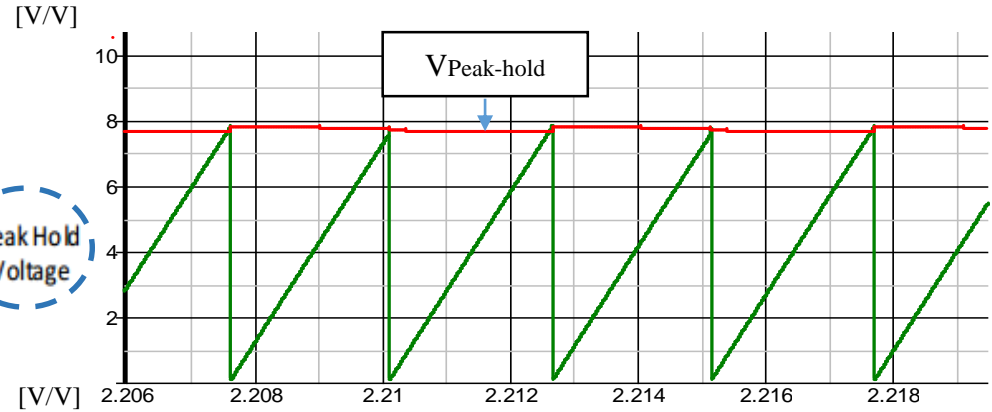


# Generation of Four-Phase PWM

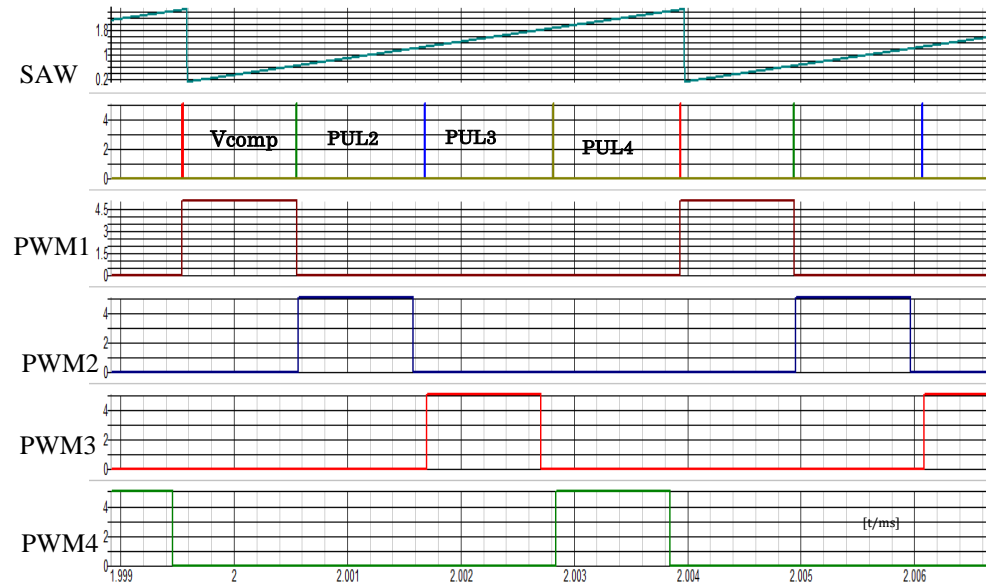
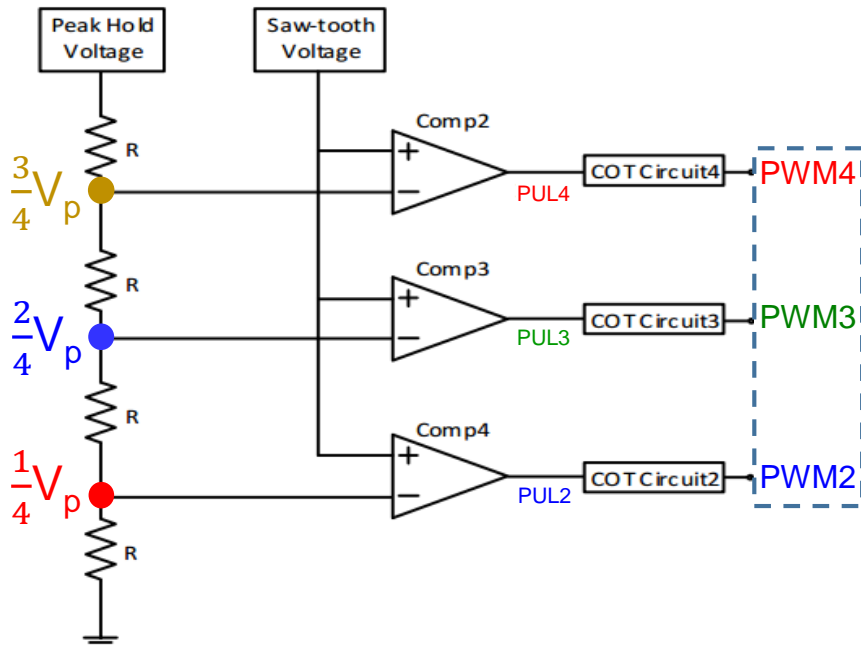
## SAW Generator & Peak Hold



## Operation waveform



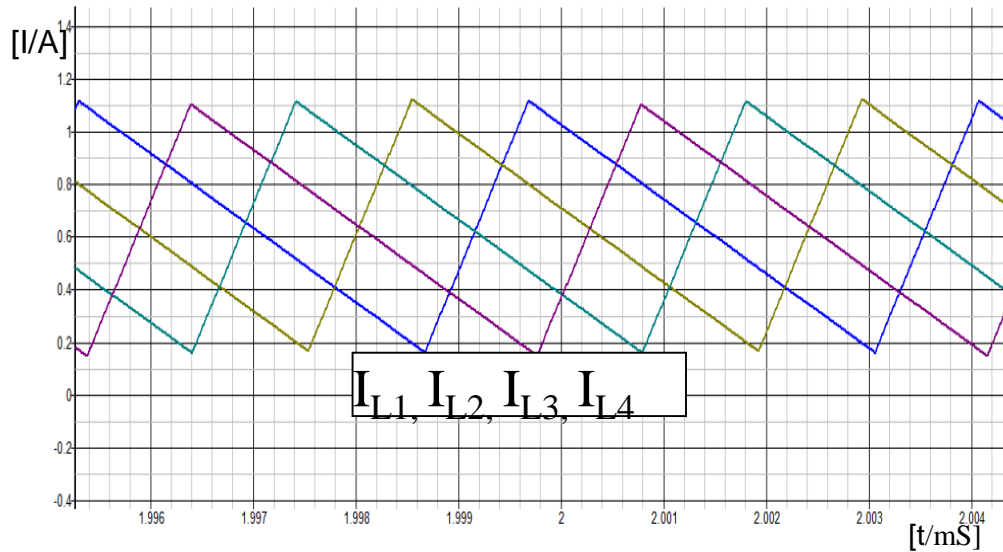
## Voltage Divider & Comparator





# Current Balance of four-phase Converter

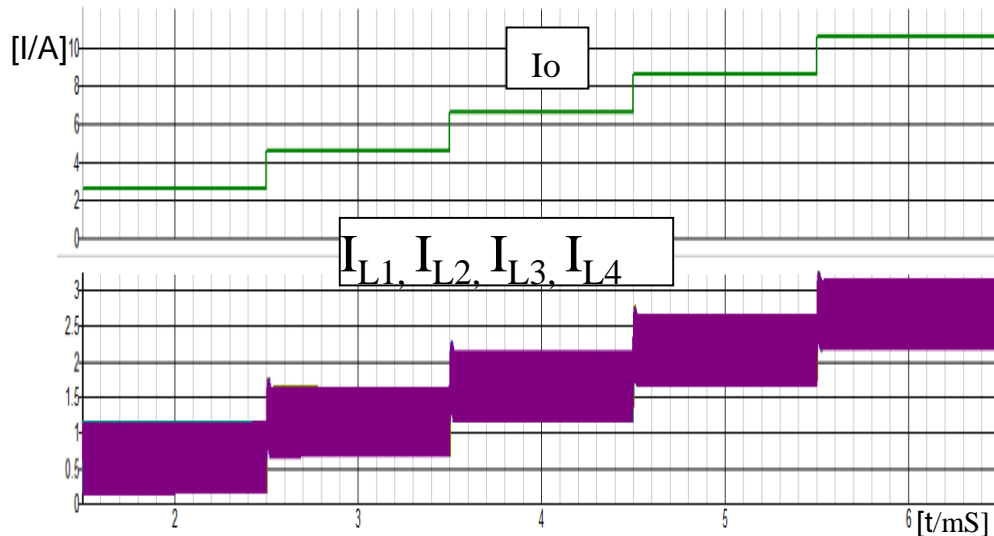
## ★ Simulation Result



Without element variations  
 $\Delta L$ ,  $\Delta T_{\text{cot}} (= \Delta C)$ ,  $\Delta V_{\text{S/H}}$



Good current balance



Large load current achieved



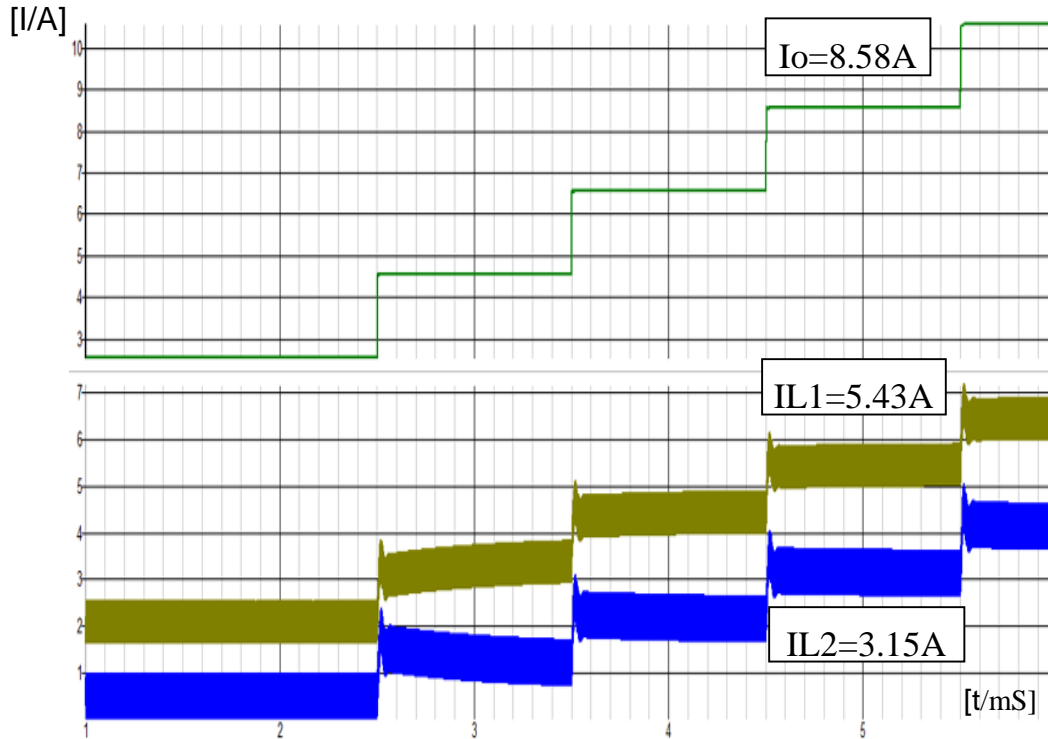
Good current balance  
 during transient response

- Research background
- Constant on-time control
- Four-phase converter solution  
via saw-tooth wave circuit
- **Automatic correction technology  
for balance of element variation**
- Conclusion

# Imbalance current (Inductance variation)

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● **Two Phase:** With element variation (Inductance)



**Imbalance result for two-phase current**



10 $\mu$ H  $\rightarrow$  11 $\mu$ H

+ 10%

Inductor

Main power supply

$$I_o = 8.58A$$

$$I_{L1} = 5.43A, I_{L2} = 3.15A$$

$$\begin{aligned} \Delta I_L &= (I_{L1} - I_{L2}) \\ &= |5.43 - 3.15| = 2.28A \end{aligned}$$

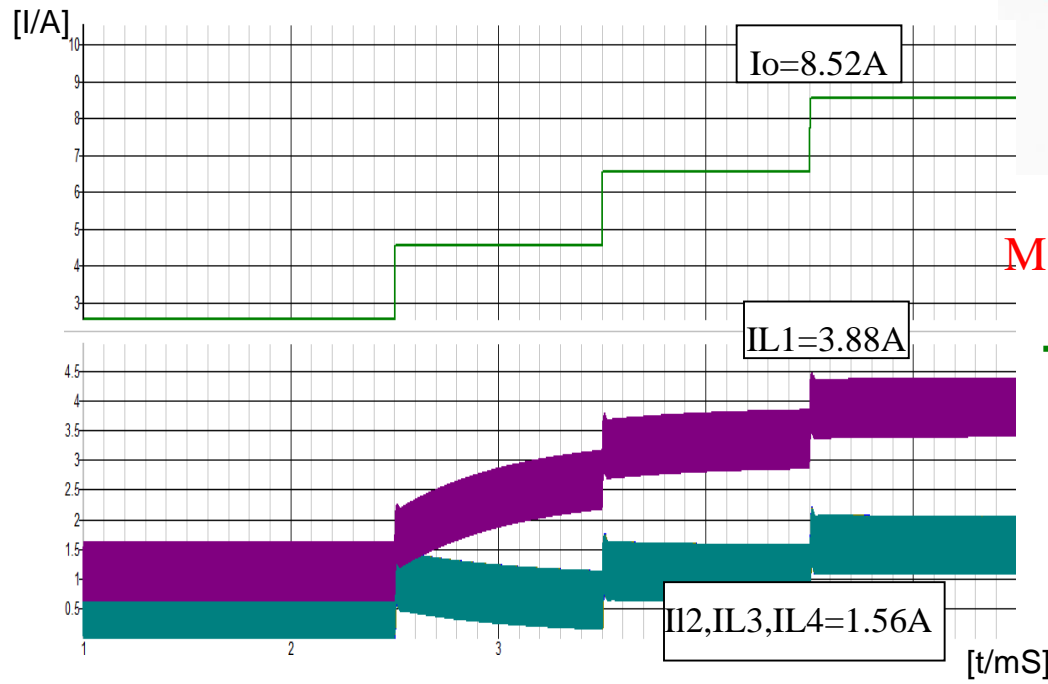
**Error Ratio:**

$$\begin{aligned} \delta &= (I_o/2 - I_n)/I_o/2 \\ &= (4.29 - 3.15)/4.29 \Rightarrow 27\% \end{aligned}$$



# Imbalance current(Capacitance variation)

● **Four Phase:** With element variation (Capacitance in COT generator)



500pF → 495pF  
- 1%  
Capacitance  
Main power supply  
High Sensitivity

**Imbalance result for four-phase current**

$$I_o = 8.52A$$

$$I_{L1} = 3.88A ,$$

$$I_{L2} = I_{L3} = I_{L4} = 1.56A$$

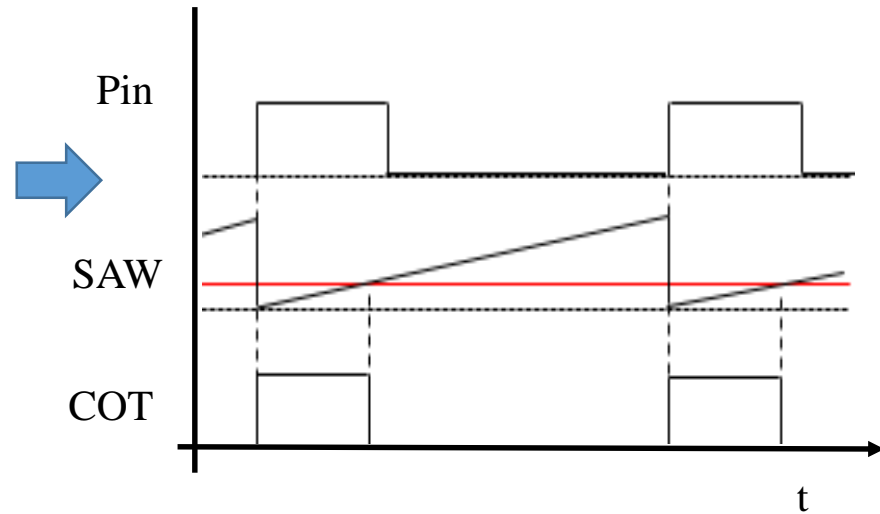
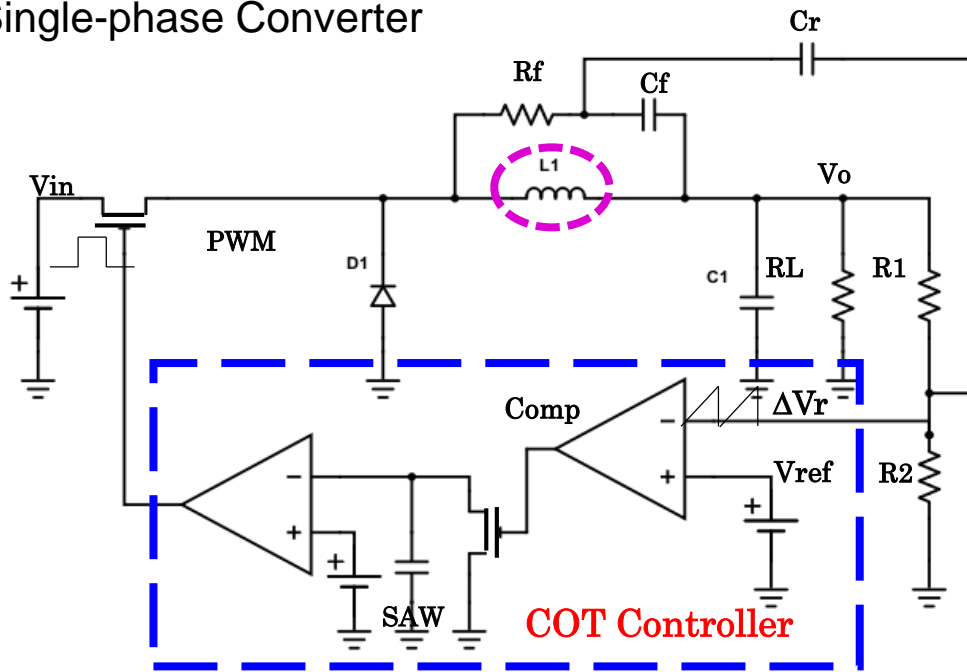
$$\delta 1 = (3.88 - 2.31) / 2.13 \Rightarrow 82\%$$

$$\delta 2 = (2.13 - 1.56) / 2.13 \Rightarrow 27\%$$

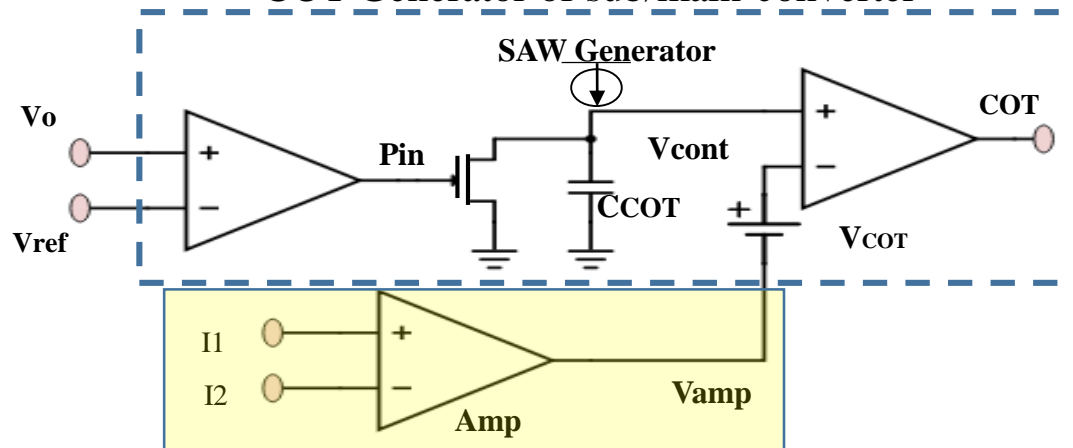


# Proposed Current Balance Modulation

## Single-phase Converter



## COT Generator of sub/main-converter



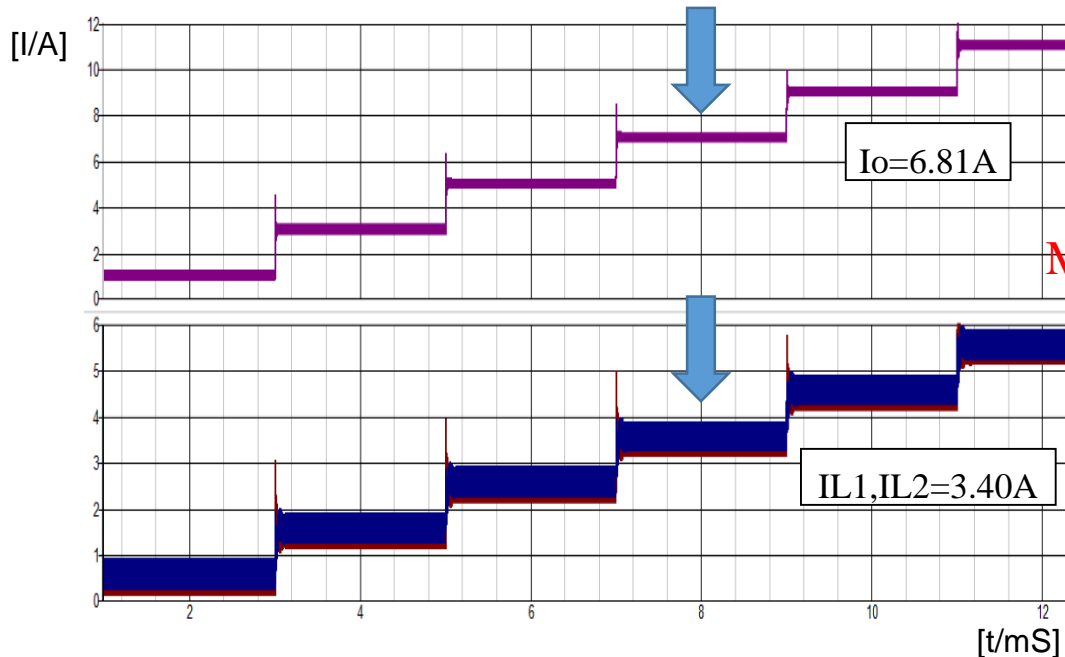
$$\begin{aligned} T_{COT} &= k \cdot V^- \\ &= k \cdot (V_{COT} + V_{amp}) \\ &= T_{COT} + \Delta T_{COT} \end{aligned}$$

## Modulation Ratio:

$$\begin{aligned} \alpha &= \Delta T_{COT} / T_{COT} \\ &= V_{amp} / V_{COT} \end{aligned}$$

# Balance current (Inductance variation)

- **Two Phase** : Result of **proposed method** with good current balance



Inductor

$10\mu\text{H} \rightarrow 11\mu\text{H}$

Main power supply

+ 10%

Good current balance

$I_o = 6.81\text{A}$

$I_{L1} = I_{L2} = 3.40\text{A}$

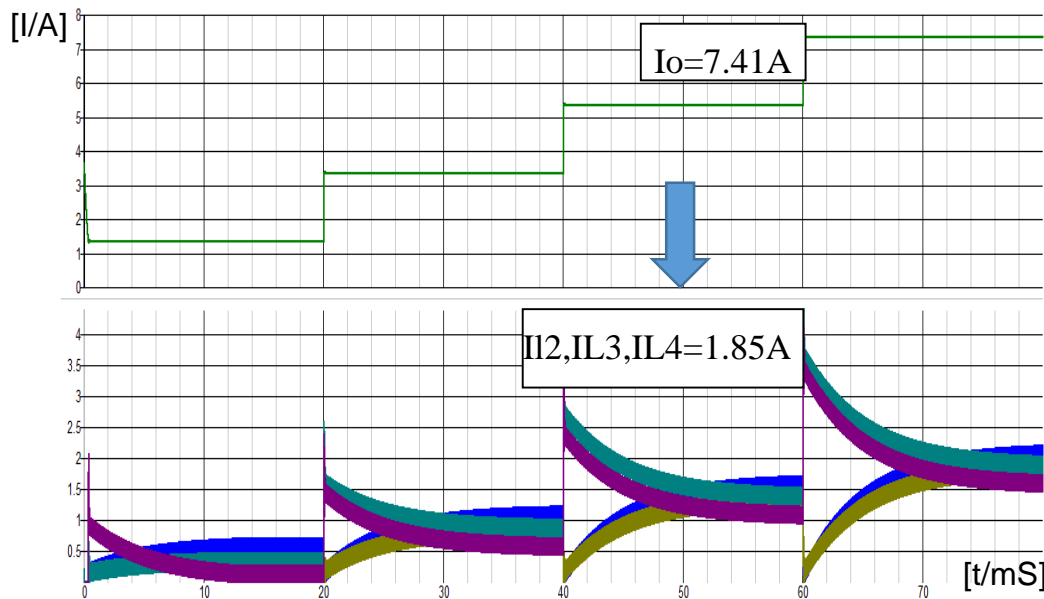
Balance result for  
two-phase current



- ★ Even if capacitance varies,  
the current balance can be secured in the same way

# Balance current (Capacitance variation)

- **Four Phase:** Result of **proposed method** with good current balance



**Balance result for four-phase current**



500pF → 495pF

Capacitance - 1%

Main power supply

**Good current balance**

$$I_o = 7.41A$$

$$I_{L1} \doteq I_{L2} \doteq I_{L3} \doteq I_{L4} \doteq 1.85A$$



## Merits of Proposed Method

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- When L or C for COT pulse is varied, inductor current of each sub-converter is automatically kept in good balance.
- There is no need to select L and C values, so the cost is reduced.
- Even if L or C values change due to temperature change, the current balance can be automatically maintained by the proposed system.



# Conclusion

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- The current imbalance due to inductance and capacitor variations is well improved.
- Current balance is very good even at large output current.

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Thank you for your attention

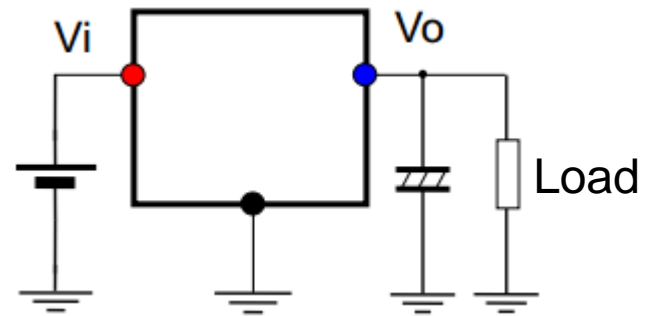
# Q&A

- Q1: Is the automatic current balancing technique for ripple-controlled power supplies suitable for conventional four-phase buck converter power supplies?
- A1: I have never thought of it before, but I think it is applicable.
- Q2: Can the correction be made even if the current of each phase varies due to the variation in the conduction resistance of the switch?
- A2: Whatever the reason, the current balance correction can be performed using the proposed technology if the current in each phase varies.
- Q3: How did you determine the gain of the current sense amplifier?
- A3: The negative feedback control can suppress the current variation to  $(1 / \text{loop gain})$ . Even if the loop gain is made quite large, it is easy to keep stable, so we determined the value of gain by experiments.

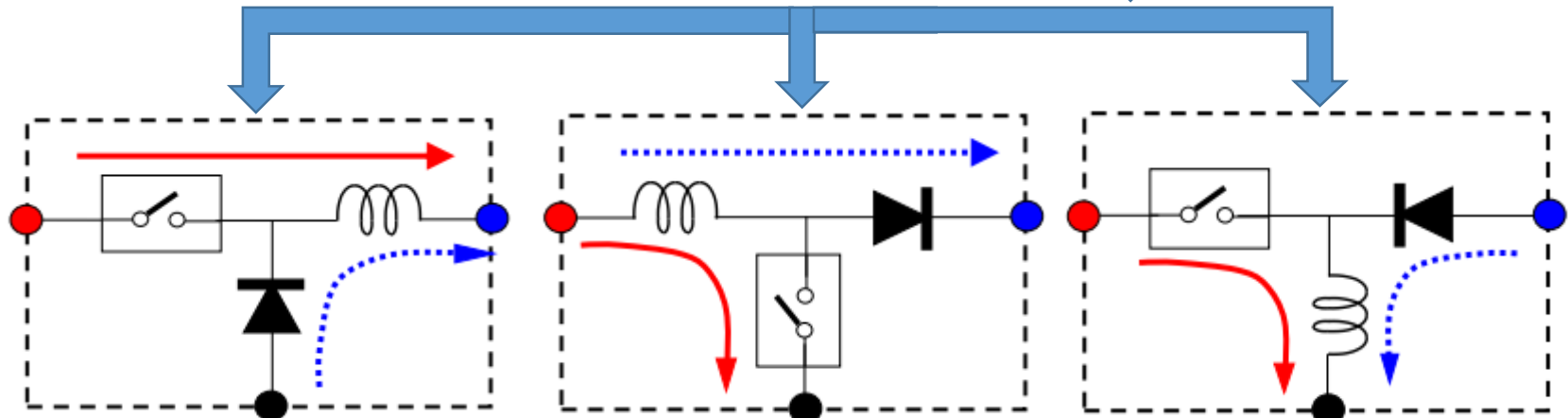
# Classifications of DC-DC Converter



DC-DC converter



Basic configuration



Buck

$$V_{in} > V_o$$

Boost

$$V_{in} < V_o$$

Buck-Boost

$$V_{in} \approx V_o$$