



Flat Pass-Band Method with Two RC Band-Stop Filters for 4-Stage Passive RC Polyphase Filter in Low-IF Receiver Systems

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Outline

1. Research Background

- Applications of RC Poly-phase Network
- Analog Complex Signal Processing Concepts

2. Analysis of 4-Stage Passive RC Network

- Frequency Responses
- Image Rejection Ratio

3. Proposed Model of 4-Stage Passive RC Network

- Flat pass-band gain with two RC band-stop filters
- Experimental Results

4. Conclusions

1. Research Background

Research Objective & Design Approach

Objective

Design of Image Rejection Filter for **Blue-tooth Receiver**:

- **Low image noise**
- **Simple Model** of RC Network

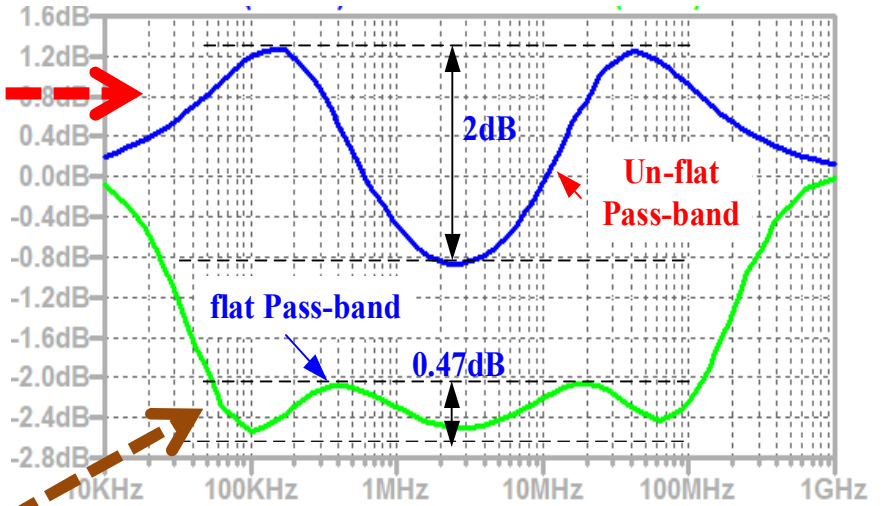
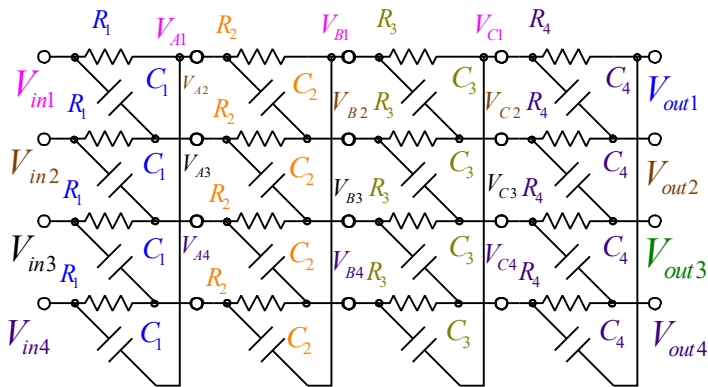
Approach

- **Derivation of transfer function of 4-stage passive rc network based on widened **superposition principle****
- **Mathematical analysis** of transfer function of 4-stage passive RC poly-phase filter
- **Flat pass-band gain** with two RC band-stop filters

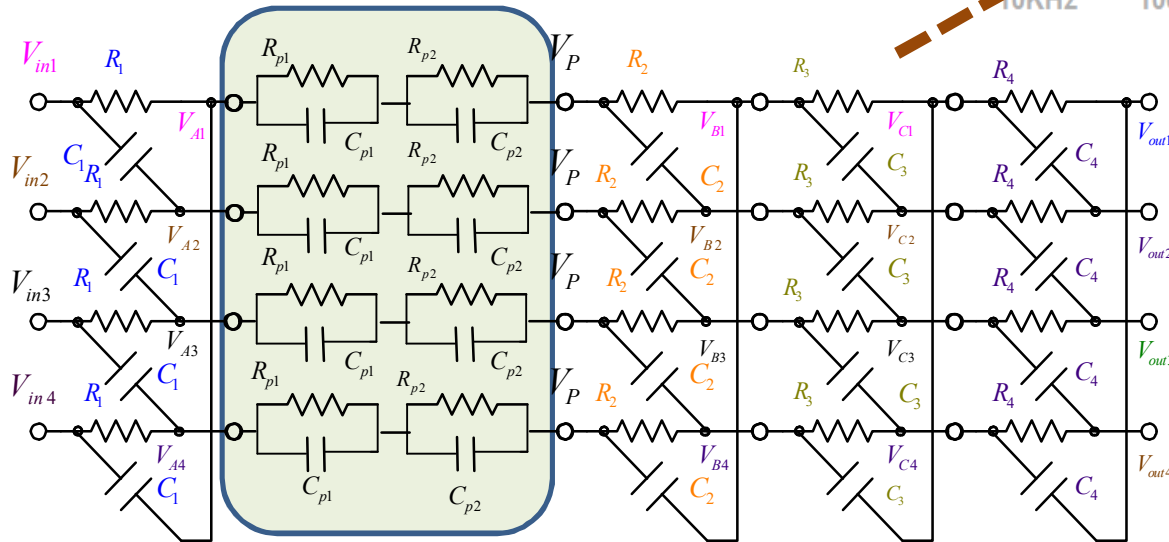
1. Research Background

Design Achievements of This Work

Conventional Design



Proposed Design

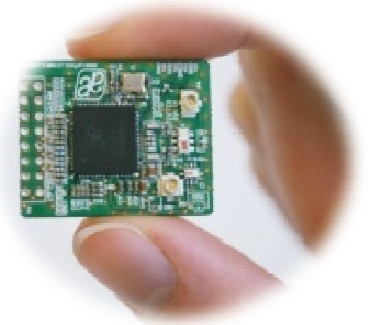
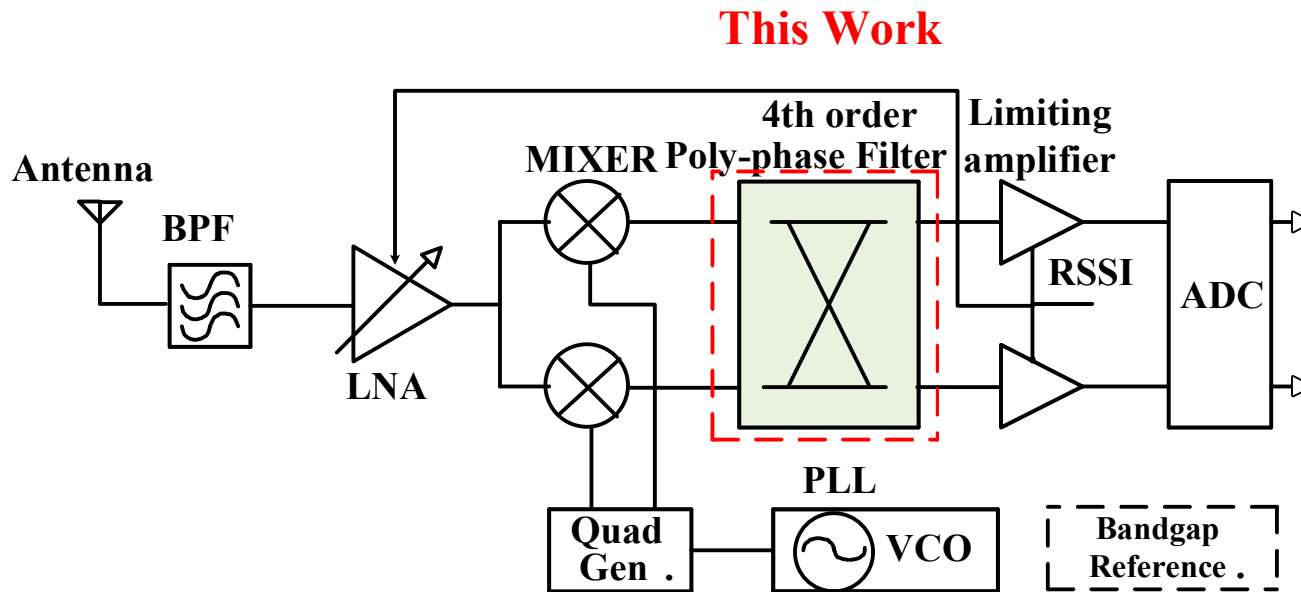


Two RC band-stop filters

Pass-band Gain
Ripple Reduction
from **2dB**
→ **0.47dB**

1. Research Background

Low-IF Receiver System Architecture



Applications:
ZigBee, Bluetooth,
TV Set Top Box ...

Merits



- Low-cost
- Small-size
- High-integration

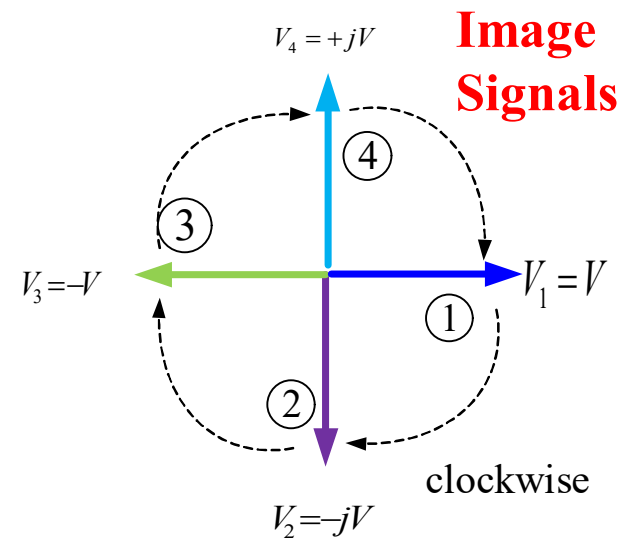
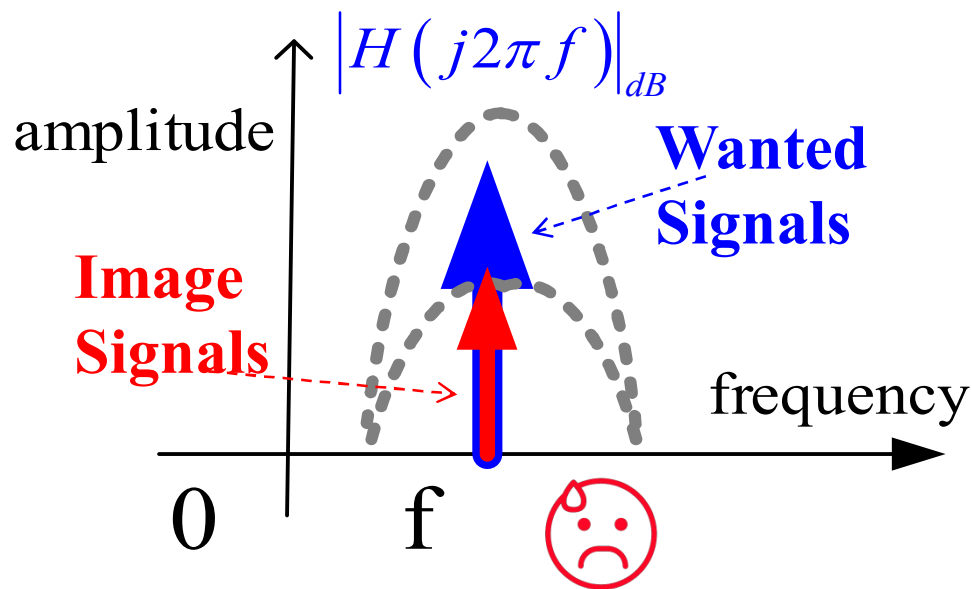
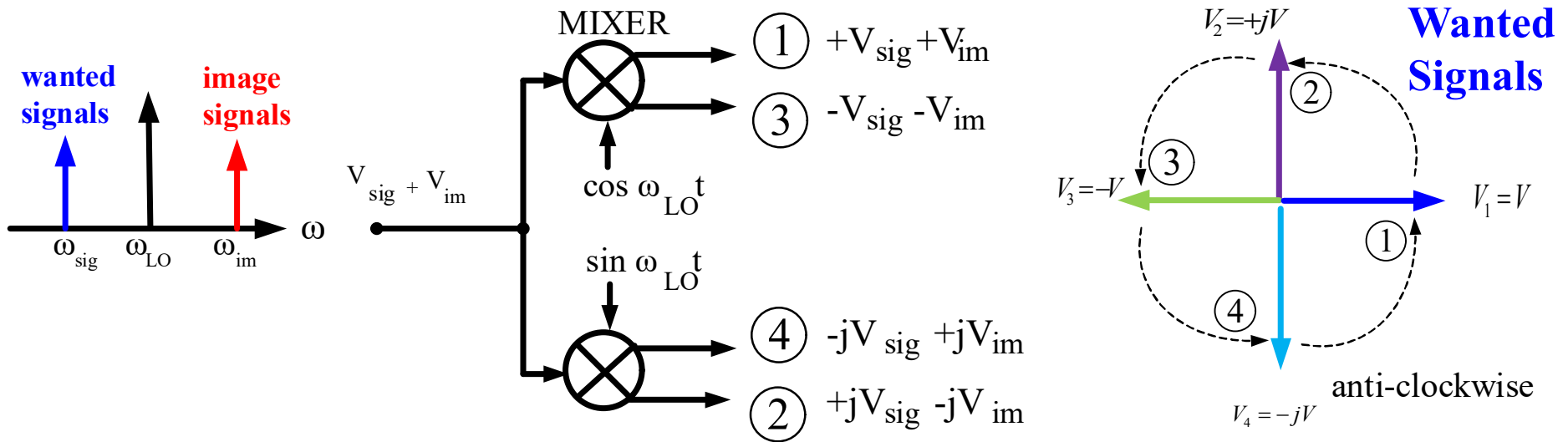
Demerits



- Image Noises
- Power Loss
- Noise Figure

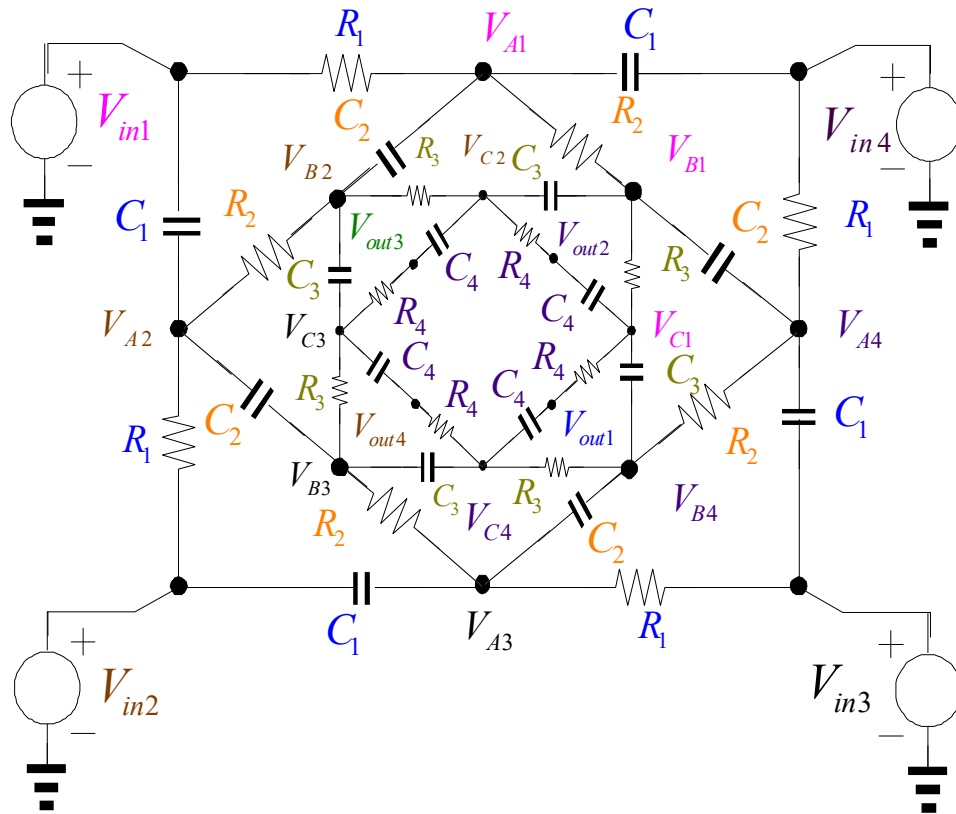
1. Research Background

Frequency Plane of Low-IF Signals



2. Analysis of 4-Stage Passive RC Network

Design of 4-Stage Passive RC Network



| Parameter | PPF |
|----------------------------|----------|
| Input IF frequency | 5MHz |
| Input IF Power | -60dBm |
| NF | 10dB |
| Gain | 0dB |
| Current Consumption | <5mA |
| Supply Voltage | 1.8V |
| Image Rejection Ratio IMRR | < -30 dB |

2. Analysis of 4-Stage Passive RC Network

Definition of Widened Superposition Principle

A superposition of energy at *one place* is proportional with **their input sources and resistance distances of transmission spaces.**

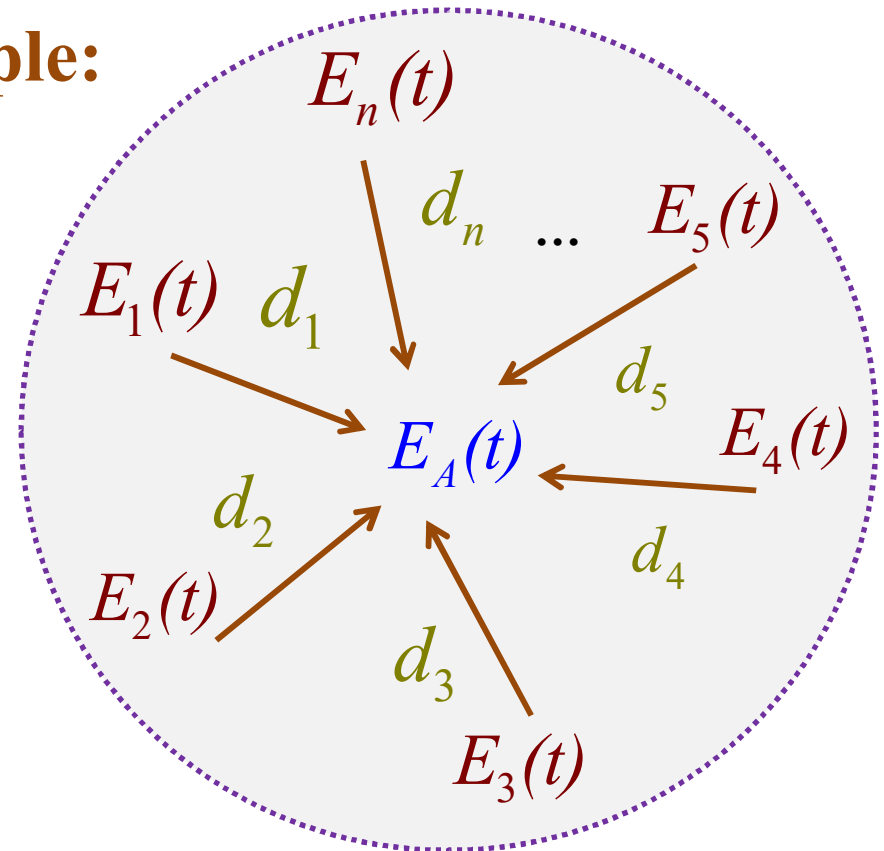
Widened Superposition Principle:

$$E_A(t) \sum_{i=1}^n \frac{1}{d_i} = \sum_{i=1}^n \frac{E_i(t)}{d_i}$$

$E_A(t)$: *energy at one place*

$E_i(t)$: *input sources*

$d_i(t)$: *resistance distances*

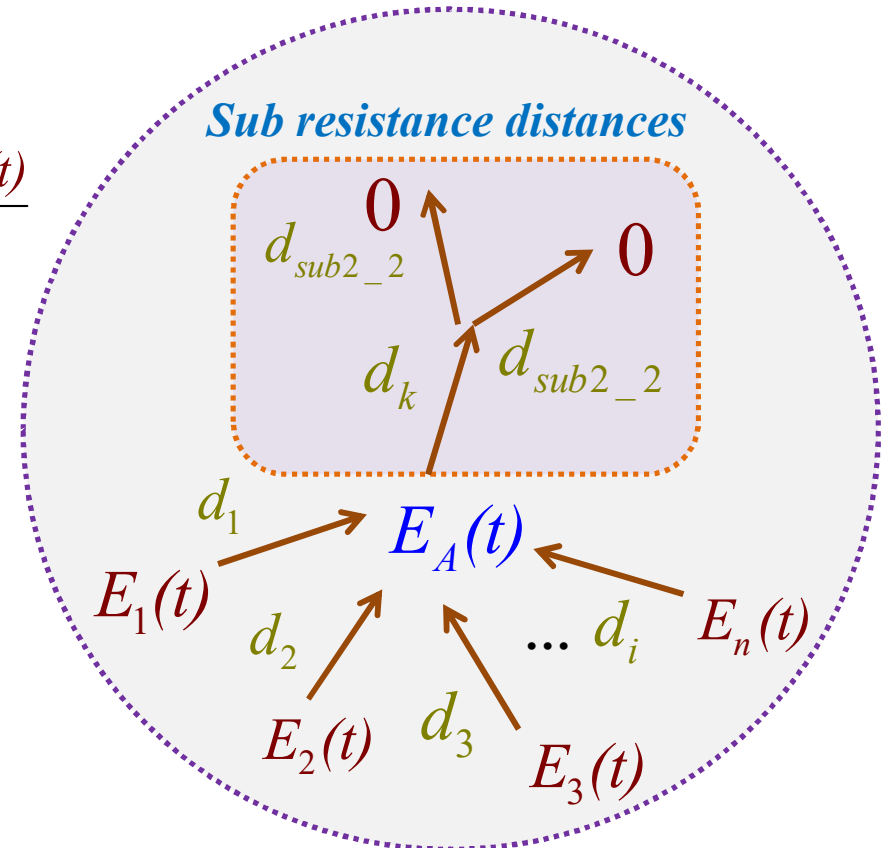


2. Analysis of 4-Stage Passive RC Network

Widened Superposition principle with sub branches

If a resistance distance is *not direct* or *divided into small branches*, an energy at every small place will be calculated by the *direct resistance distances* of every branch.

$$E_A(t) \left(\sum_{i=1}^n \frac{1}{d_i} + \frac{1}{d_k + \frac{1}{\frac{1}{d_{k_sub1}} + \frac{1}{d_{k_sub2}} + \dots}}} \right) = \sum_{i=1}^n \frac{E_i(t)}{d_i}$$



$E_A(t)$: energy at one place

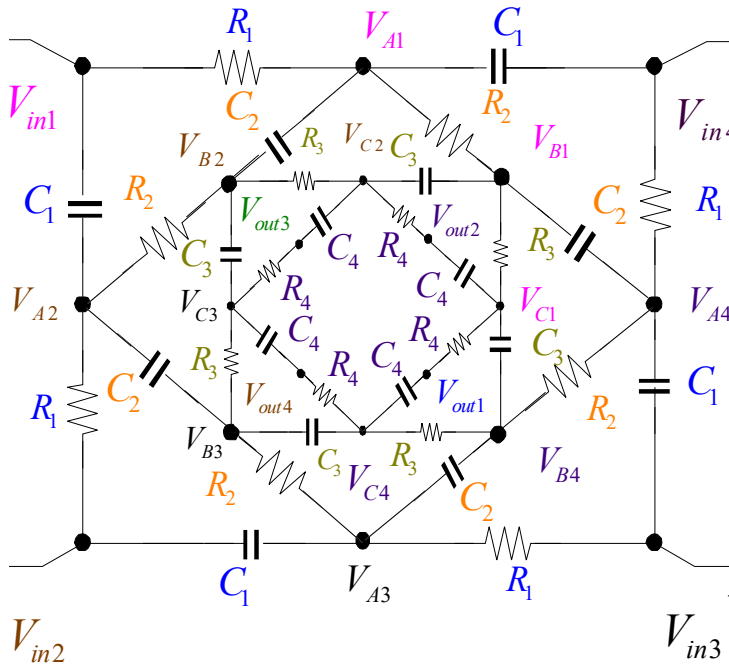
$E_i(t)$: input sources

$d_i(t)$: resistance distances

$d_k(t)$: sub resistance distances

2. Analysis of 4-Stage Passive RC Network

Derivation of Output Voltages on 1st Loop



Widened Superposition Principle



$$\left\{ \begin{aligned} V_{A1} Y_{total_A} &= \frac{V_{in1}}{R_1} + \frac{V_{in4}}{Z_{C1}} \\ V_{A2} Y_{total_A} &= \frac{V_{in2}}{R_1} + \frac{V_{in1}}{Z_{C1}} \\ V_{A3} Y_{total_A} &= \frac{V_{in3}}{R_1} + \frac{V_{in2}}{Z_{C1}} \\ V_{A4} Y_{total_A} &= \frac{V_{in4}}{R_1} + \frac{V_{in3}}{Z_{C1}} \end{aligned} \right.$$

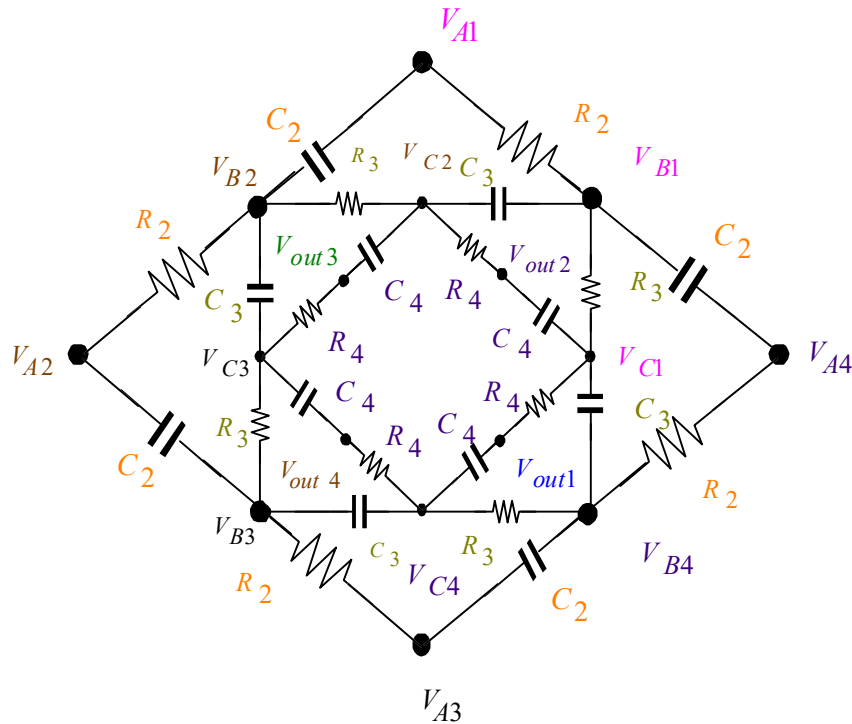
Here:

$$Y_{total_A} = \frac{1}{R_1} + \frac{1}{Z_{C1}} + \frac{1}{R_2 + \frac{1}{\frac{1}{Z_{C2}} + \frac{1}{R_3 + \frac{1}{\frac{1}{Z_{C3}} + \frac{1}{R_4 + \frac{1}{Z_{C4}}}}}}} + \frac{1}{Z_{C2} + \frac{1}{\frac{1}{R_2} + \frac{1}{\frac{1}{R_3 + \frac{1}{\frac{1}{Z_{C3}} + \frac{1}{R_4 + \frac{1}{Z_{C4}}}}}}} + \frac{1}{Z_{C3} + \frac{1}{\frac{1}{R_3} + \frac{2}{Z_{C4} + R_4}}}} + \frac{1}{Z_{C4} + \frac{1}{\frac{1}{R_4} + \frac{2}{Z_{C4} + R_4}}}}$$

$$= \frac{[2R_1Z_{C1} + (R_1 + Z_{C1})(R_2 + Z_{C2})][2R_3Z_{C3} + (R_3 + Z_{C3})(R_4 + Z_{C4})] + 2(R_3 + Z_{C3} + R_4 + Z_{C4})[(R_1 + Z_{C1})R_2Z_{C2} + R_1Z_{C1}(R_2 + Z_{C2})]}{R_1Z_{C1} \left\{ (R_2 + Z_{C2})[2R_3Z_{C3} + (R_3 + Z_{C3})(R_4 + Z_{C4})] + 2R_2Z_{C2}(R_3 + Z_{C3} + R_4 + Z_{C4}) \right\}}$$

2. Analysis of 4-Stage Passive RC Network

Derivation of Output Voltages on 2nd Loop



Widened Superposition Principle

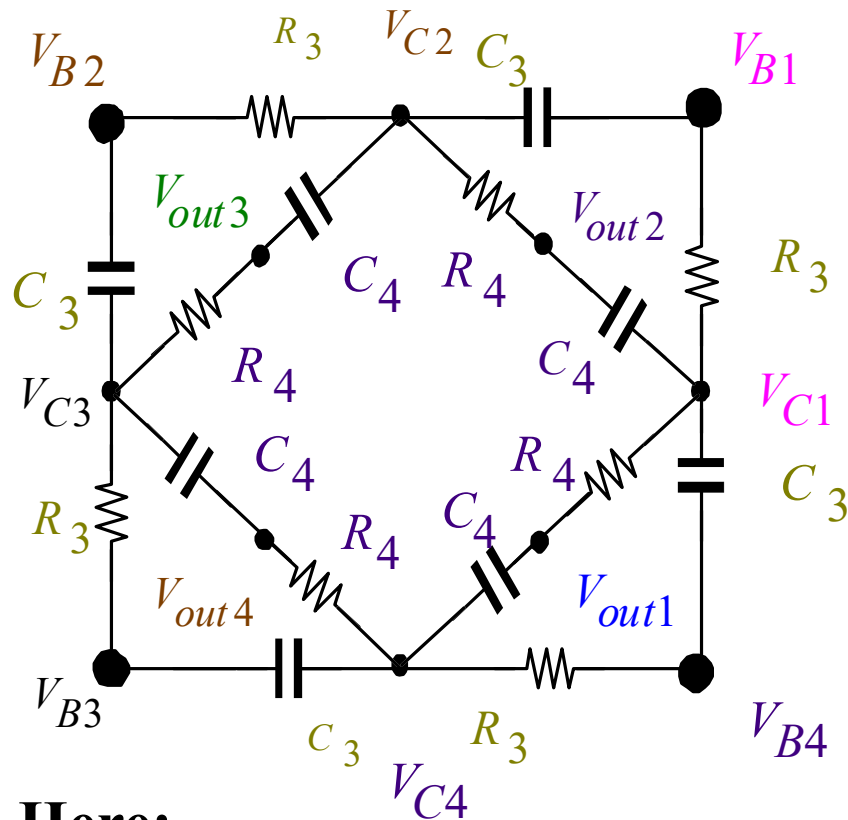
$$\left\{ \begin{aligned} V_{B1} Y_{total_B} &= \frac{V_{A1}}{R_2} + \frac{V_{A4}}{Z_{C2}} \\ V_{B2} Y_{total_B} &= \frac{V_{A2}}{R_2} + \frac{V_{A1}}{Z_{C2}} \\ V_{B3} Y_{total_B} &= \frac{V_{A3}}{R_2} + \frac{V_{A2}}{Z_{C2}} \\ V_{B4} Y_{total_B} &= \frac{V_{A4}}{R_2} + \frac{V_{A3}}{Z_{C2}} \end{aligned} \right.$$

Here: $Y_{total_B} = \frac{1}{R_2} + \frac{1}{Z_{C2}} + \frac{1}{R_3 + \frac{1}{\frac{1}{Z_{C3}} + \frac{2}{Z_{C4} + R_4}}} + \frac{1}{Z_{C3} + \frac{1}{\frac{1}{R_3} + \frac{2}{Z_{C4} + R_4}}}$

$$= \frac{(R_2 + Z_{C2}) [2R_3Z_{C3} + (R_3 + Z_{C3})(R_4 + Z_{C4})] + 2R_2Z_{C2}(R_3 + Z_{C3} + R_4 + Z_{C4})}{R_2Z_{C2} [2R_3Z_{C3} + (R_3 + Z_{C3})(R_4 + Z_{C4})]}$$

2. Analysis of 4-Stage Passive RC Network

Derivation of Output Voltages on 3rd Loop



Widened Superposition Principle

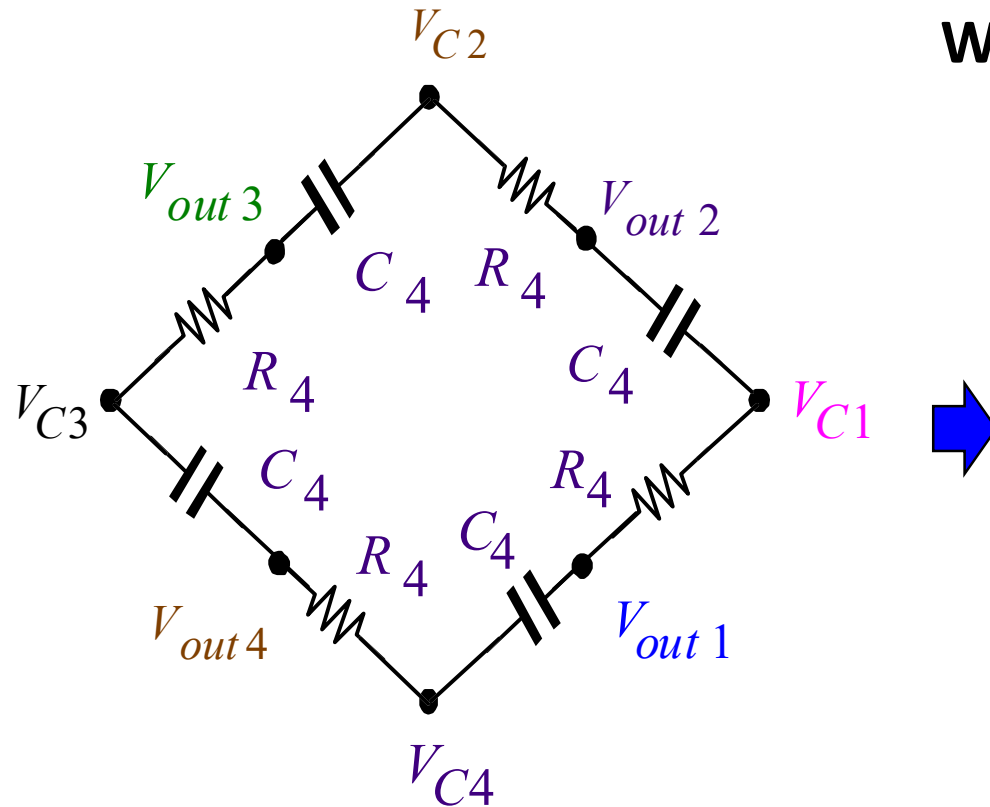
$$\begin{cases} V_{C1} Y_{total_C} = \frac{V_{B1}}{R_3} + \frac{V_{B4}}{Z_{C3}} \\ V_{C2} Y_{total_C} = \frac{V_{B2}}{R_3} + \frac{V_{B1}}{Z_{C3}} \\ V_{C3} Y_{total_C} = \frac{V_{B3}}{R_3} + \frac{V_{B2}}{Z_{C3}} \\ V_{C4} Y_{total_C} = \frac{V_{B4}}{R_3} + \frac{V_{B3}}{Z_{C3}} \end{cases}$$

Here:

$$Y_{total_C} = \frac{1}{R_3} + \frac{1}{Z_{C3}} + \frac{2}{Z_{C4} + R_4} = \frac{(Z_{C3} + R_3)(Z_{C4} + R_4) + 2R_3Z_{C3}}{R_3Z_{C3}(Z_{C4} + R_4)}$$

2. Analysis of 4-Stage Passive RC Network

Derivation of Output Voltages on 4th Loop



Widened Superposition Principle

$$\left\{ \begin{array}{l} V_{out1} Y_{total_D} = \frac{V_{C1}}{R_4} + \frac{V_{C4}}{Z_{C4}} \\ V_{out2} Y_{total_D} = \frac{V_{C2}}{R_4} + \frac{V_{C1}}{Z_{C4}} \\ V_{out3} Y_{total_D} = \frac{V_{C3}}{R_4} + \frac{V_{C2}}{Z_{C4}} \\ V_{out4} Y_{total_D} = \frac{V_{C4}}{R_4} + \frac{V_{C3}}{Z_{C4}} \end{array} \right.$$

Here:

$$Y_{total_D} = \frac{1}{R_4} + \frac{1}{Z_{C4}} = \frac{R_4 + Z_{C4}}{R_4 Z_{C4}}$$

2. Analysis of 4-Stage Passive RC Network

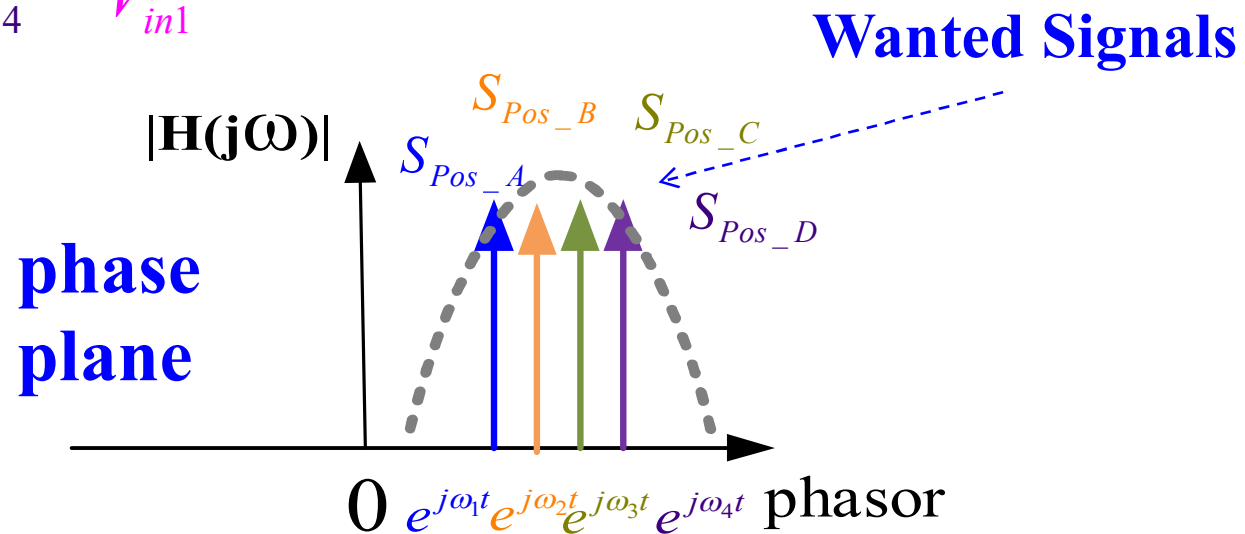
Model of Input Wanted Signals

$$S_{Pos_poly} \{V_1(t); V_2(t); V_3(t); V_4(t)\}$$

$$= \{1; j; -1; -j\} V_{pos}(t) = \left\{ 1; e^{j\frac{\pi}{2}}; e^{j\pi}; e^{j\frac{3\pi}{2}} \right\} \sum_{k=1}^n A_k \cos(\omega_k t + \theta_k)$$

Positive poly-phase signals

$$\frac{V_{in1}}{V_{in2}} = \frac{V_{in2}}{V_{in3}} = \frac{V_{in3}}{V_{in4}} = \frac{V_{in4}}{V_{in1}} = -j$$



2. Analysis of 4-Stage Passive RC Network

Derivation of Transfer Function (Wanted Signal)

Transfer Function

$$H = \frac{V_{out1}}{V_{in1}} = \frac{V_{out2}}{V_{in2}} = \frac{V_{out3}}{V_{in3}} = \frac{V_{out4}}{V_{in4}}$$

$$= \frac{(Z_{C4} - jR_4)(Z_{C3} - jR_3)(Z_{C2} - jR_2)(Z_{C1} - jR_1)}{\left[\begin{aligned} & \left[2R_1Z_{C1} + (Z_{C2} + R_2)(Z_{C1} + R_1) \right] \left[2R_3Z_{C3} + (Z_{C3} + R_3)(Z_{C4} + R_4) \right] \\ & + 2(Z_{C3} + R_3 + Z_{C4} + R_4) \left[(Z_{C1} + R_1)R_2Z_{C2} + (Z_{C2} + R_2)R_1Z_{C1} \right] \end{aligned} \right]}$$

$$Z_{C1} = \frac{1}{j2\pi fC_1}; Z_{C2} = \frac{1}{j2\pi fC_2} \quad f_1 = \frac{1}{2\pi R_1C_1}; f_2 = \frac{1}{2\pi R_2C_2}; f_{21} = \frac{1}{2\pi R_2C_1};$$

$$Z_{C3} = \frac{1}{j2\pi fC_3} \quad f_3 = \frac{1}{2\pi R_3C_3}; f_{31} = \frac{1}{2\pi R_3C_1}; f_{32} = \frac{1}{2\pi R_3C_2};$$

$$Z_{C4} = \frac{1}{j2\pi fC_4} \quad f_4 = \frac{1}{2\pi R_4C_4}; f_{41} = \frac{1}{2\pi R_4C_1}; f_{42} = \frac{1}{2\pi R_4C_2}; f_{43} = \frac{1}{2\pi R_4C_3};$$

2. Analysis of 4-Stage Passive RC Network

Derivation of Transfer Function (Wanted Signal)

Transfer Function

$$H = \frac{\left\{ s^4 + js^3 (f_4 + f_3 + f_2 + f_1) - s^2 \left[f_4 (f_3 + f_2 + f_1) + f_3 (f_2 + f_1) + f_2 f_1 \right] \right.}{\left. \left\{ -js \left\{ f_4 \left[f_3 (f_2 + f_1) + f_2 f_1 \right] + f_3 f_2 f_1 \right\} + f_4 f_3 f_2 f_1 \right\} \right.}$$

$$H = \frac{\left\{ s^4 + s^3 \left(f_4 + f_3 + f_2 + f_1 + 2 \left[(f_{43} + f_{42} + f_{41}) + (f_{32} + f_{31}) + f_{21} \right] \right) \right.}{\left. \left\{ +s^2 \left[\begin{aligned} & f_4 (f_3 + f_2 + f_1) + f_3 (f_2 + f_1) + f_2 f_1 \\ & + 4 f_{43} f_{21} + 2 \left(\begin{aligned} & f_4 \left((f_{32} + f_{31}) + f_{21} \right) + f_3 \left((f_{42} + f_{41}) + f_{21} \right) \\ & + f_2 \left((f_{43} + f_{41}) + f_{31} \right) + f_1 \left((f_{43} + f_{42}) + f_{32} \right) \end{aligned} \right) \end{aligned} \right] \right.}$$

$$\left. \left\{ +s \left\{ f_4 \left[f_3 (f_2 + f_1) + f_2 f_1 \right] + f_3 f_2 f_1 + 2 \left(\begin{aligned} & f_4 (f_3 f_{21} + f_2 f_{31} + f_1 f_{32}) \\ & + f_3 (f_2 f_{41} + f_1 f_{42}) + f_2 f_1 f_{43} \end{aligned} \right) \right\} \right.}$$

$$\left. \left\{ + f_4 f_3 f_2 f_1 \right\} \right.}$$

2. Analysis of 4-Stage Passive RC Network

Derivation of Transfer Function (Wanted Signal)

$$a_1 = f_4 + f_3 + f_2 + f_1$$

$$a_2 = f_4 (f_3 + f_2 + f_1) + f_3 (f_2 + f_1) + f_2 f_1$$

$$a_3 = f_4 [f_3 (f_2 + f_1) + f_2 f_1] + f_3 f_2 f_1$$

$$a_4 = f_4 f_3 f_2 f_1$$

$$a_5 = a_1 + 2[(f_{43} + f_{42} + f_{41}) + (f_{32} + f_{31}) + f_{21}]$$

$$a_6 = a_2 + 4f_{43}f_{21} + 2 \left(\begin{aligned} & f_4 ((f_{32} + f_{31}) + f_{21}) + f_3 ((f_{42} + f_{41}) + f_{21}) \\ & + f_2 ((f_{43} + f_{41}) + f_{31}) + f_1 ((f_{43} + f_{42}) + f_{32}) \end{aligned} \right)$$

$$a_7 = a_3 + 2(f_4 (f_3 f_{21} + f_2 f_{31} + f_1 f_{32}) + f_3 (f_2 f_{41} + f_1 f_{42}) + f_2 f_1 f_{43})$$

Transfer function

$$H_{Pos}(j2\pi f) = \frac{s^4 + ja_1 s^3 - a_2 s^2 - ja_3 s + a_4}{s^4 + a_5 s^3 + a_6 s^2 + a_7 s + a_4}$$

2. Analysis of 4-Stage Passive RC Network

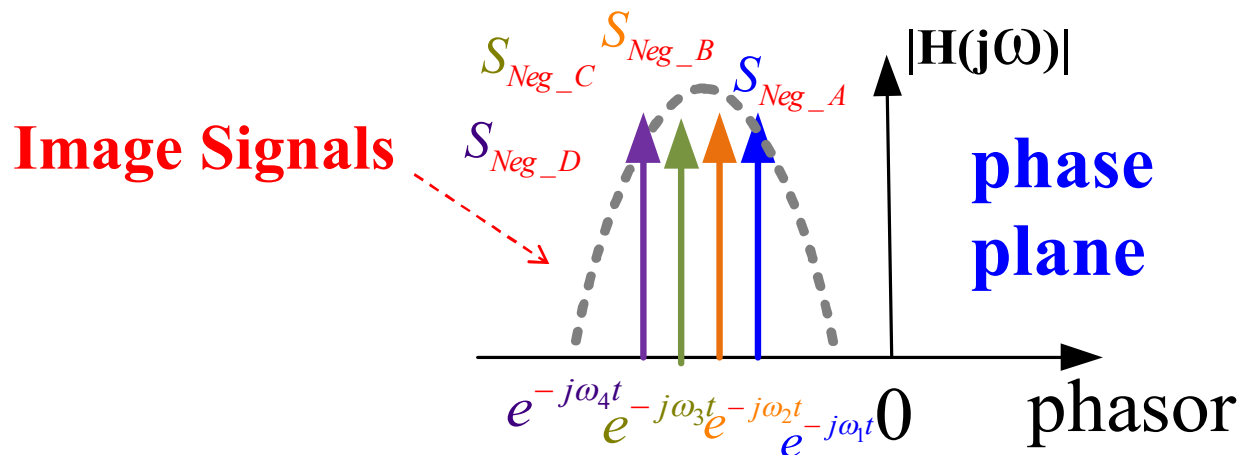
Model of Input Image Signals

$$S_{Neg_poly} \{V_1(t); V_2(t); V_3(t); V_4(t)\}$$

$$= \{V(t); -jV(t); -V(t); jV(t)\} = \left\{ V(t); e^{-j\frac{\pi}{2}}V(t); e^{-j\pi}V(t); e^{-j\frac{3\pi}{2}}V(t) \right\}$$

Negative poly-phase signals

$$\frac{V_{in1}}{V_{in2}} = \frac{V_{in2}}{V_{in3}} = \frac{V_{in3}}{V_{in4}} = \frac{V_{in4}}{V_{in1}} = +j$$



2. Analysis of 4-Stage Passive RC Network

Derivation of Transfer Function (Image Signal)

Transfer Function

$$H = \frac{(Z_{C4} + jR_4)(Z_{C3} + jR_3)(Z_{C2} + jR_2)(Z_{C1} + jR_1)}{\left[\begin{aligned} & \left[2R_1Z_{C1} + (Z_{C2} + R_2)(Z_{C1} + R_1) \right] \left[2R_3Z_{C3} + (Z_{C3} + R_3)(Z_{C4} + R_4) \right] \\ & + 2(Z_{C3} + R_3 + Z_{C4} + R_4) \left[(Z_{C1} + R_1)R_2Z_{C2} + (Z_{C2} + R_2)R_1Z_{C1} \right] \end{aligned} \right]}$$



$$H = \frac{\left\{ s^4 - js^3(f_4 + f_3 + f_2 + f_1) - s^2 \left[f_4(f_3 + f_2 + f_1) + f_3(f_2 + f_1) + f_2f_1 \right] + js \left\{ f_4 \left[f_3(f_2 + f_1) + f_2f_1 \right] + f_3f_2f_1 \right\} + f_4f_3f_2f_1 \right\}}{\left[\begin{aligned} & s^4 + s^3(f_4 + f_3 + f_2 + f_1 + 2[(f_{43} + f_{42} + f_{41}) + (f_{32} + f_{31}) + f_{21}]) + s^2 \left[\begin{aligned} & f_4(f_3 + f_2 + f_1) + f_3(f_2 + f_1) + f_2f_1 \\ & + 4f_{43}f_{21} + 2 \left(\begin{aligned} & f_4((f_{32} + f_{31}) + f_{21}) + f_3((f_{42} + f_{41}) + f_{21}) \\ & + f_2((f_{43} + f_{41}) + f_{31}) + f_1((f_{43} + f_{42}) + f_{32}) \end{aligned} \right) \end{aligned} \right] \\ & + s \left\{ f_4 \left[f_3(f_2 + f_1) + f_2f_1 \right] + f_3f_2f_1 + 2 \left(\begin{aligned} & f_4(f_3f_{21} + f_2f_{31} + f_1f_{32}) \\ & + f_3(f_2f_{41} + f_1f_{42}) + f_2f_1f_{43} \end{aligned} \right) \right\} + f_4f_3f_2f_1 \end{aligned} \right]}$$



$$H_{Neg}(j2\pi f) = \frac{s^4 - ja_1s^3 - a_2s^2 + ja_3s + a_4}{s^4 + a_5s^3 + a_6s^2 + a_7s + a_4}$$

2. Analysis of 4-Stage Passive RC Network

Composed Transfer Function of 4-Stage Passive RC Network

Wanted Signals

$$H_{Pos}(j2\pi f) = \frac{s^4 + ja_1s^3 - a_2s^2 - ja_3s + a_4}{s^4 + a_5s^3 + a_6s^2 + a_7s + a_4}; \forall f > 0$$

Image Signals

$$H_{Neg}(j2\pi f) = \frac{s^4 - ja_1s^3 - a_2s^2 + ja_3s + a_4}{s^4 + a_5s^3 + a_6s^2 + a_7s + a_4}; \forall f < 0$$

Composed transfer function

$$|H(f)| = \frac{|f^4 + a_1f^3 + a_2f^2 + a_3f + a_4|}{\sqrt{(f^4 + a_4 - a_6f^2)^2 + (a_7f - a_5f^3)^2}}; \forall f \in R$$

Image Rejection Ratio

$$IRR = \frac{H_{Pos}(j2\pi f)}{H_{Neg}(j2\pi f)} = \frac{(f_1 + f)(f_2 + f)(f_3 + f)(f_4 + f)}{(f_1 - f)(f_2 - f)(f_3 - f)(f_4 - f)}$$

2. Analysis of 4-Stage Passive RC Network

Analysis of Transfer Function (Positive Frequency)

$$|H(f)| = \frac{f^4 + a_1 f^3 + a_2 f^2 + a_3 f + a_4}{\sqrt{(f^4 + a_4 - a_6 f^2)^2 + (a_7 f - a_5 f^3)^2}}; \forall f > 0$$

$$\lim_{f \rightarrow 0} |H(f)| = \lim_{f \rightarrow 0} \frac{f^4 + a_1 f^3 + a_2 f^2 + a_3 f + a_4}{\sqrt{(f^4 + a_4 - a_6 f^2)^2 + (a_7 f - a_5 f^3)^2}} = 1$$

$$\lim_{f \rightarrow \infty} |H(f)| = \lim_{f \rightarrow \infty} \frac{f^4 + a_1 f^3 + a_2 f^2 + a_3 f + a_4}{\sqrt{(f^4 + a_4 - a_6 f^2)^2 + (a_7 f - a_5 f^3)^2}} = 1$$

$$\min(|H(f)|) \text{ as } f = \sqrt[4]{f_4 f_3 f_2 f_1}$$

Applying Cauchy-Schwarz inequality theorem:

$$a, b > 0, a^2 + b^2 \geq 2ab; \min(a^2 + b^2) = 2ab \text{ as } "a = b"$$

$$(f^4 + a_4 - a_6 f^2)^2 + (a_7 f - a_5 f^3)^2 \geq 2|(f^4 + a_4 - a_6 f^2)|(a_7 f - a_5 f^3)|$$

$$|(f^4 + a_4 - a_6 f^2)| = |(a_7 f - a_5 f^3)|; \Rightarrow \begin{cases} f_{\min 1} = \dots \\ f_{\min 2} = \dots \end{cases} \Rightarrow \begin{cases} \max 1(|H(f)|) \\ \max 2(|H(f)|) \end{cases}$$

2. Analysis of 4-Stage Passive RC Network

Analysis of Transfer Function (Negative Frequency)

$$|H(f)| = \frac{f^4 - a_1 f^3 + a_2 f^2 - a_3 f + a_4}{\sqrt{(f^4 + a_4 - a_6 f^2)^2 + (a_7 f - a_5 f^3)^2}}; \forall f < 0$$

$$\lim_{f \rightarrow 0} |H(f)| = \lim_{f \rightarrow 0} \frac{f^4 - a_1 f^3 + a_2 f^2 - a_3 f + a_4}{\sqrt{(f^4 + a_4 - a_6 f^2)^2 + (a_7 f - a_5 f^3)^2}} = 1$$

$$\lim_{f \rightarrow -\infty} |H(f)| = \lim_{f \rightarrow -\infty} \frac{f^4 - a_1 f^3 + a_2 f^2 - a_3 f + a_4}{\sqrt{(f^4 + a_4 - a_6 f^2)^2 + (a_7 f - a_5 f^3)^2}} = 1$$

$$\min(|H(f)|_{dB}) = -\infty; \text{ as } f = -f_1 \vee f = -f_2 \vee f = -f_3 \vee f = -f_4$$

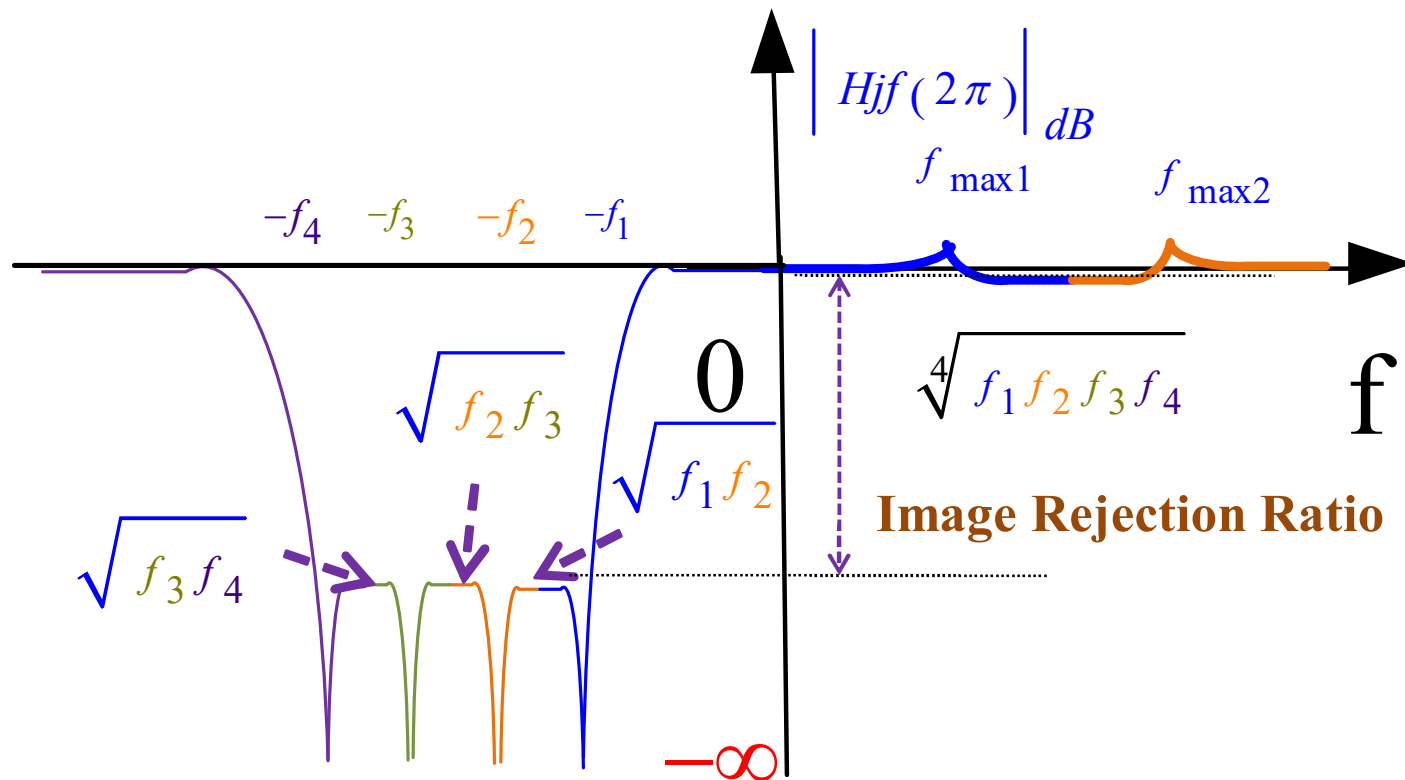
$$\max 1(|H(f)|) \text{ as } f = \sqrt{f_1 f_2}; \max 2(|H(f)|) \text{ as } f = \sqrt{f_2 f_3}; \max 3(|H(f)|) \text{ as } f = \sqrt{f_3 f_4}$$

2. Analysis of 4-Stage Passive RC Network

Frequency Responses of 4-Stage Passive RC Network

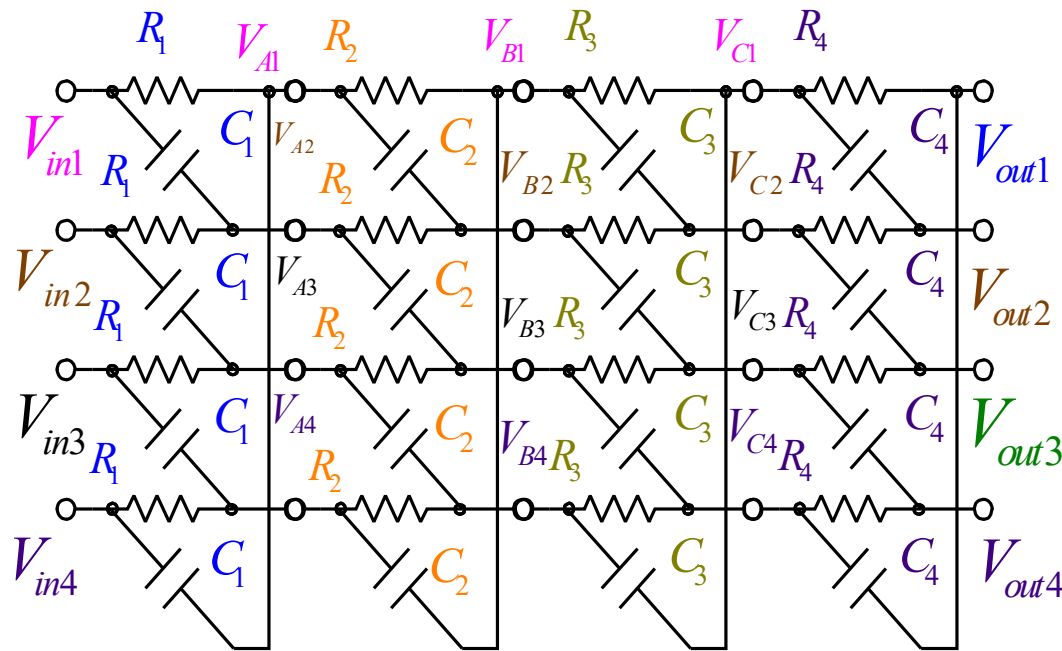
Transfer function $|H(f)| = \frac{|f^4 + a_1 f^3 + a_2 f^2 + a_3 f + a_4|}{\sqrt{(f^4 + a_4 - a_6 f^2)^2 + (a_7 f - a_5 f^3)^2}}; \forall f \in R$

Frequency Responses



3. Proposed Model of 4-Stage Passive RC Network

Model of 4-Stage Passive RC Network



$$R_1 = 1k\Omega; C_1 = 227 pF;$$

$$R_2 = 1k\Omega; C_2 = 106 pF;$$

$$R_3 = 1k\Omega; C_3 = 39.8 pF;$$

$$R_4 = 1k\Omega; C_4 = 19.9 pF;$$

$$f_1 = 0.7 MHz;$$

$$f_2 = 1.5 MHz; f_{21} = 0.7 MHz;$$

$$f_3 = 4 MHz; f_{31} = 0.7 MHz; f_{32} = 1.5 MHz;$$

$$f_4 = 8 MHz; f_{41} = 0.7 MHz; f_{42} = 1.5 MHz; f_{43} = 4 MHz;$$

3. Proposed Model of 4-Stage Passive RC Network

Simplified Model of 4-Stage Passive RC Network

$$a_1 = f_4 + f_3 + f_2 + f_1 = 1.42 * 10^7$$

$$a_2 = f_4 (f_3 + f_2 + f_1) + f_3 (f_2 + f_1) + f_2 f_1 = 5.95 * 10^{13}$$

$$a_3 = f_4 [f_3 (f_2 + f_1) + f_2 f_1] + f_3 f_2 f_1 = 8.3 * 10^{19}$$

$$a_4 = f_4 f_3 f_2 f_1 = 3.36 * 10^{25}$$

$$a_5 = a_1 + 2[(f_{43} + f_{42} + f_{41}) + (f_{32} + f_{31}) + f_{21}] = 3.24 * 10^7$$

$$a_6 = a_2 + 4f_{43}f_{21} + 2 \left(\begin{array}{l} f_4 ((f_{32} + f_{31}) + f_{21}) + f_3 ((f_{42} + f_{41}) + f_{21}) \\ + f_2 ((f_{43} + f_{41}) + f_{31}) + f_1 ((f_{43} + f_{42}) + f_{32}) \end{array} \right) = 1.66 * 10^{14}$$

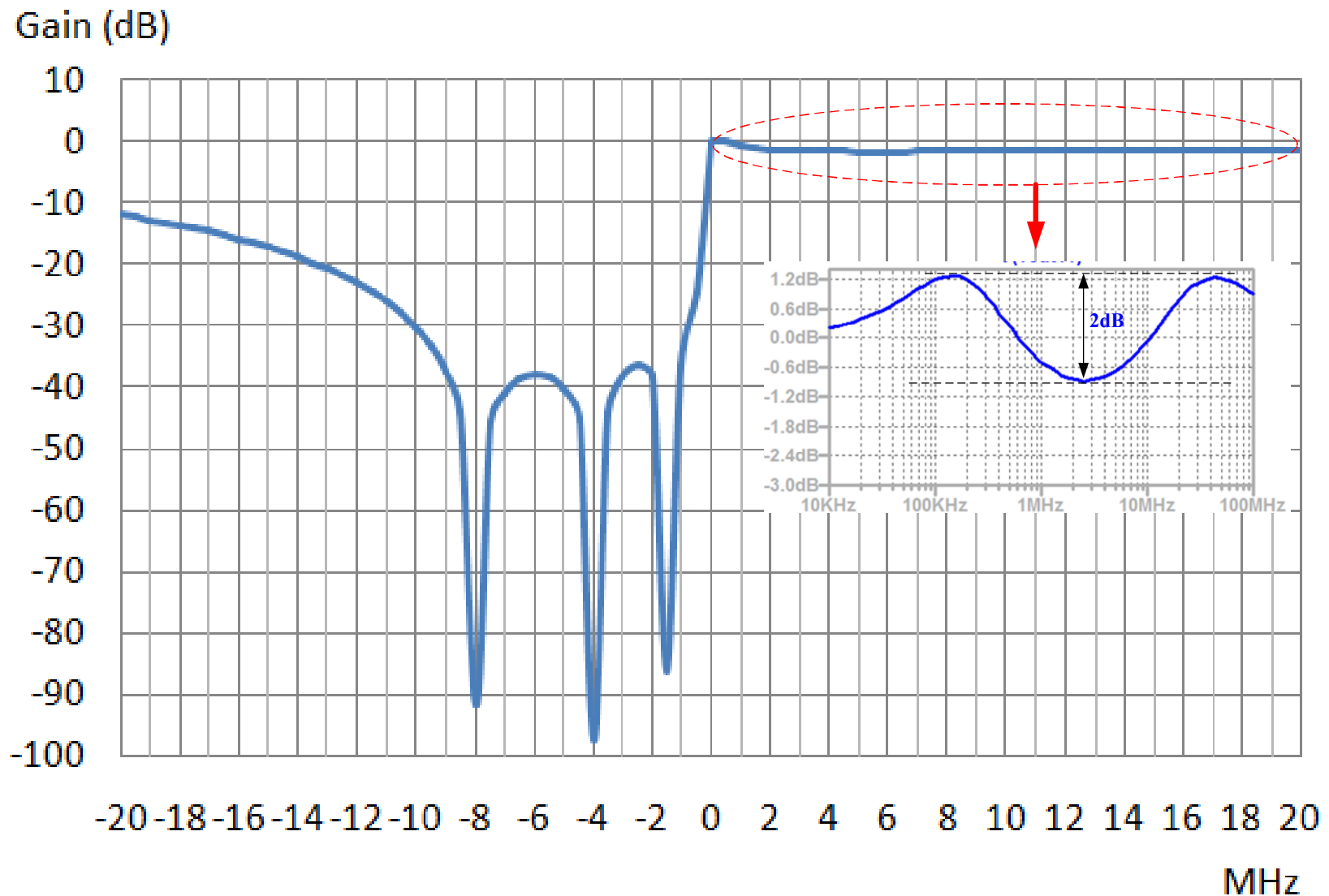
$$a_7 = a_3 + 2(f_4 (f_3 f_{21} + f_2 f_{31} + f_1 f_{32}) + f_3 (f_2 f_{41} + f_1 f_{42}) + f_2 f_1 f_{43}) = 1.87 * 10^{20}$$

Transfer function

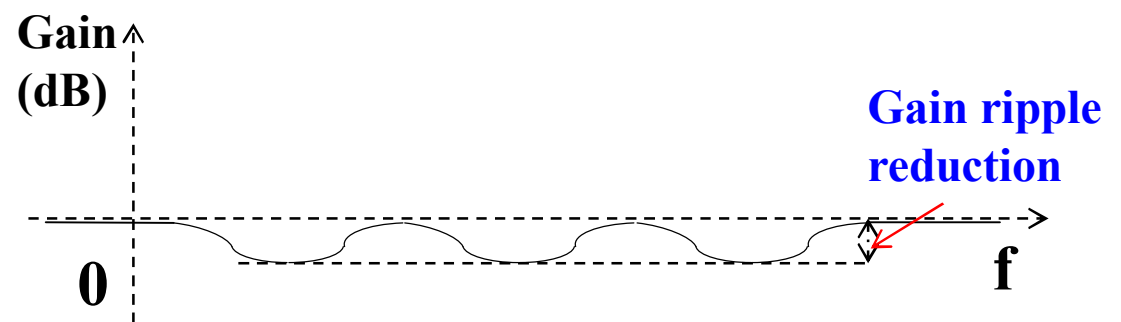
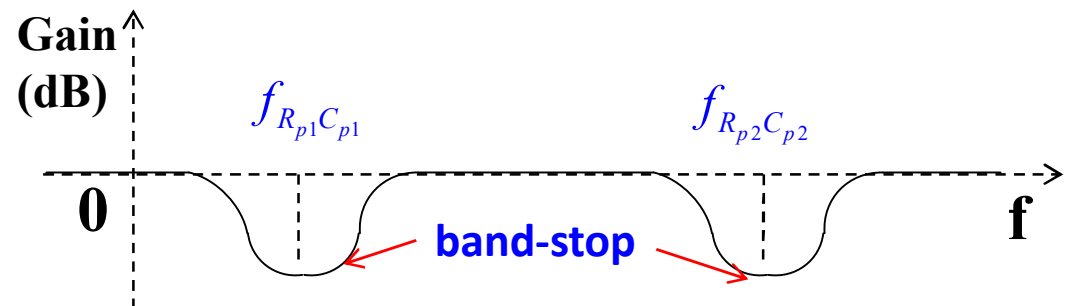
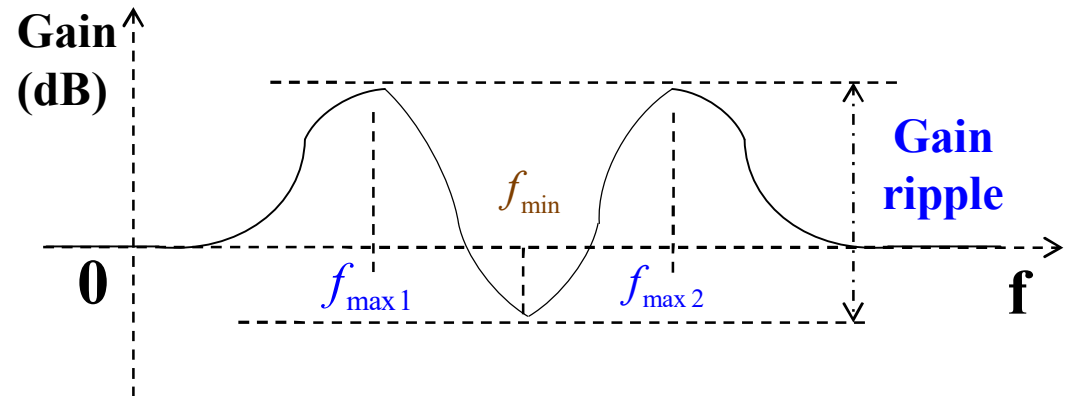
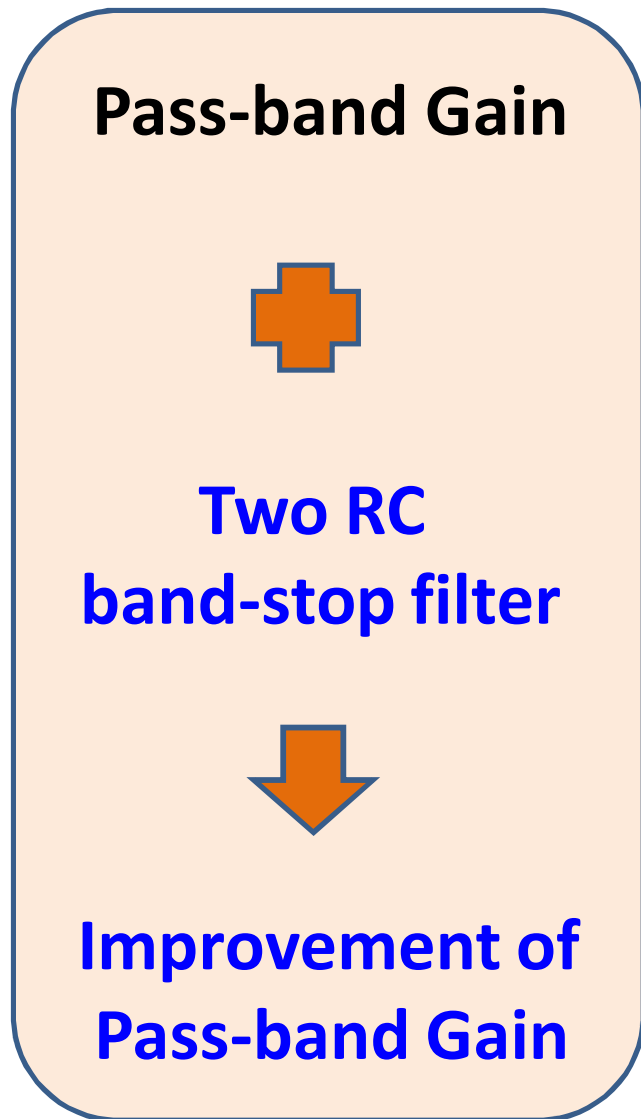
$$|H(f)|_{dB} = \frac{|f^4 + 1.42 * 10^7 f^3 + 5.95 * 10^{13} f^2 + 8.3 * 10^{19} f + 3.36 * 10^{25}|}{\sqrt{(f^4 + 3.36 * 10^{25} - 1.66 * 10^{14} f^2)^2 + (1.87 * 10^{20} f - 3.24 * 10^7 f^3)^2}}$$

3. Proposed Model of 4-Stage Passive RC Network

Experimental Results of 4-Stage Passive RC Network



3. Proposed Model of 4-Stage Passive RC Network Algorithm of Flat Pass-band Gain

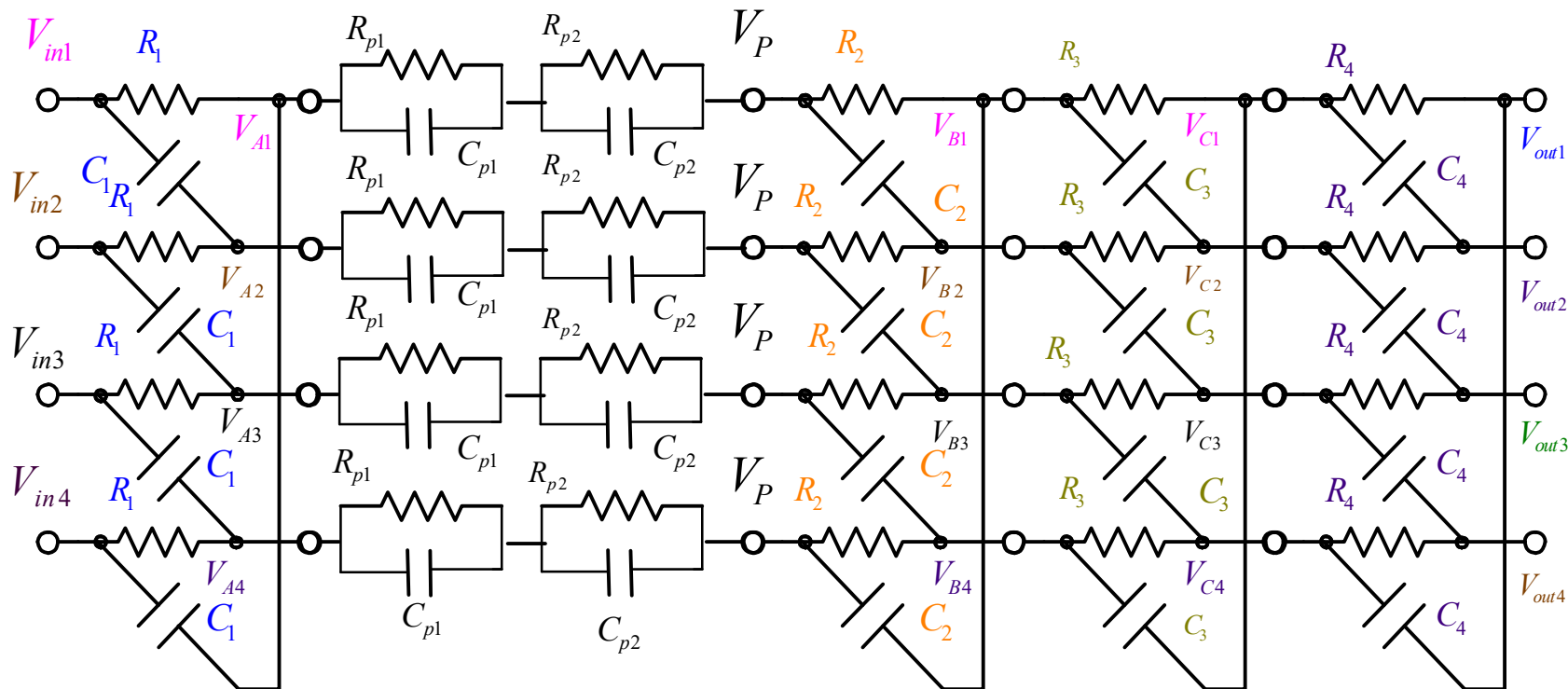


3. Proposed Model of 4-Stage Passive RC Network

Proposed Design of Two RC Band-stop Filters

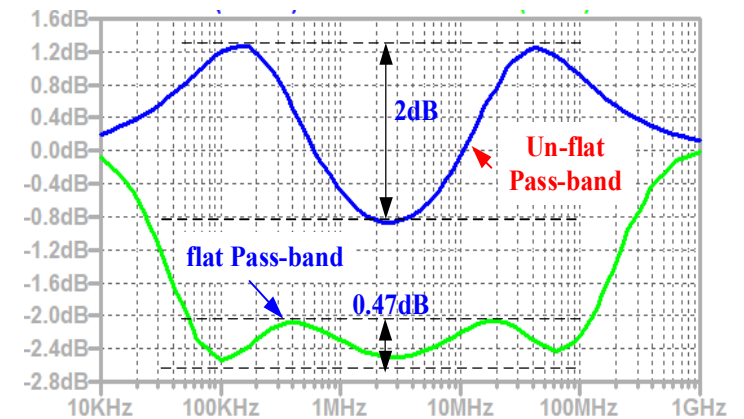
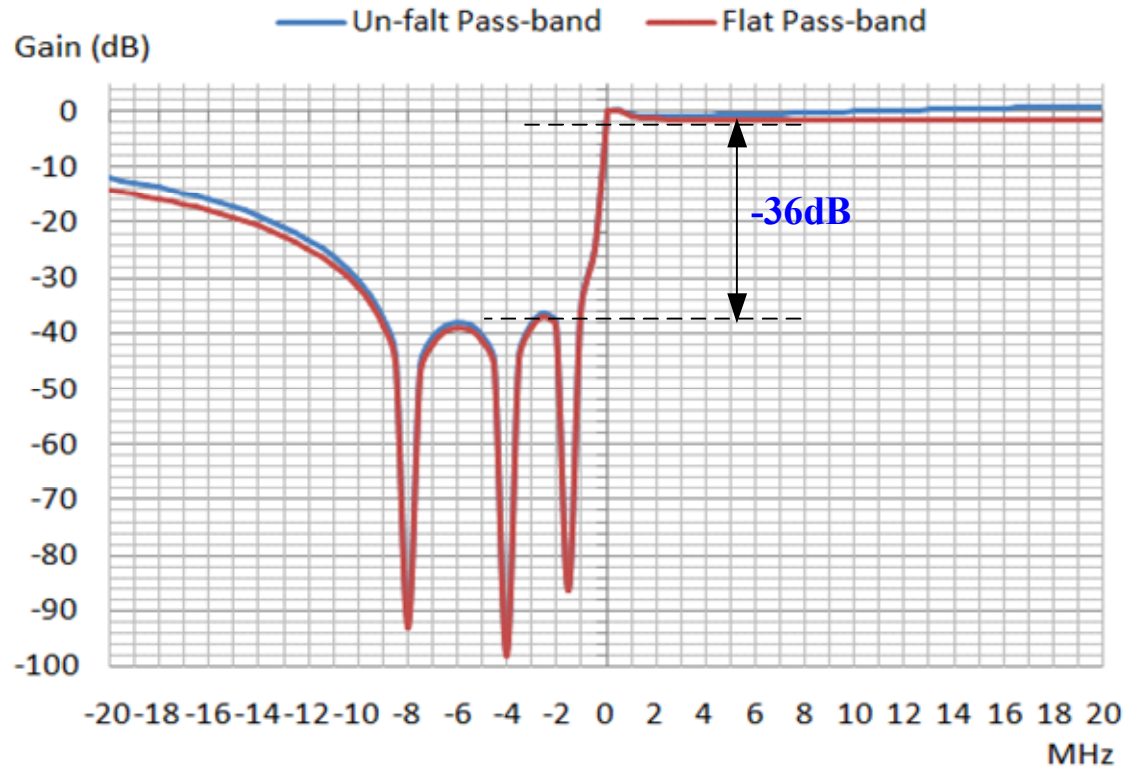
$$R_1 = 1k\Omega; C_1 = 227 pF; R_{p1} = 6k\Omega; C_{p1} = 5nF; R_{p2} = 100\Omega; C_{p2} = 12 pF;$$

$$R_2 = 1k\Omega; C_2 = 106 pF; R_3 = 1k\Omega; C_3 = 39.8 pF; R_4 = 1k\Omega; C_4 = 19.9 pF;$$



3. Proposed Model of 4-Stage Passive RC Network

Experimental Results of Proposed Polyphase Filter



Flat Pass-band Gain

Improvement of pass-band gain ripple
→ from **2dB** into **0.47dB**

4. Conclusions

This Work:

- **Derivation of transfer function** of poly-phase network based on superposition principle
- **Mathematical analysis** and **model** of 4-stage passive RC poly-phase filter
- **Improvement of pass-band gain ripple from 2dB into 0.47dB** with **two RC band-stop filters**
- **Image rejection ratio: -36dB**

Future of Work

- **Analysis of IQ mismatches of poly-phase signals**
- **Analysis of Parasitic of RC components**

Thanks for your kind attention!



谢谢