

High-Resolution Low-Sampling-Rate $\Delta\Sigma$ ADC Linearity Short-Time Test Algorithm

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OUTLINE

- Research background and objective
- Proposed linearity test method
- Simulation configuration and results
- Conclusion

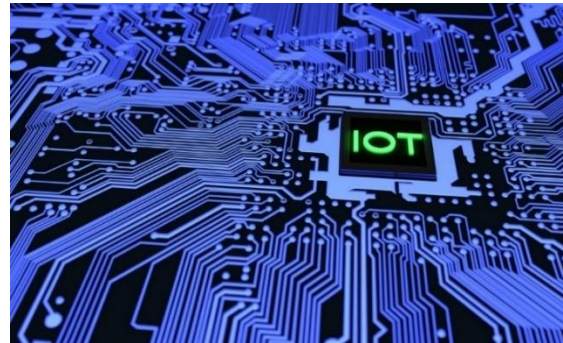
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Research Background

IOT (Internet of things)

- Testing and evaluation of IOT devices are becoming important.



- Mass production shipment of IOT devices requires high quality and low cost testing.



Research Objective

High resolution, low speed $\Delta\Sigma$ ADC

- Sensor interface key components
- Mass production test
 - ✓ Linearity test takes a long time.
 - ✓ In most cases, it is omitted.

High reliability requirements



- ✓ Perform its linearity test in a short time
- ✓ Develop its algorithm

$\Delta\Sigma$ ADC Testing Challenge

Sensor + amplifier + $\Delta\Sigma$ ADC + microcomputer



4 difficulties for its mass production shipping test.

- ① Low speed sampling
- ② High resolution



Long test time

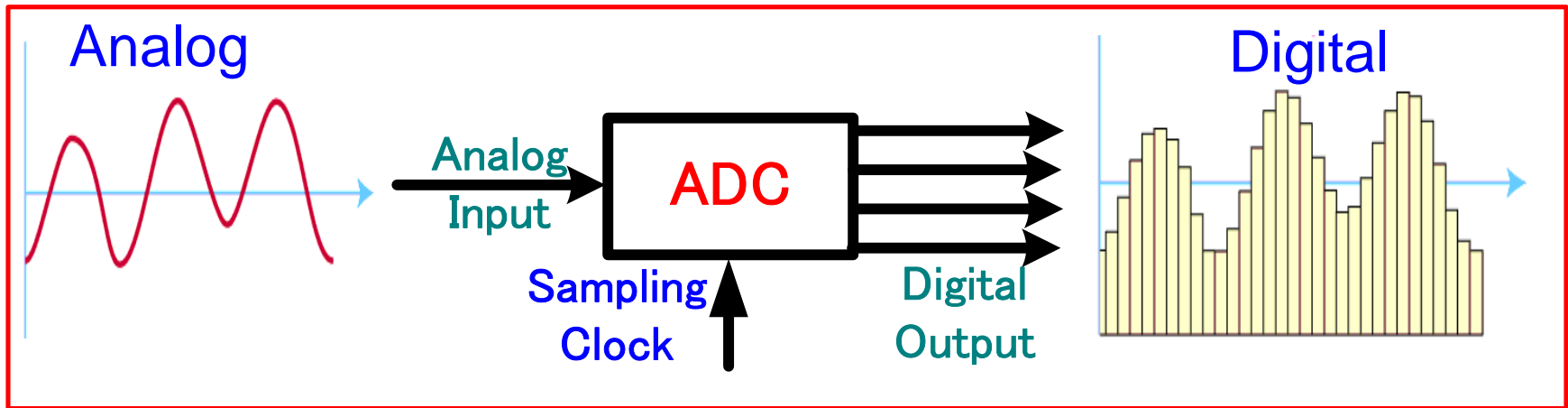
- ③ High linearity analog input signal
- ④ Complex ADC output signal processing

1 US dollar chip



Test time should be less than 1 second

ADC Role in Digital Era

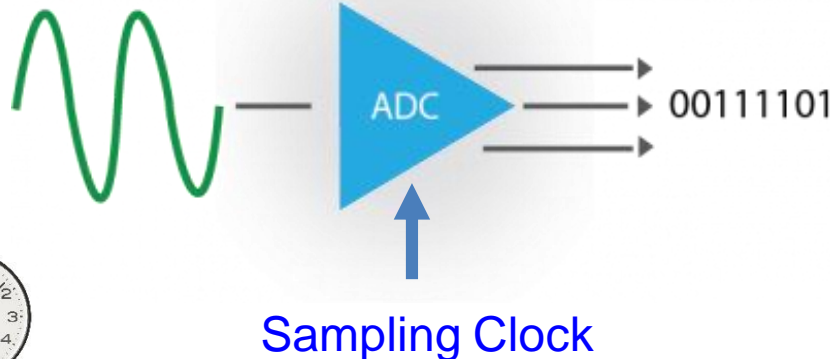


Analog signal :
continuous signal



Digital signal :
discrete numerical signal

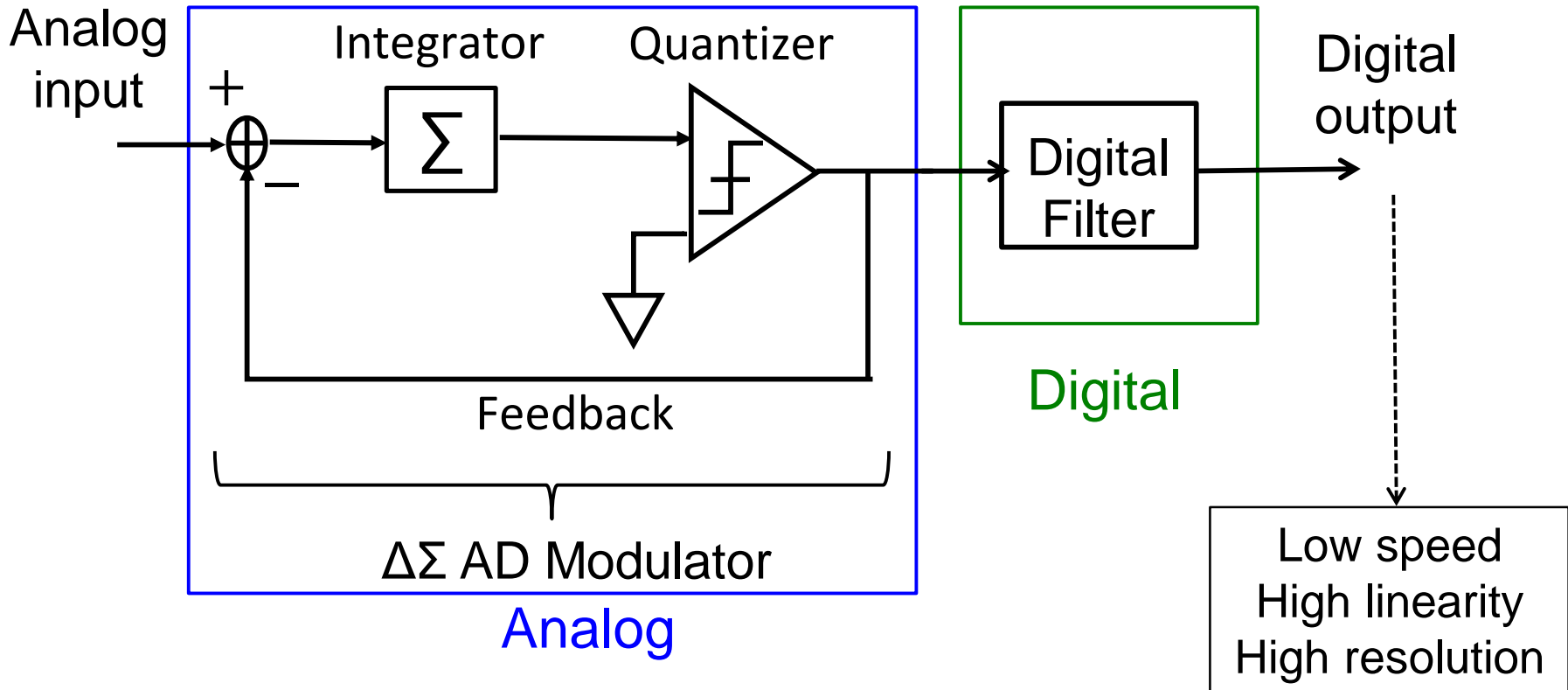
- ◆ Natural signal (sound, light)
- ◆ Analog clock



- ◆ Binary number
- ◆ Digital clock

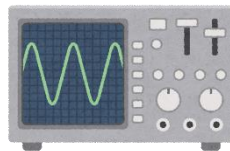


$\Delta\Sigma$ ADC



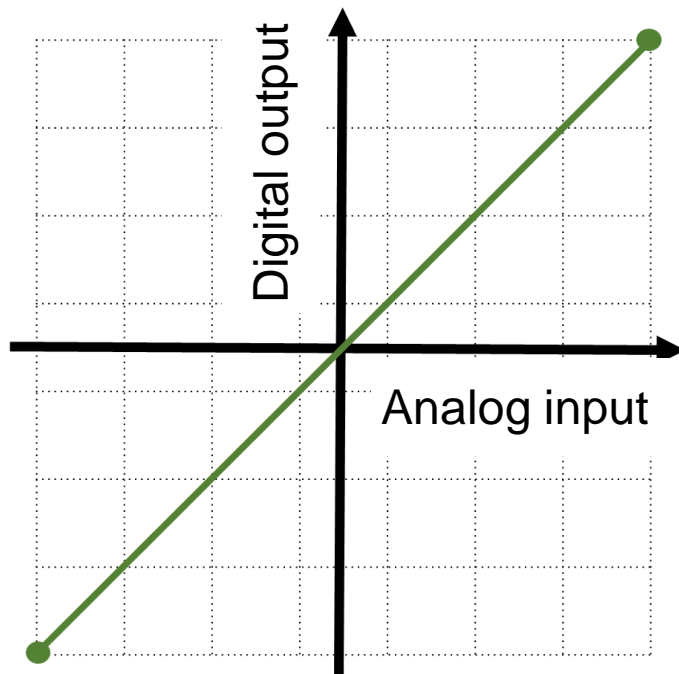
< Application >

- Measurement
- Audio system
- Satellite communication

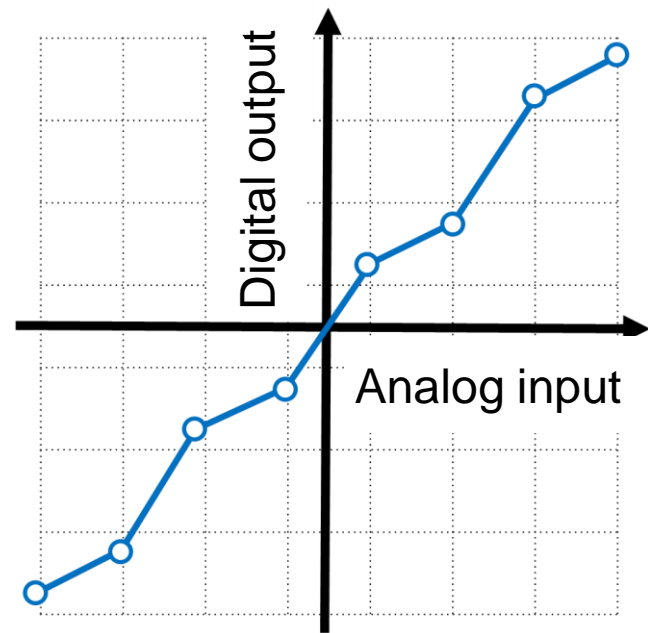


Linearity of $\Delta\Sigma$ ADC

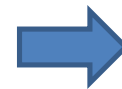
Ideal characteristic (linear)



Actual (nonlinear)



Circuit imperfection, variation



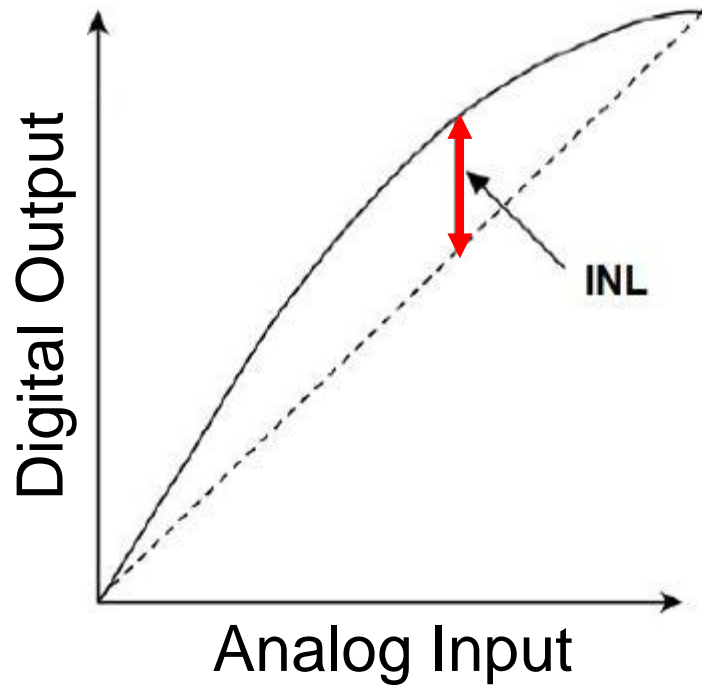
Nonlinear



Linearity :

- ✓ Important performance item
- ✓ Need its accurate test in a short time.

Integral Non-Linearity: INL



If INL is large :

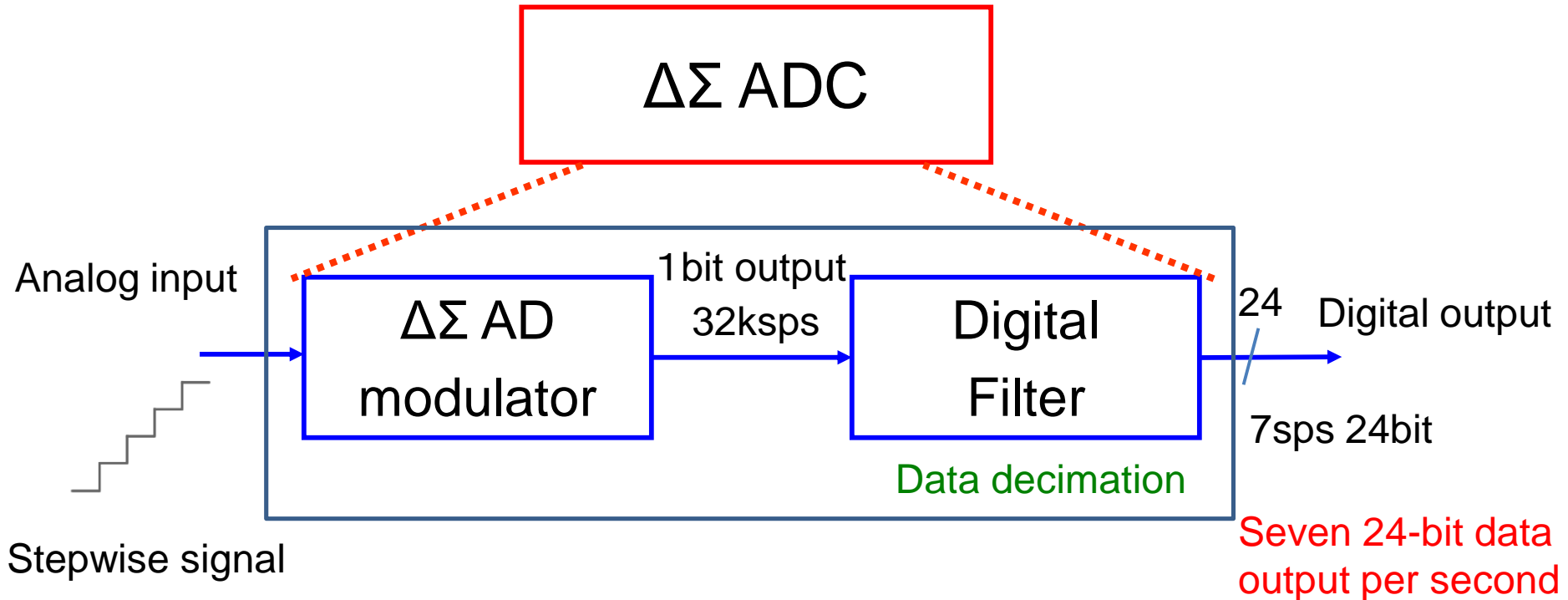
- ✓ Missing codes occur
- ✓ Lack of monotonicity

Deviation between the ideal input threshold value and the measured threshold level of a certain output code.

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Problem of Direct Linearity Test



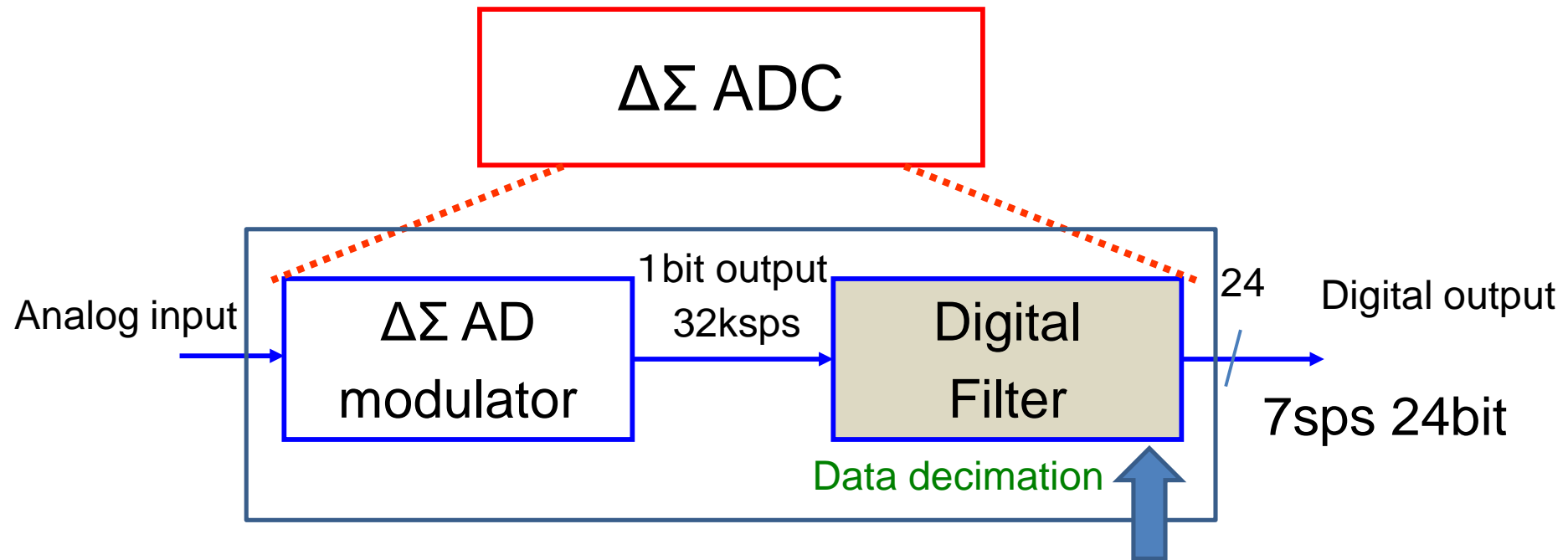
Linearity test time

Assuming 4 point per code
 $(1/7) \times 2^{24} \times 4$ seconds = 104 day !



Totally unrealistic

Digital Filter Test



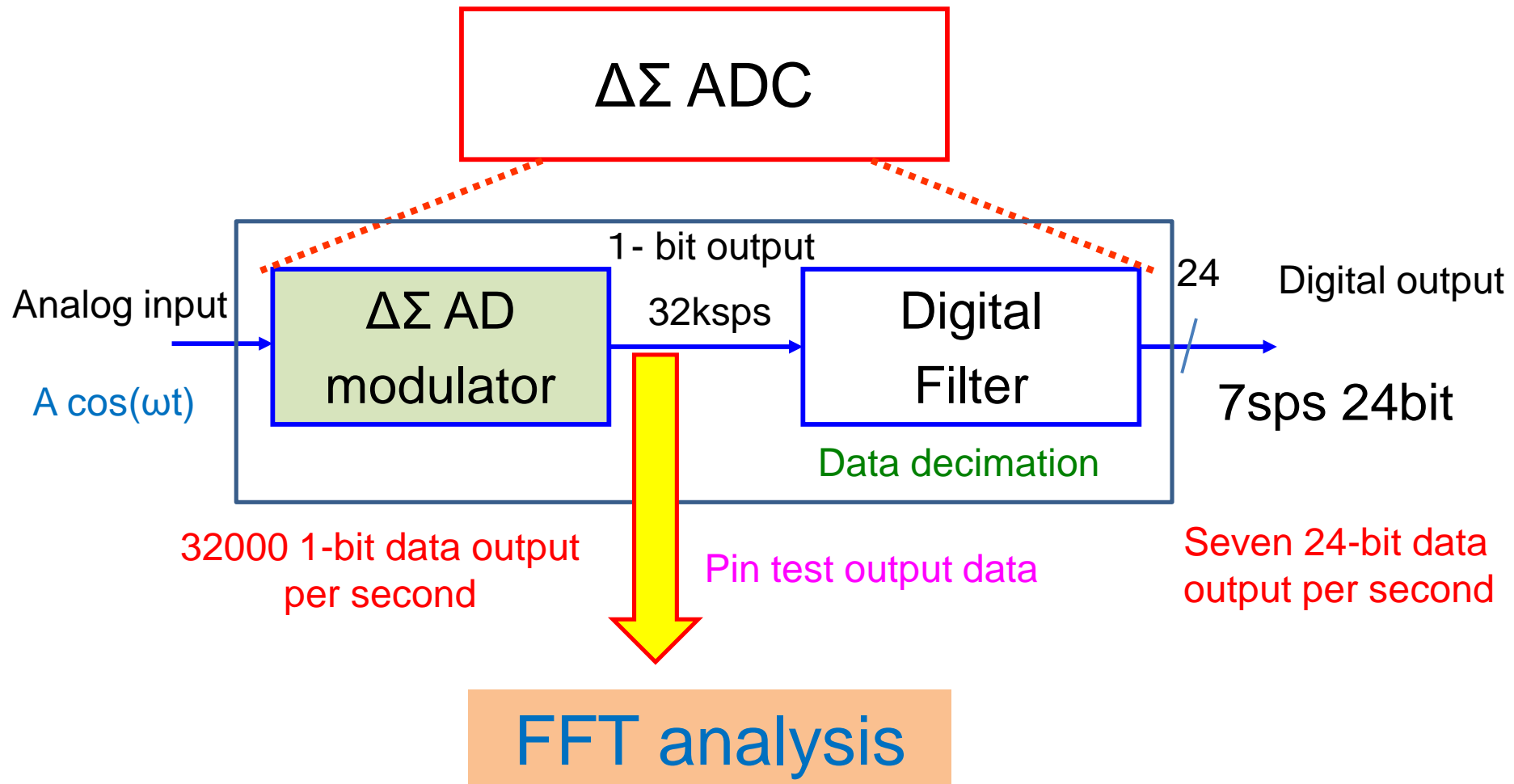
Digital filter does NOT affect the linearity.

Only pass or fail.

**Test with
scan path method**

$\Delta\Sigma$ AD Modulator Test

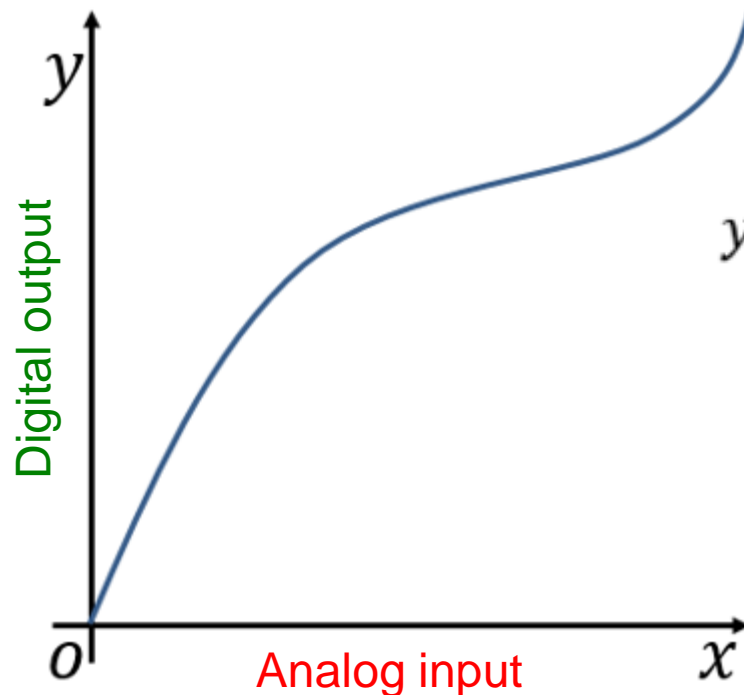
Proposed: Cosine Input & FFT Analysis



I/O Characteristic Modeling of Modulator

Modeling by polynomial approximation

- ✓ Assumption: I/O characteristics are continuous in the AD modulator.



$$y = a_0 + a_1x + a_2x^2 + \dots + a_nx^n$$

3rd order model for simplicity :

$$y(t) = a_1x(t) + a_3x(t)^3$$

Polynomial Coefficient Estimation

Analog cosine input :
 $x(t) = A \cos(\omega t)$



Modulator 1-bit output stream

FFT

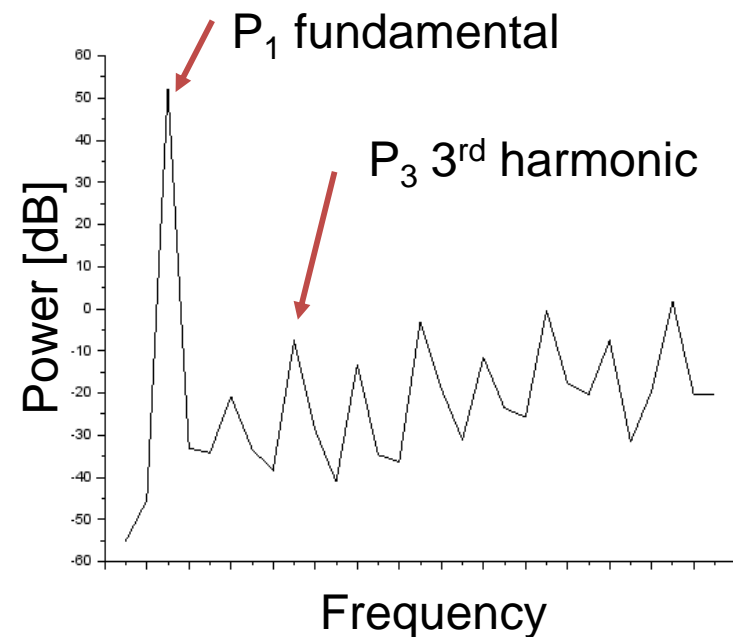


Measure fundamental &
 3rd harmonic power



Estimate a_1, a_3 :
 $y(t) = a_1 x(t) + a_3 x(t)^3$

Proposed algorithm



Fundamental / 3rd Harmonic Power and Polynomial Coefficients

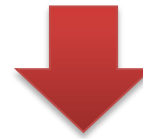
Cosine input :

$$x(t) = A \cos \omega t$$

Output characteristic model :

$$y(t) = a_1 x(t) + a_3 x(t)^3$$

$$y(t) = a_1 A \cos \omega t + a_3 (A \cos \omega t)^3$$



$$(a_1 A + \frac{3}{4} a_3 A^3) \cos \omega t + \frac{1}{4} a_3 A^3 \cos 3 \omega t$$



Fundamental



3rd harmonic

$$a_1 A + \frac{3}{4} a_3 A^3$$

$$\frac{1}{4} a_3 A^3$$

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Simulation Verification of Proposed Algorithm

Proposed $\Delta\Sigma$ ADC linearity test method



- Highly accurate estimation of polynomial coefficients from FFT values
- Modulator 1 bit data output of 2^{20}
 $2^{20} / (32 \times 1000) = 32$ seconds

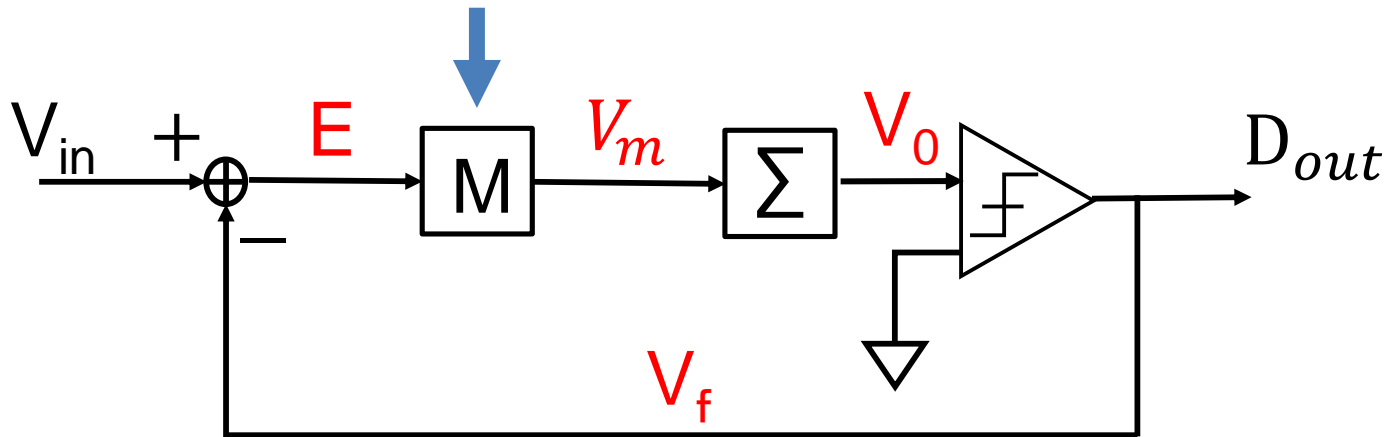


- Test time drastically reduced
- 32 pieces are tested in parallel simultaneously, equivalent testing time per unit is 1 second .

1st-order Modulator, 3rd-order Nonlinearity Model

3rd-order nonlinearity model

$$V_m = E - k * E^3 \quad (k > 0)$$



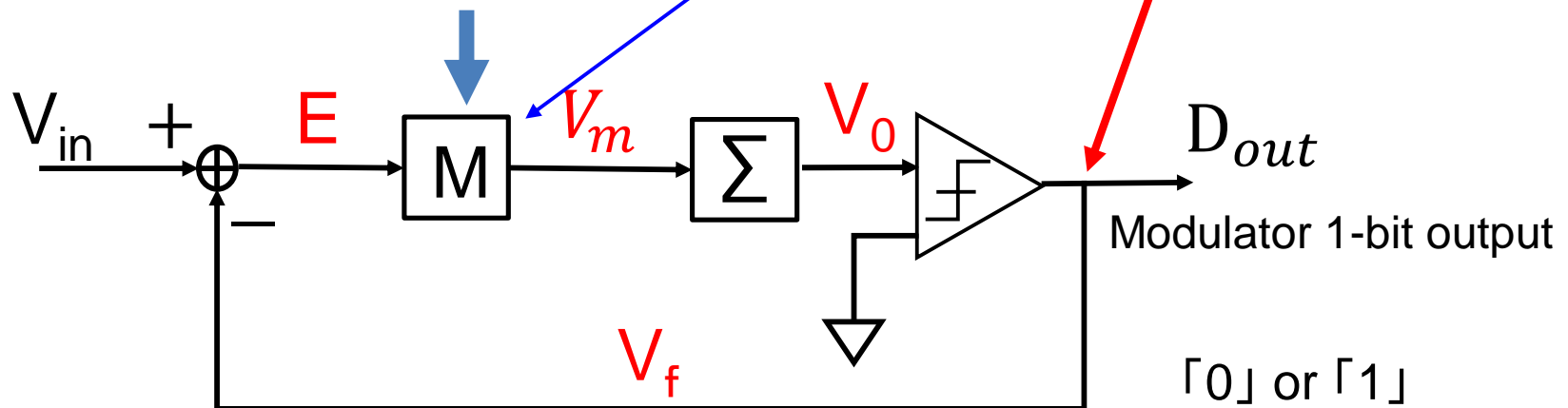
1st-order modulator

DC Input Simulation

- ◆ Number of data : $N=2^{20}$
- ◆ V_{in} : DC = -1.0 ~ +1.0
- ◆ $k = 0.0001, 0.0005, 0.001, 0.005, 0.01$

$$V_m = E - k * E^3 \quad (k > 0)$$

Control by the number of 1's



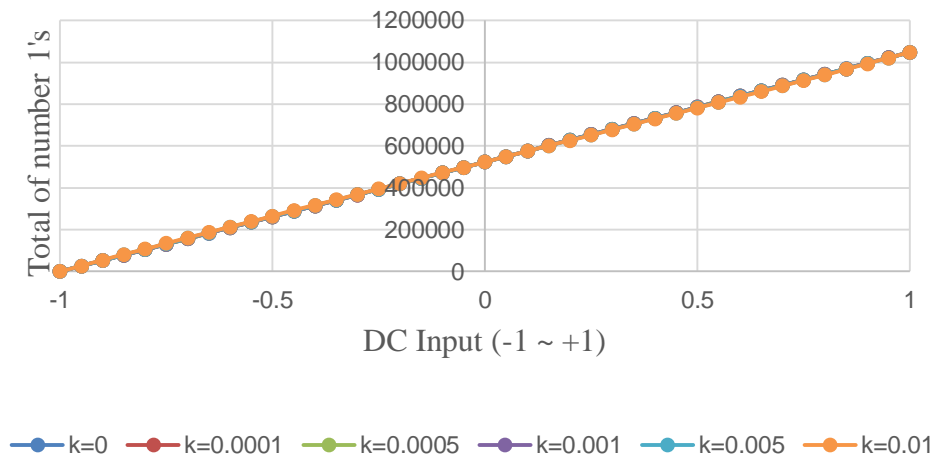
1st-order modulator

DC Input Simulation Result

Number of modulator output:

$$N=2^{20}$$

Number of output 1's

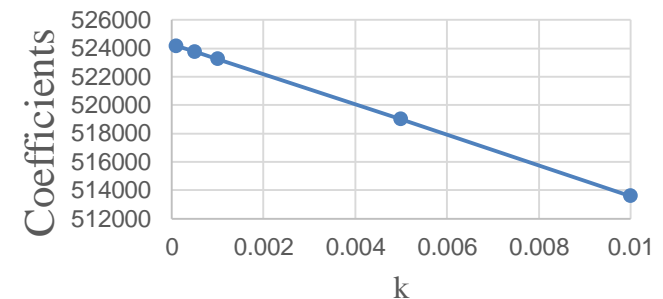


DC characteristic curve fitting

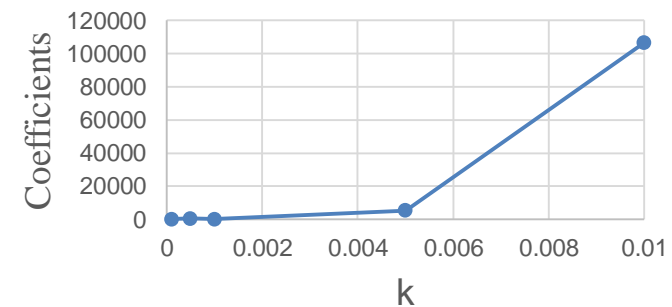


$$y = a_3 \cdot x^3 + a_1 \cdot x$$

a_1



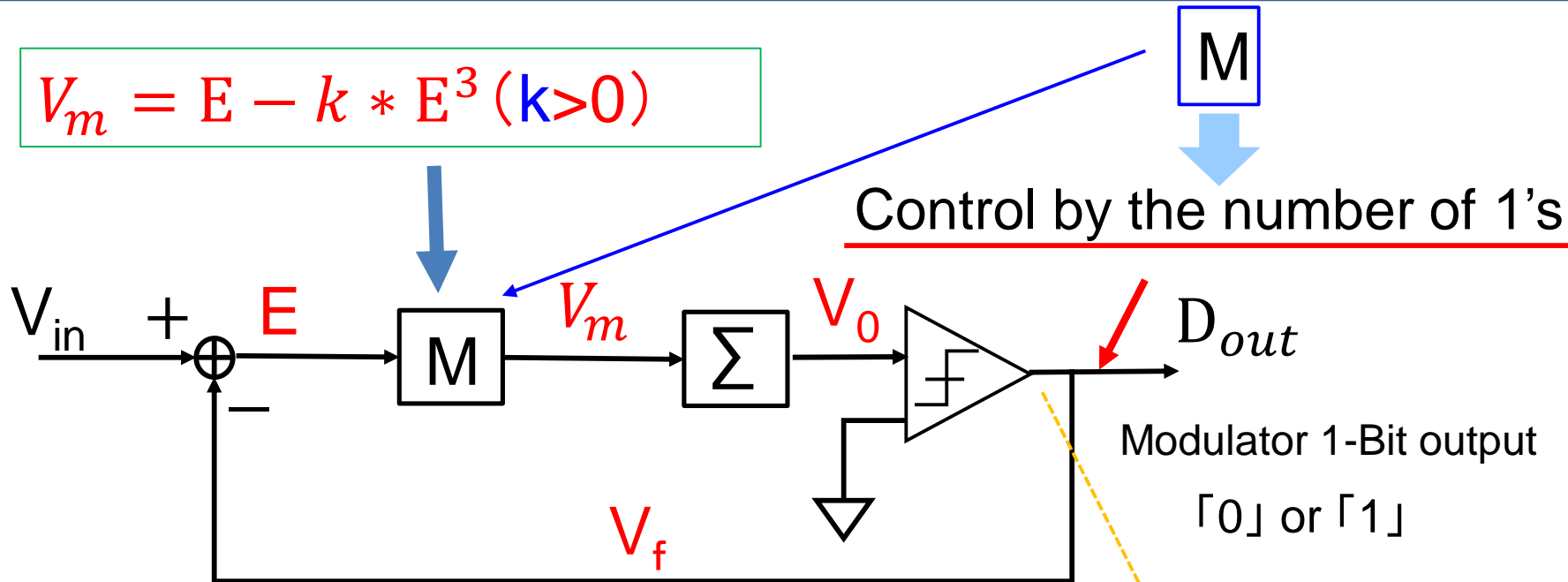
a_3



k	a_3	a_1
0.0001	104.84	524180
0.0005	524.48	523760
0.0010	1050.5	523240
0.0050	5282.5	519000
0.0100	10643.0	513610

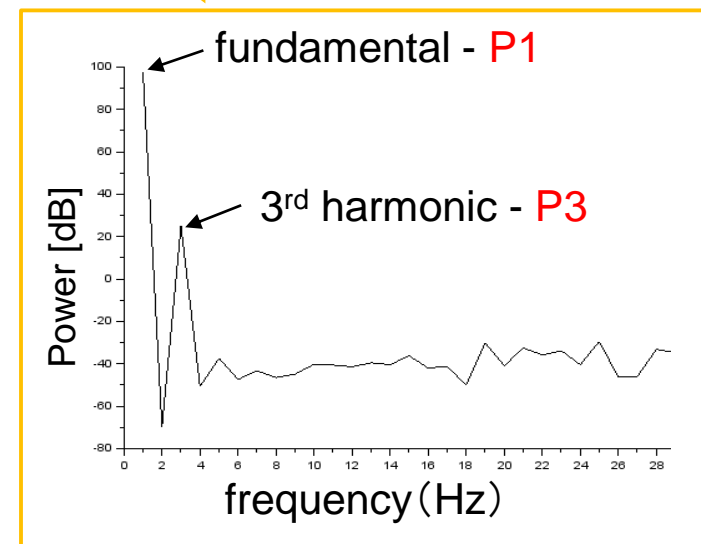
Cosine Input Simulation Configuration

$$V_m = E - k * E^3 \quad (k > 0)$$

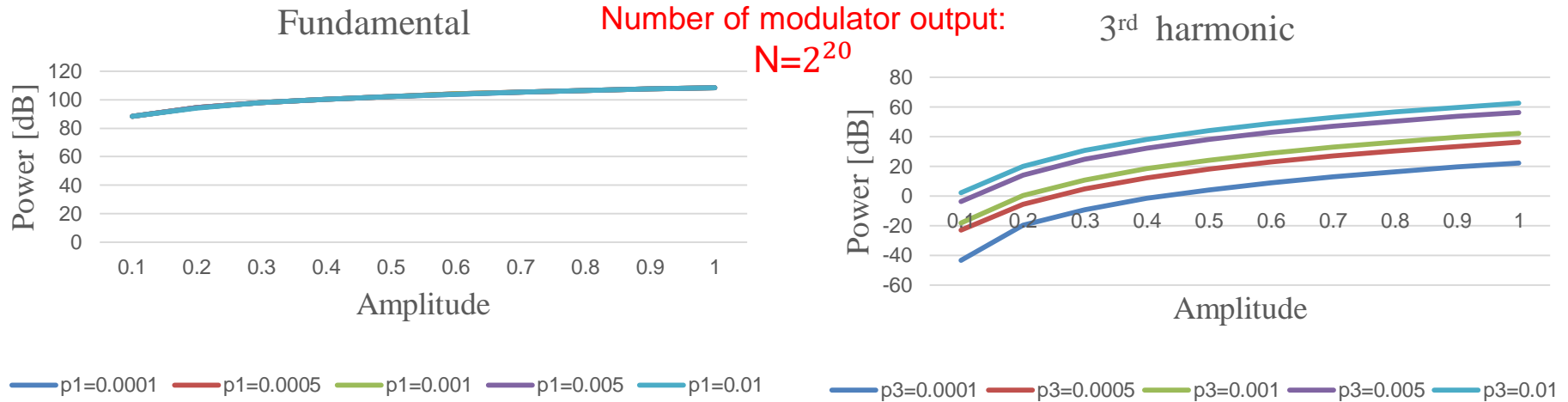


1st-order modulator

- ◆ Number of data : $N=2^{20}$
- ◆ $V_{in} : A\cos(\omega t)$ ($A = 0.1 \sim 1$)
- ◆ $k=0.0001, 0.0005, 0.001, 0.005, 0.01$



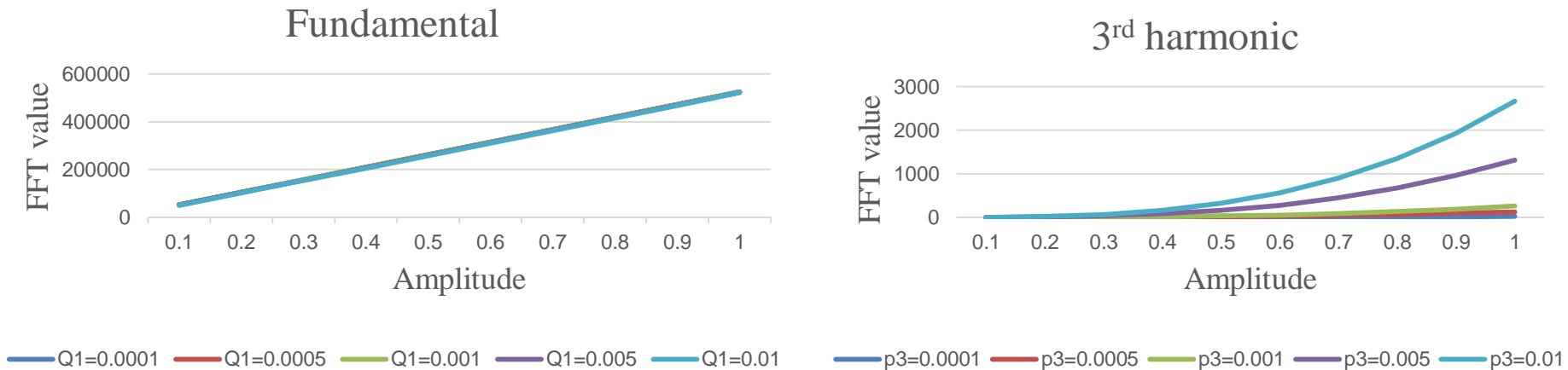
Cosine Input Simulation Result



$$\text{Power} = 20\log(\text{FFT}_{\text{value}}) - 6.02 \text{ [dB]}$$



FFT result



Find Spectrum Power from DC Characteristics

- ◆ 1st - order modulator
- ◆ Number of 1-bit output data :
 $N=2^{20}$

By nonlinearity

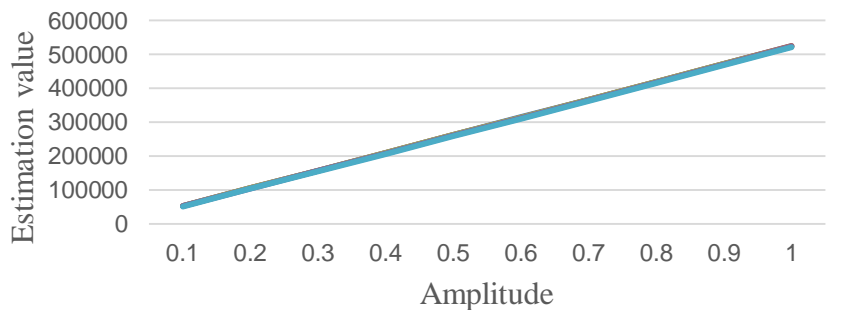
$$\text{Fundamental : } a_1 A + \frac{3}{4} a_3 A^3$$

$$\text{3rd harmonic : } \frac{1}{4} a_3 A^3$$

A: amplitude

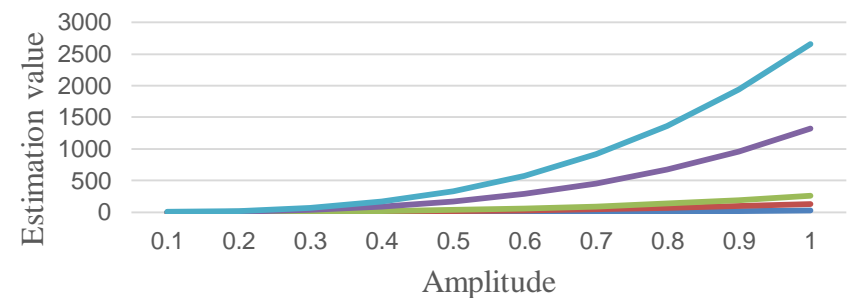
k	a_3	a_1
0.0001	104.84	524180
0.0005	524.48	523760
0.0010	1050.5	523240
0.0050	5282.5	519000
0.0100	10643.0	513610

Fundamental estimation value



— Q1=0.0001 — Q1=0.0005 — Q1=0.001 — Q1=0.005 — Q1=0.01

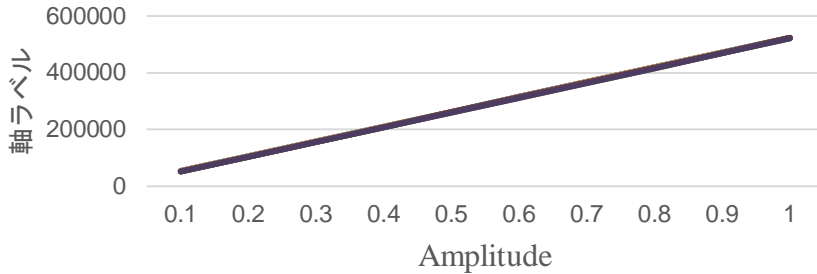
3rd harmonic estimation value



— Q3=0.0001 — Q3=0.0005 — Q3=0.001 — Q3=0.005 — Q3=0.01

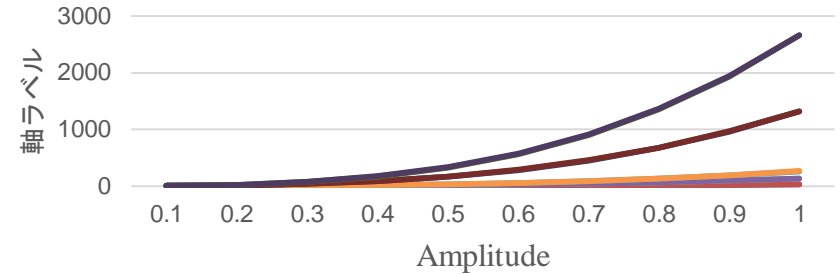
Comparison Between Estimated and FFT Values

Fundamental values



- p1=0.0001
- Q1=0.0001
- p1=0.0005
- Q1=0.0005
- p1=0.001
- Q1=0.001
- p1=0.005
- Q1=0.005
- p1=0.01
- Q1=0.01

3rd harmonic values



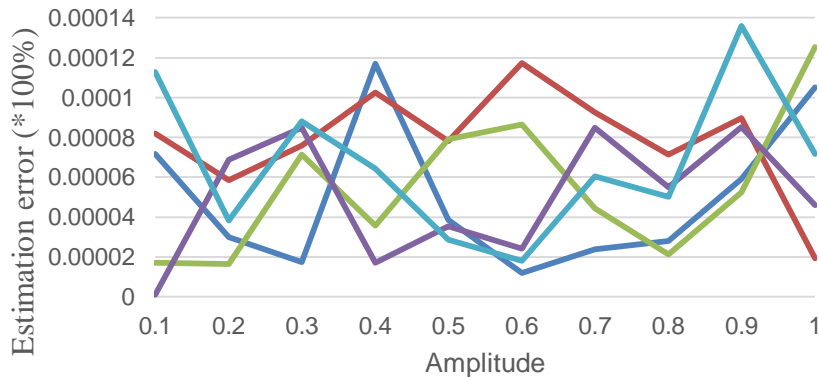
- p3=0.0001
- Q3=0.0001
- p3=0.0005
- Q3=0.0005
- p3=0.001
- Q3=0.001
- p3=0.005
- Q3=0.005
- p3=0.01
- Q3=0.01

P_1 : fundamental obtained by FFT
 Q_1 : estimated fundamental

$$\text{Error} = \frac{Q_{\text{values}} - P_{\text{values}}}{Q_{\text{values}}}$$

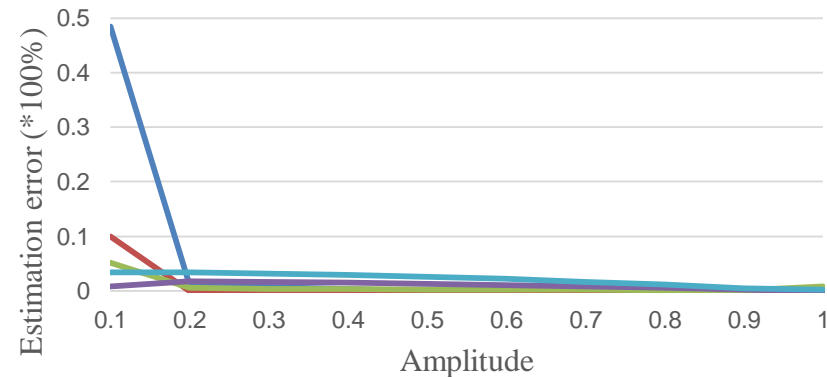
P_3 : 3rd harmonic obtained by FFT
 Q_3 : estimated 3rd harmonic

Estimation error of fundamental



- k=0.0001
- k=0.0005
- k=0.001
- k=0.005
- k=0.01

Estimation error of 3rd harmonic



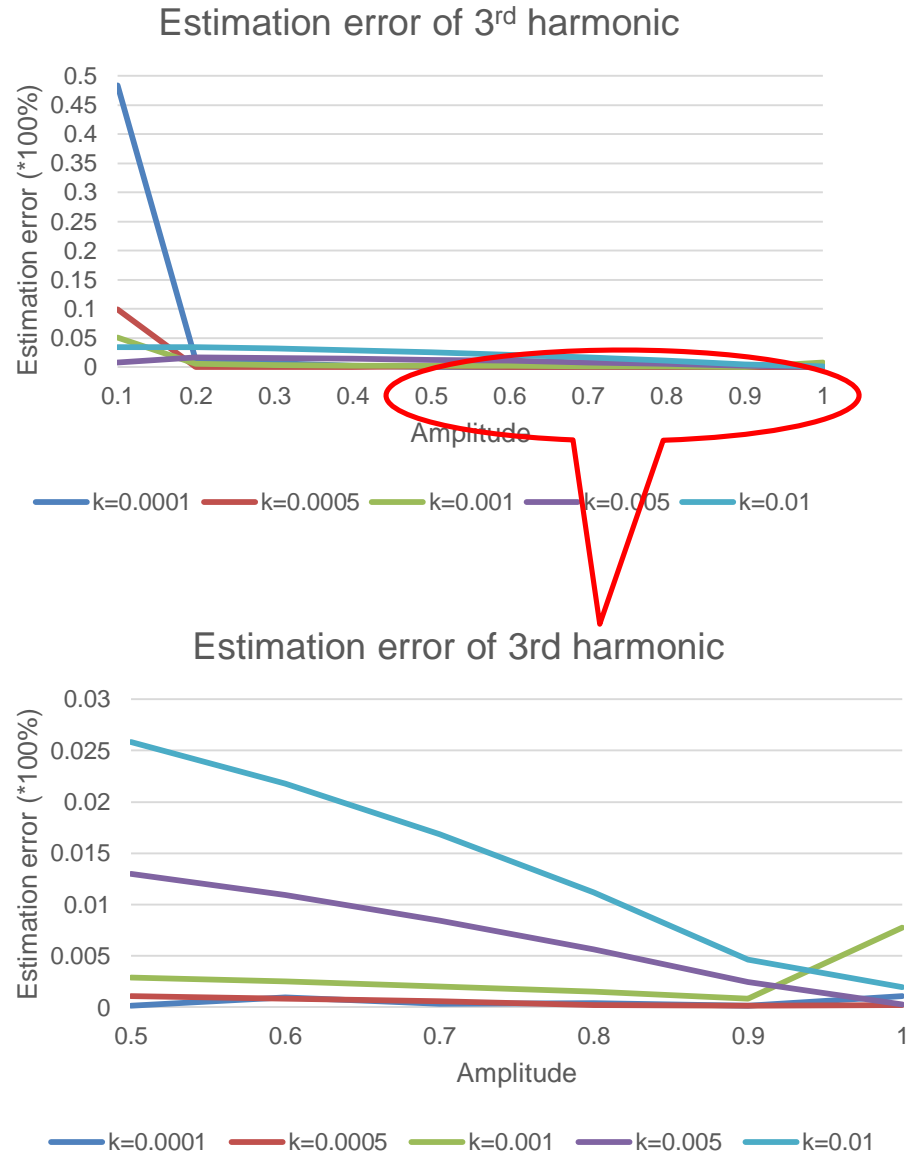
- k=0.0001
- k=0.0005
- k=0.001
- k=0.005
- k=0.01

$N=2^{20}$ Accurate Estimation Condition for 3rd Harmonic

1st -order modulator

Good condition
3rd harmonic

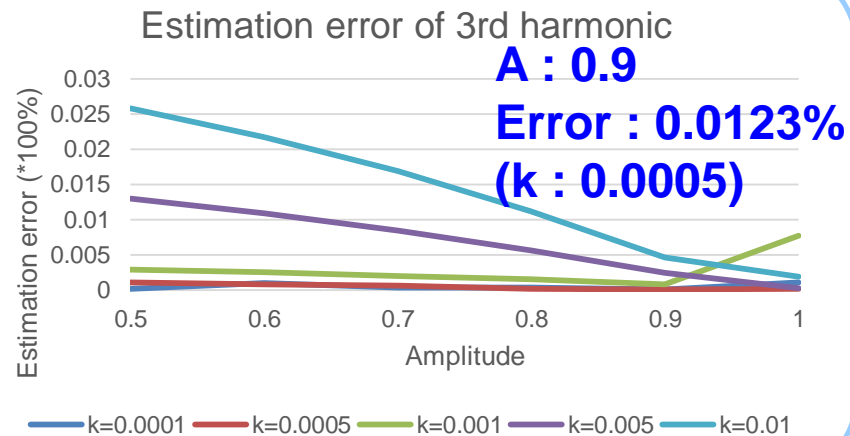
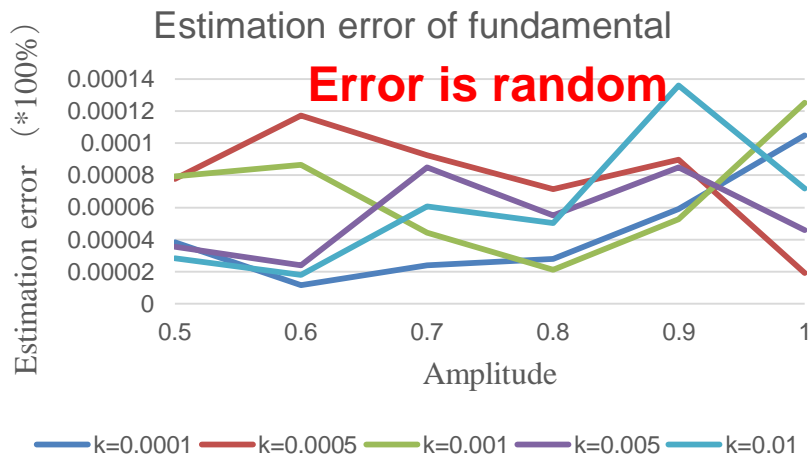
Amplitude = 0.9
Error = 0.0123%
($k = 0.0005$)



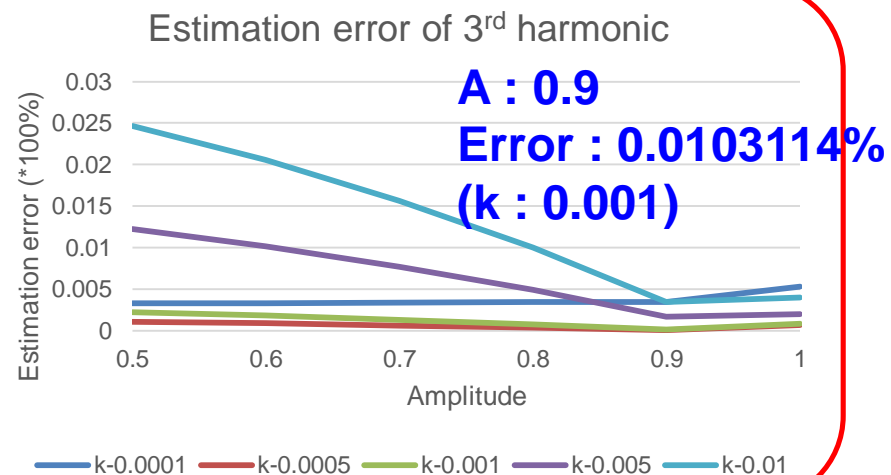
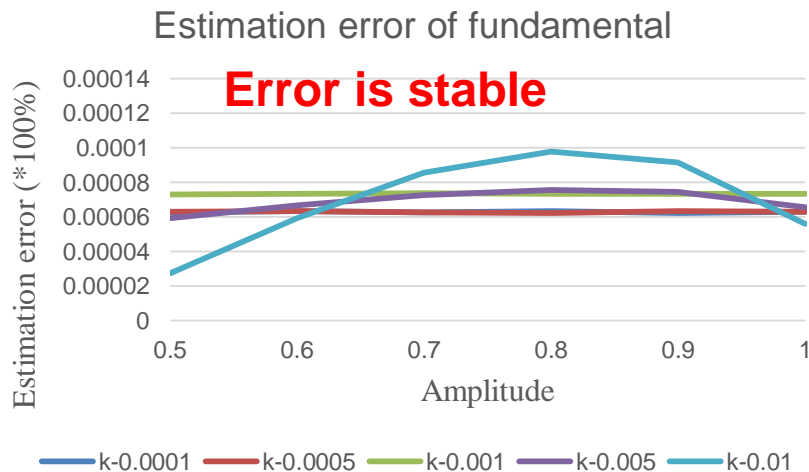
$N=2^{20}$

Comparison of 1st and 2nd -order Modulators

1st -order modulator

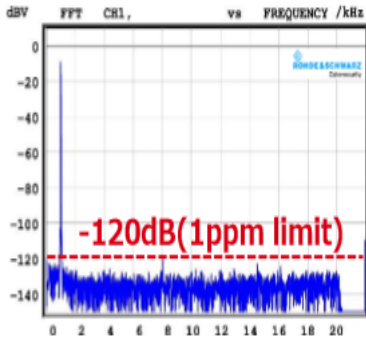


2nd -order modulator



DUT Measurement Result

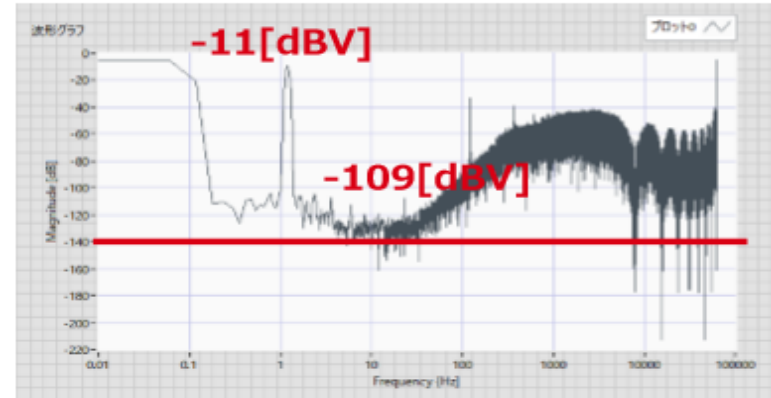
Measurements results from Rohm semiconductor company



Output : 1kHz 44.1ksps
 THD : 122dB(~Fifth Harmonics)
 SN : 132dB(Filter:20kHzLPF)

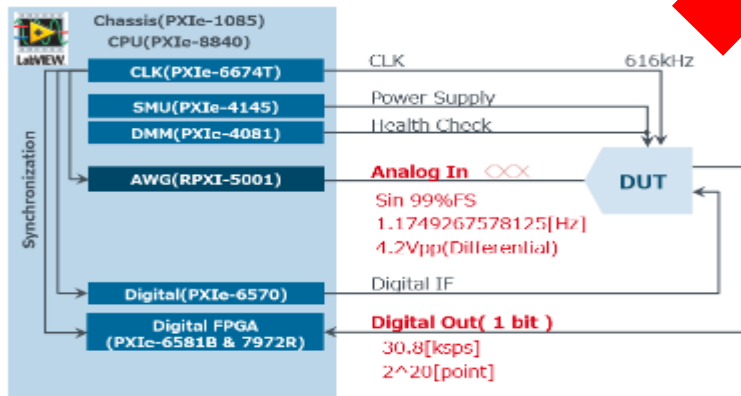
Meet the requirements

Signal from our developed AWG
 (AWG: Arbitrary Waveform Generator)

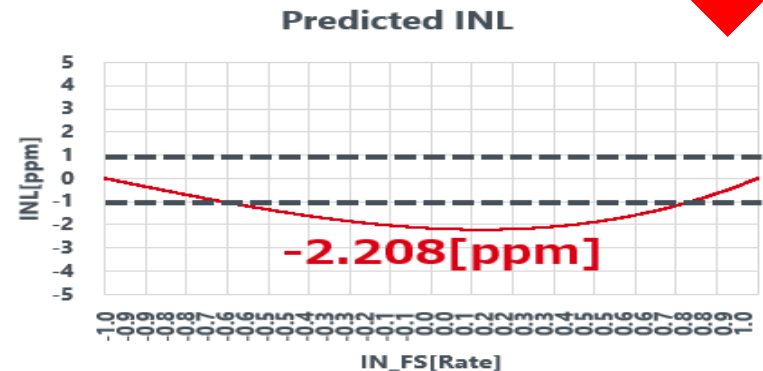


Experimental result of
 the modulator output FFT

Test System Diagram and Test Condition



Use of NI PXI system
 for experiment



Obtained INL prediction
 with the proposed method

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Conclusion

- High resolution, low speed $\Delta\Sigma$ ADC linearity short time testing algorithm
- ✓ Polynomial modeling of modulator input / output characteristics
- ✓ FFT of modulator 1-bit output stream for cosine input
- ✓ Estimate polynomial coefficients from fundamental and harmonic powers
- Verified by simulation and experiments that the proposed method is feasible.

Drastic testing time reduction:

104days  32 seconds

Future Work

Consideration of the followings:

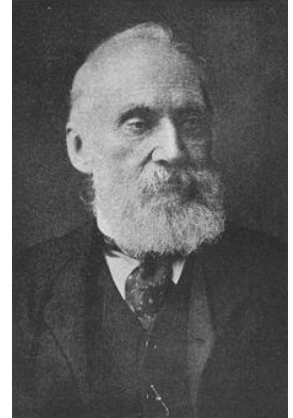
- Higher-order distortions
 - ➔ High-order polynomial modeling
- Application to high-order modulators
- Application to multi-bit modulators

Final Statement

No Science without Measurement



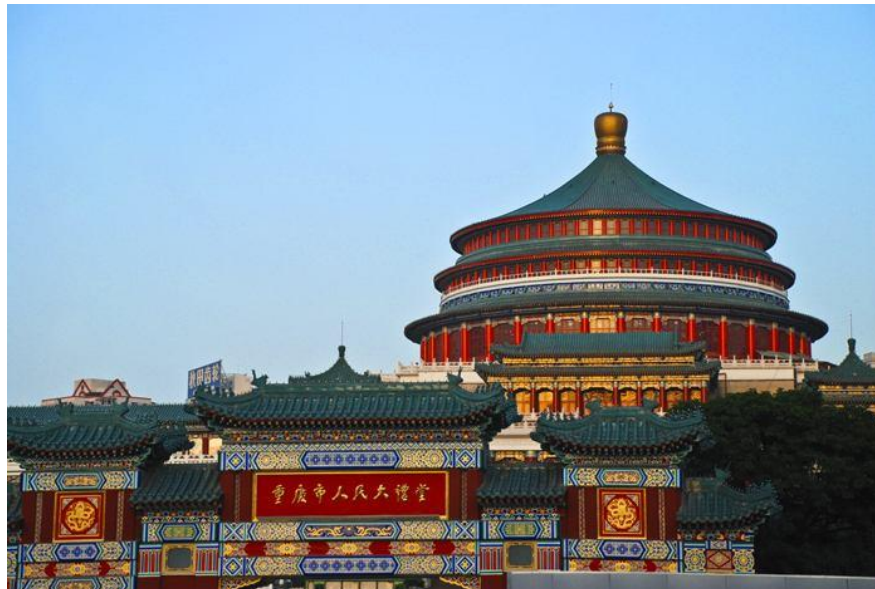
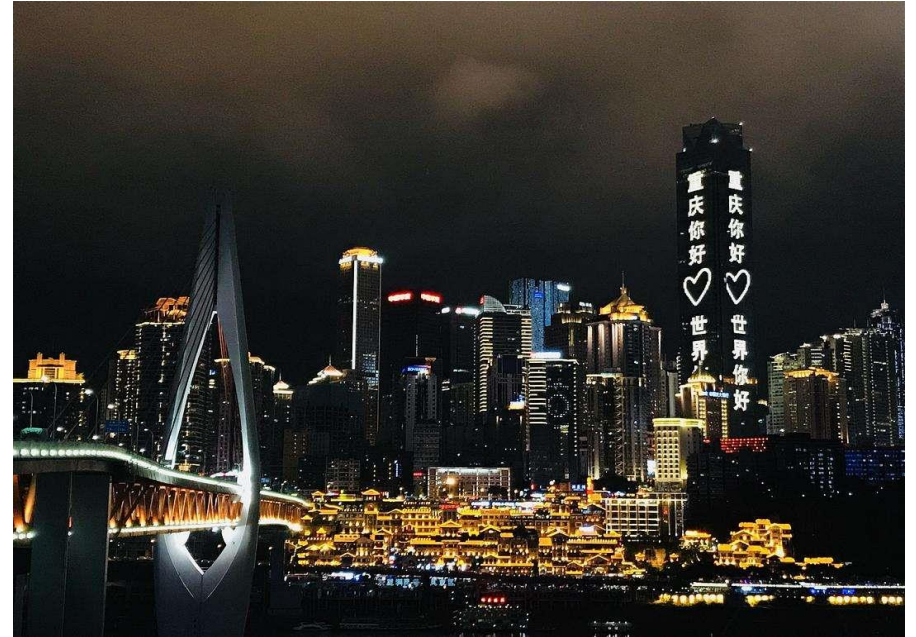
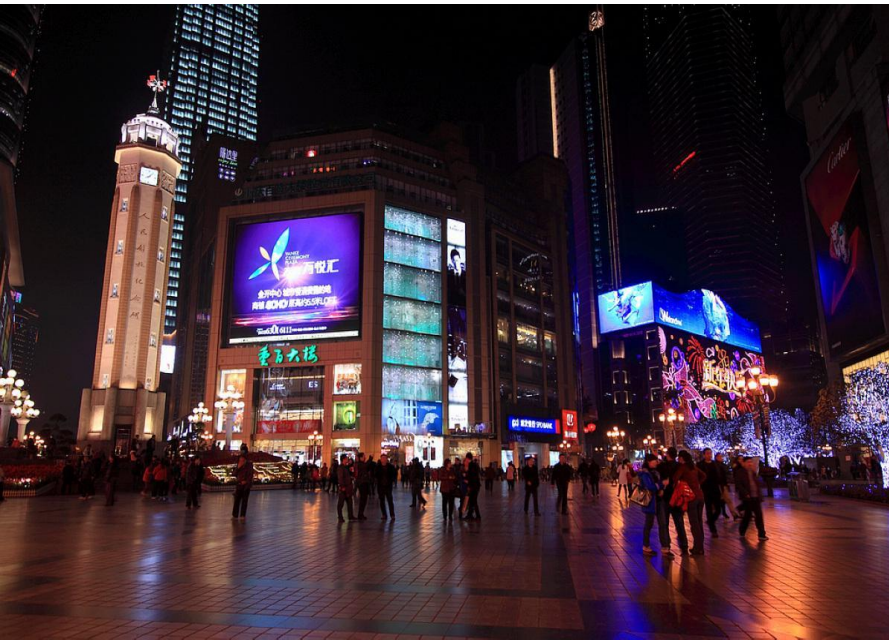
No Production without Testing



Lord Kelvin

Kelvin PMP

Thanks for listening!



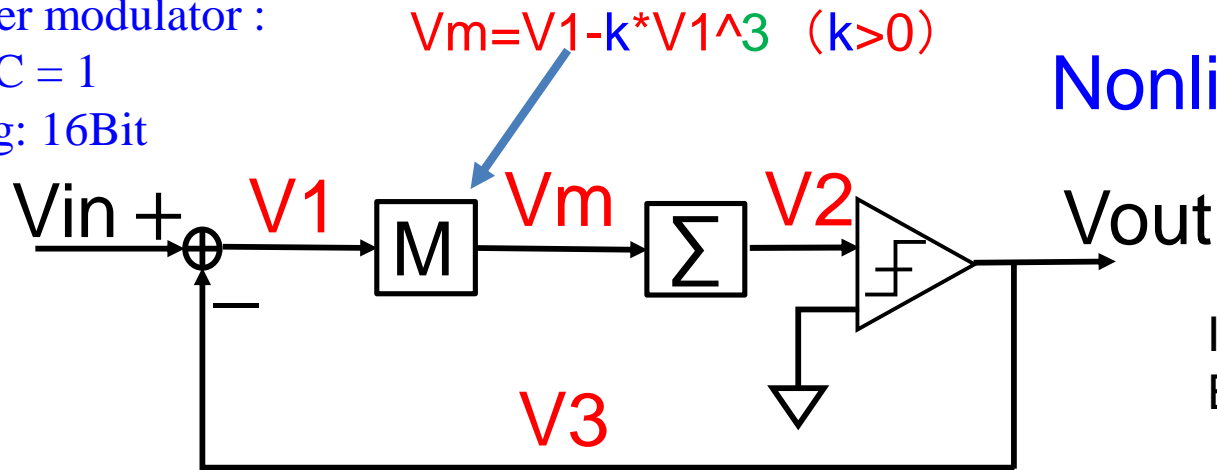
Appendix

DC Input Amplitude

First order modulator :

Input: DC = 1

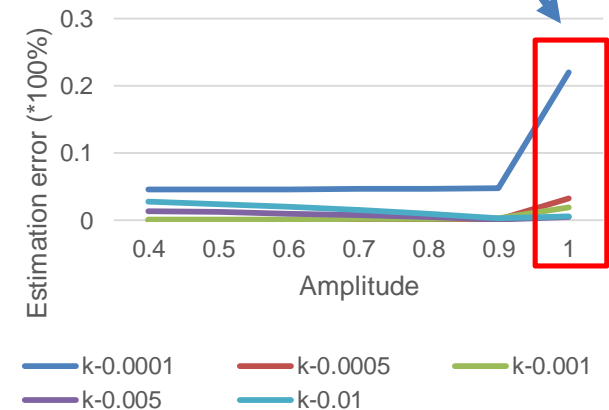
Sampling: 16Bit



Nonlinearity Model

If $A=1$
Estimation error

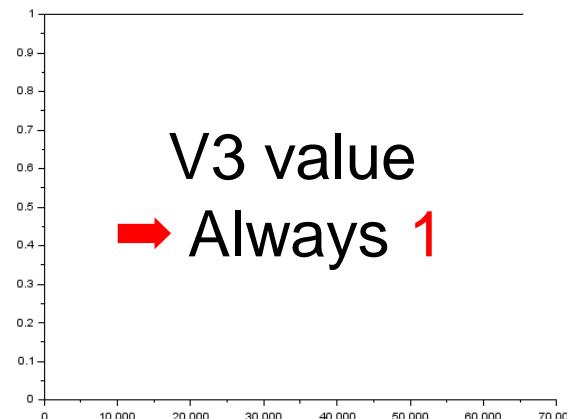
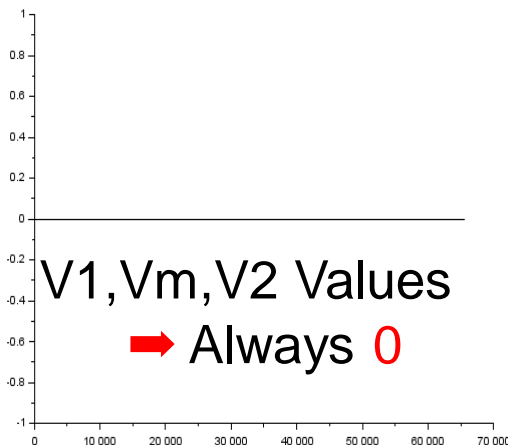
become bigger



$$V_1(i) = V_{in}(i) - V_3(i)$$

$$V_m(i) = V_1(i) - k \cdot V_1(i)^3 \quad (K > 0)$$

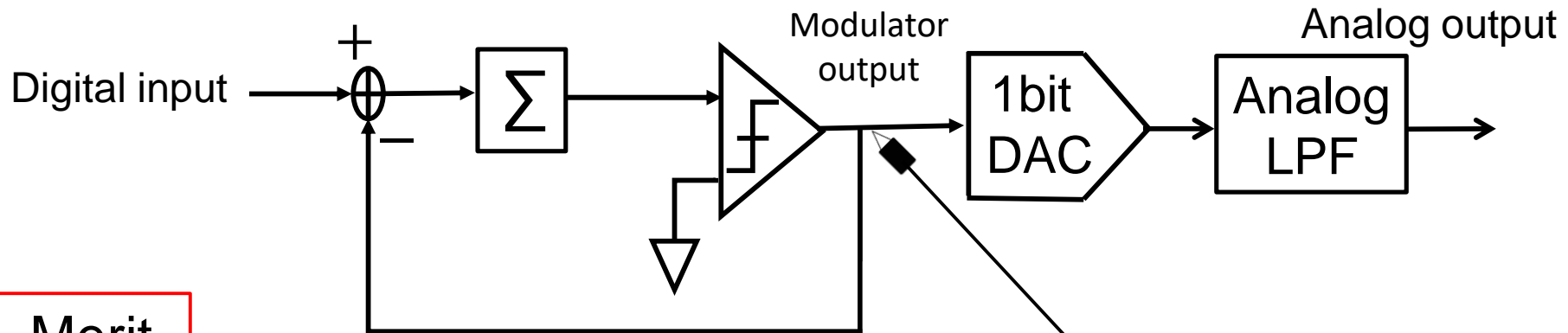
$$V_2(i) = V_2(i-1) + V_m(i)$$



So, $A=1$.

→ It can't be modulator.

Merits & Demerits of $\Delta\Sigma$ DAC



Merit

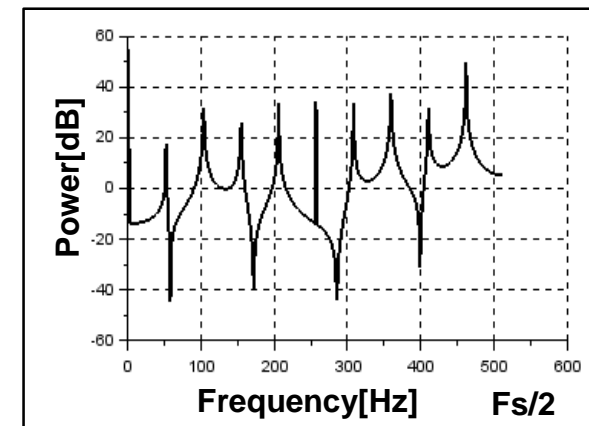
- Mostly digital circuit
- High linear & high resolution for low frequency signal generation

Demerit

- Limit cycle problem for small input



Limit cycle



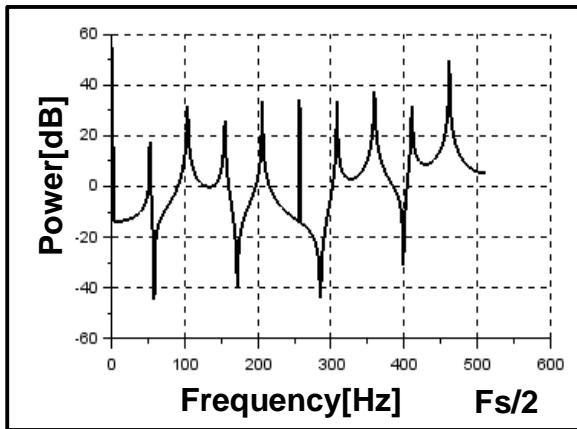
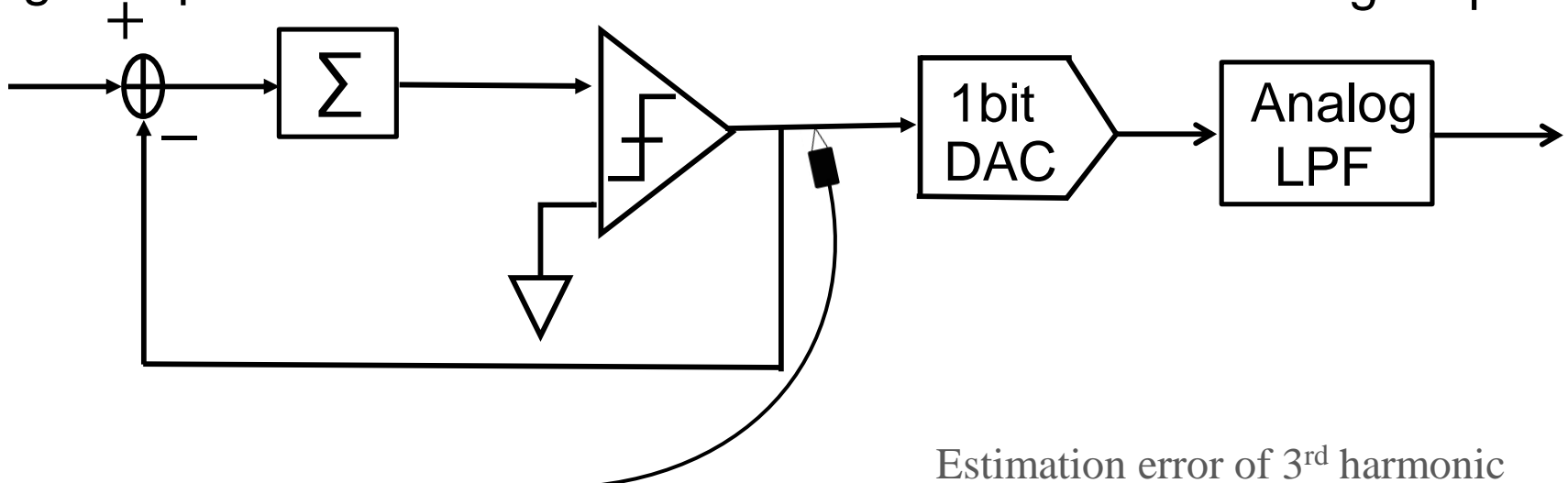
✘ Due to modulator nonlinearity by quantizer

DC small signal input

Small signal input

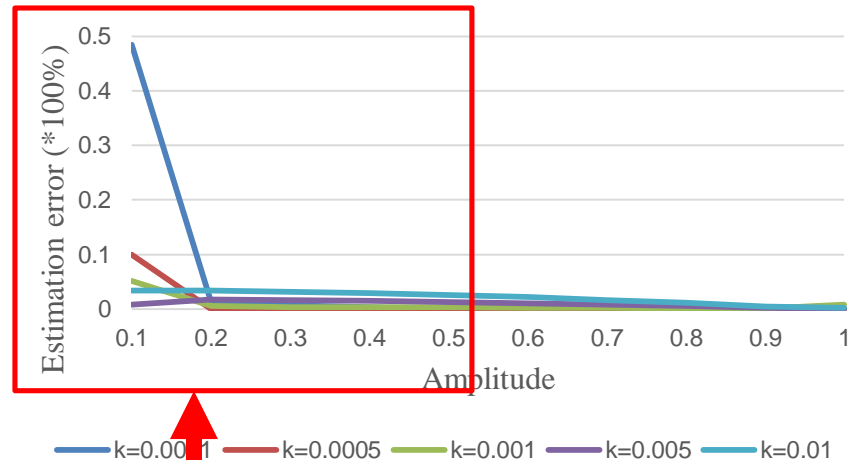
Digital input

Analog output

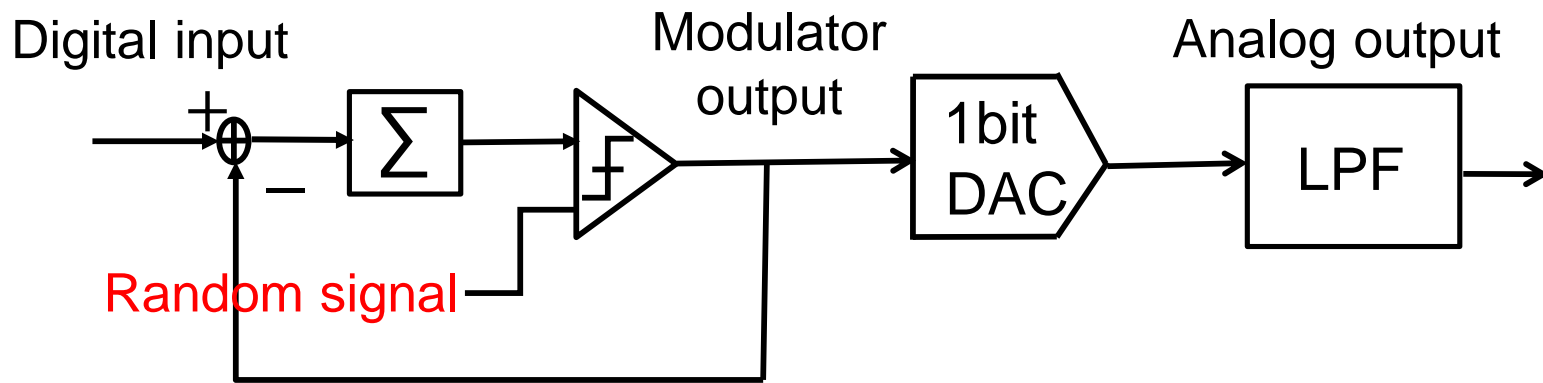


Limit cycle

Estimation error of 3rd harmonic



Limit cycle solution



< Features >

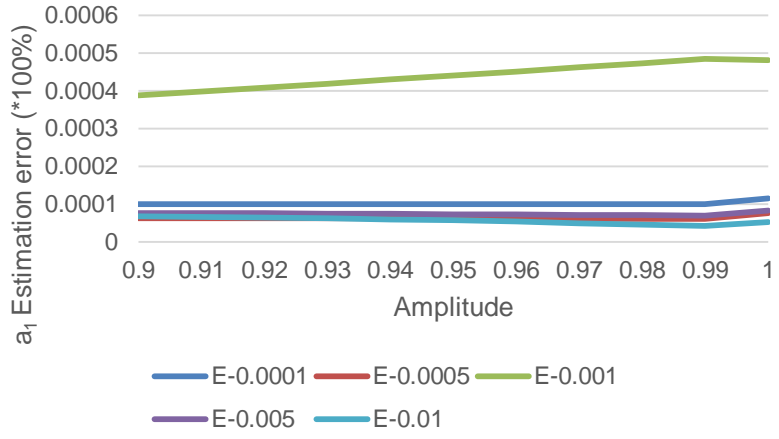
- ① NOT sacrifice input range
- ② NOT affect signal band, thanks to noise-shaping
- ③ Easily generate random signal.

First-order modulator (3rd nonlinearity)

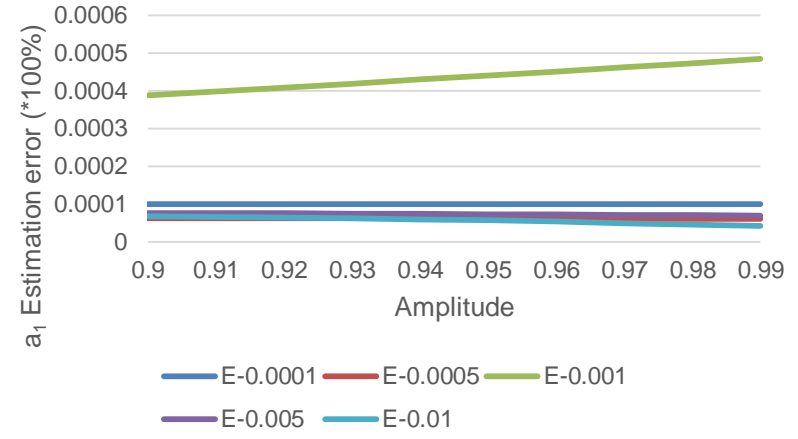
fundamental

Sampling:18Bit A : 0.9 ~ 1 amplitude increase step:0.01

The fundamental estimation error of 18Bit

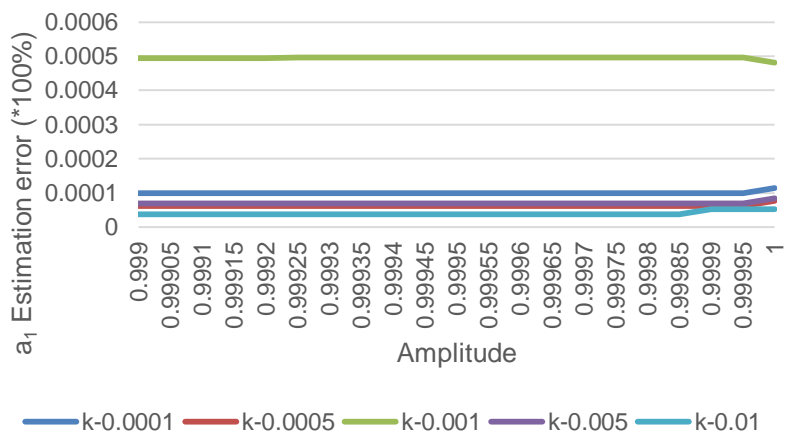


The fundamental estimation error of 18Bit

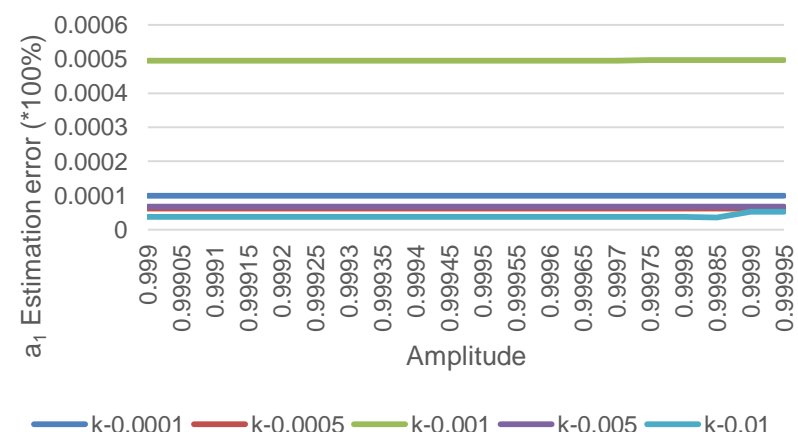


Sampling:18Bit A : 0.999 ~ 1 amplitude increase step:0.0005

The fundamental estimation error of 18bit



The fundamental estimation error of 18Bit

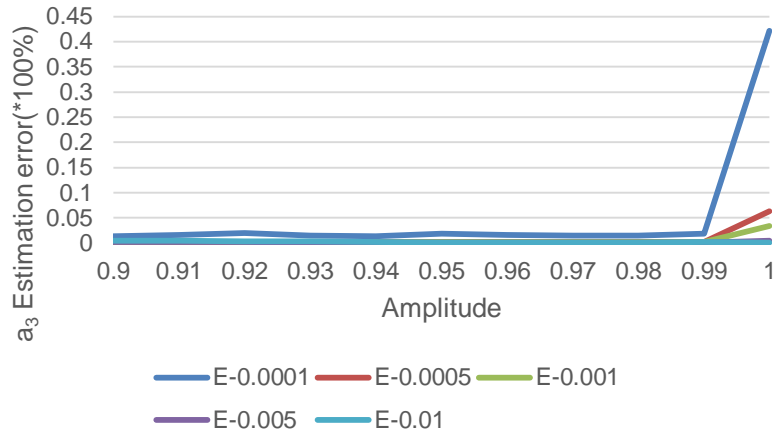


First-order modulator (3rd nonlinearity)

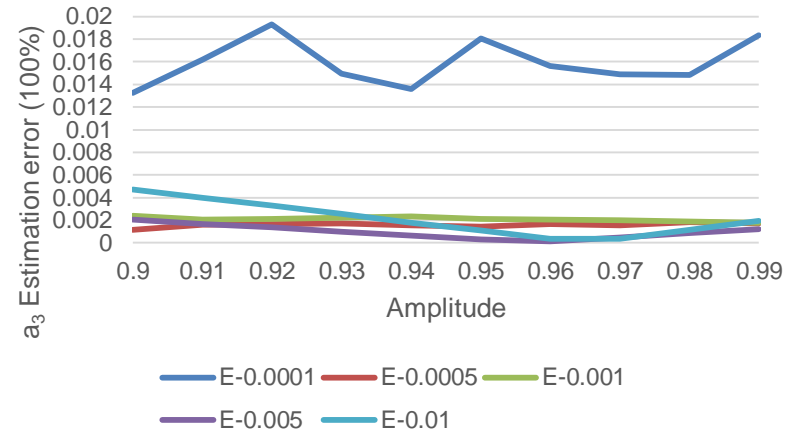
3rd harmonic

Sampling:18Bit A : 0.9 ~ 1 amplitude increase step:0.01

The 3rd harmonics estimation error of 18Bit

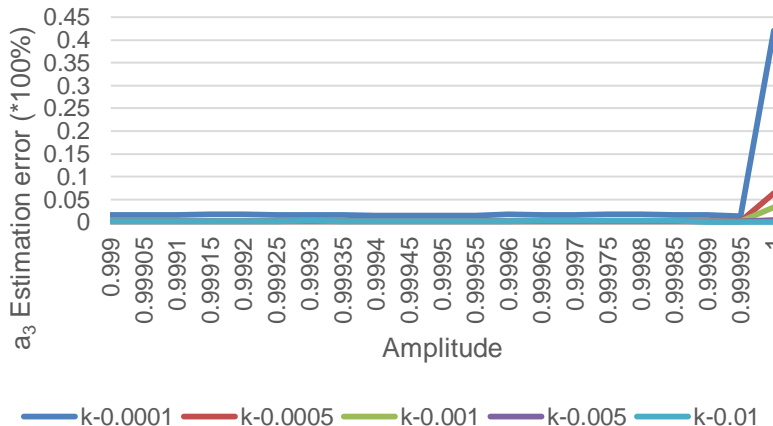


The 3rd harmonics estimation error of 18Bit

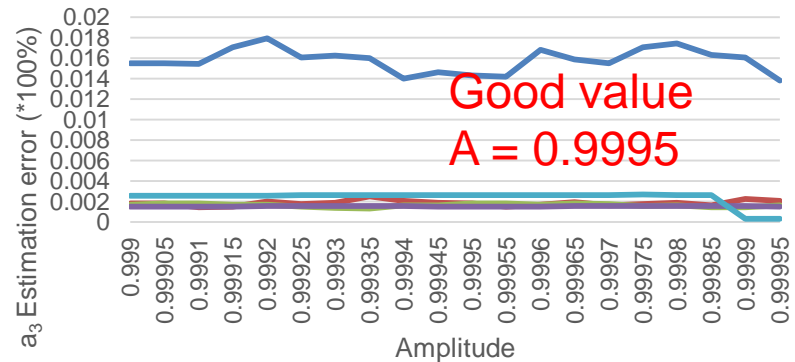


Sampling:18Bit A : 0.999 ~ 1 amplitude increase step:0.0005

The 3rd harmonic estimation error of 18Bit



The 3rd harmonics estimation error of 18Bit



First-order modulator

3rd harmonic

