

Multi-Phase Full/Half Wave Type Resonant Converter with Automatic Current Balance against Element Variation

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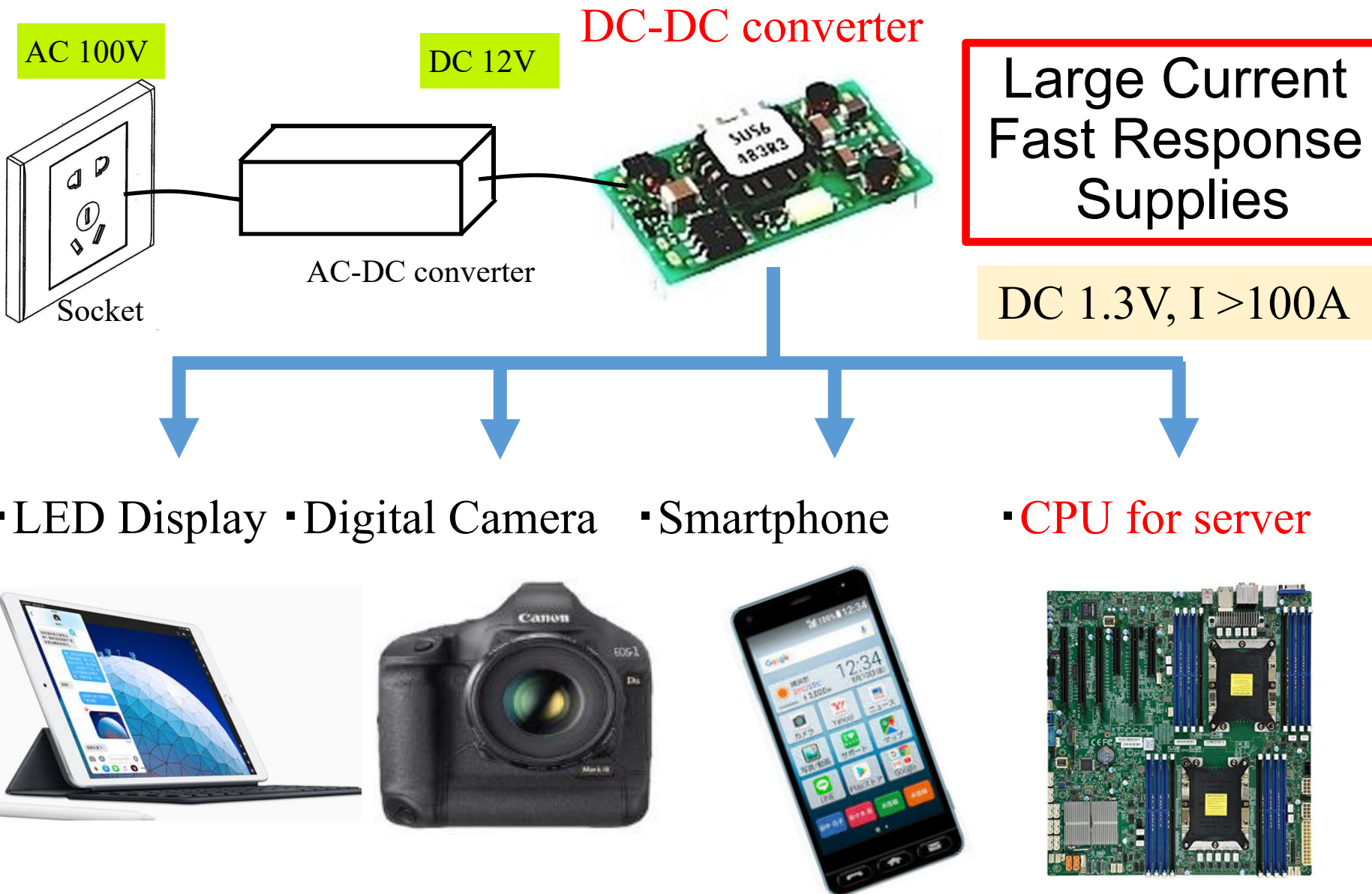
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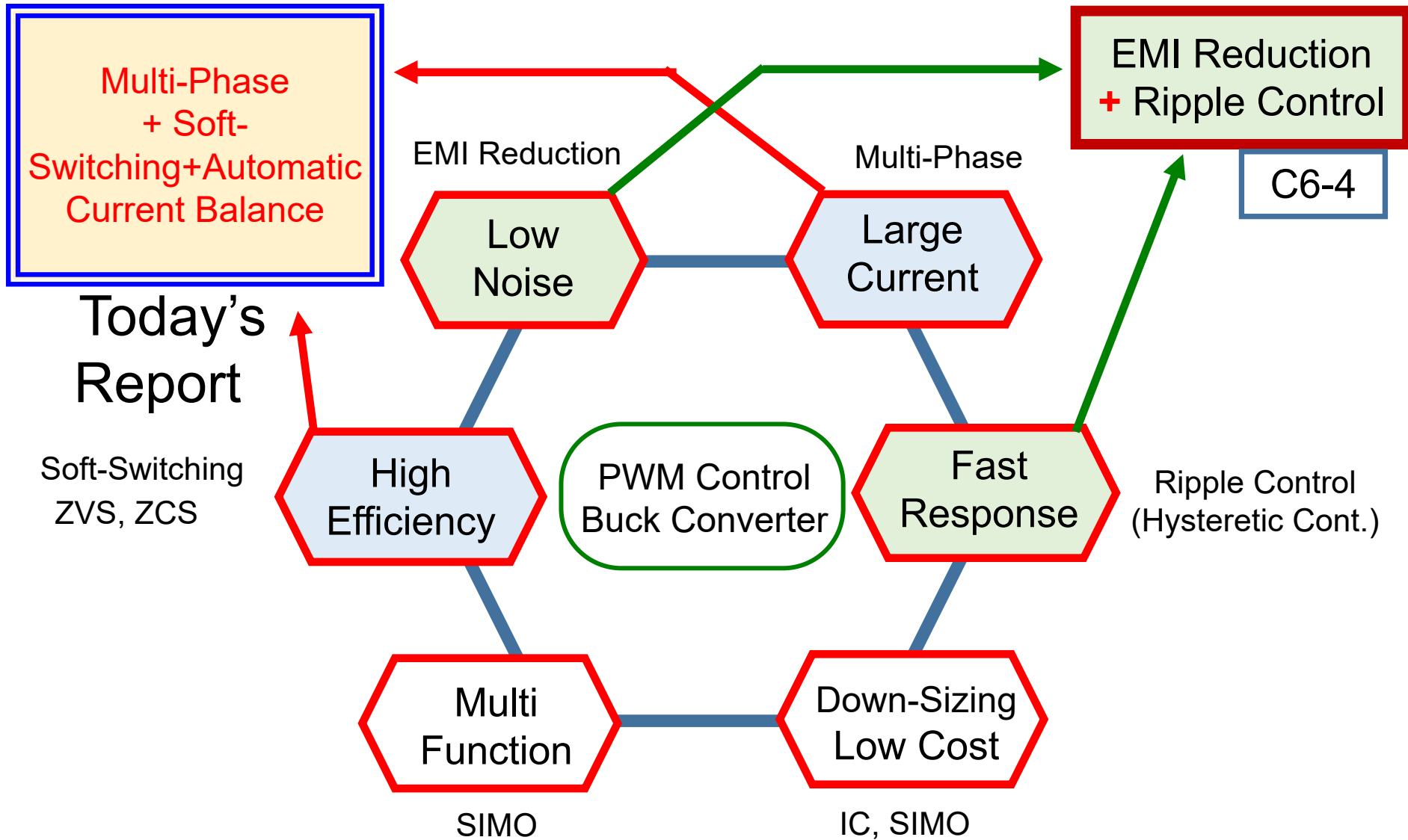


- Research background
- Full/Half wave type soft switching converter
- Multi-phase soft switching converter
- Automatic current balance technology
- Conclusion

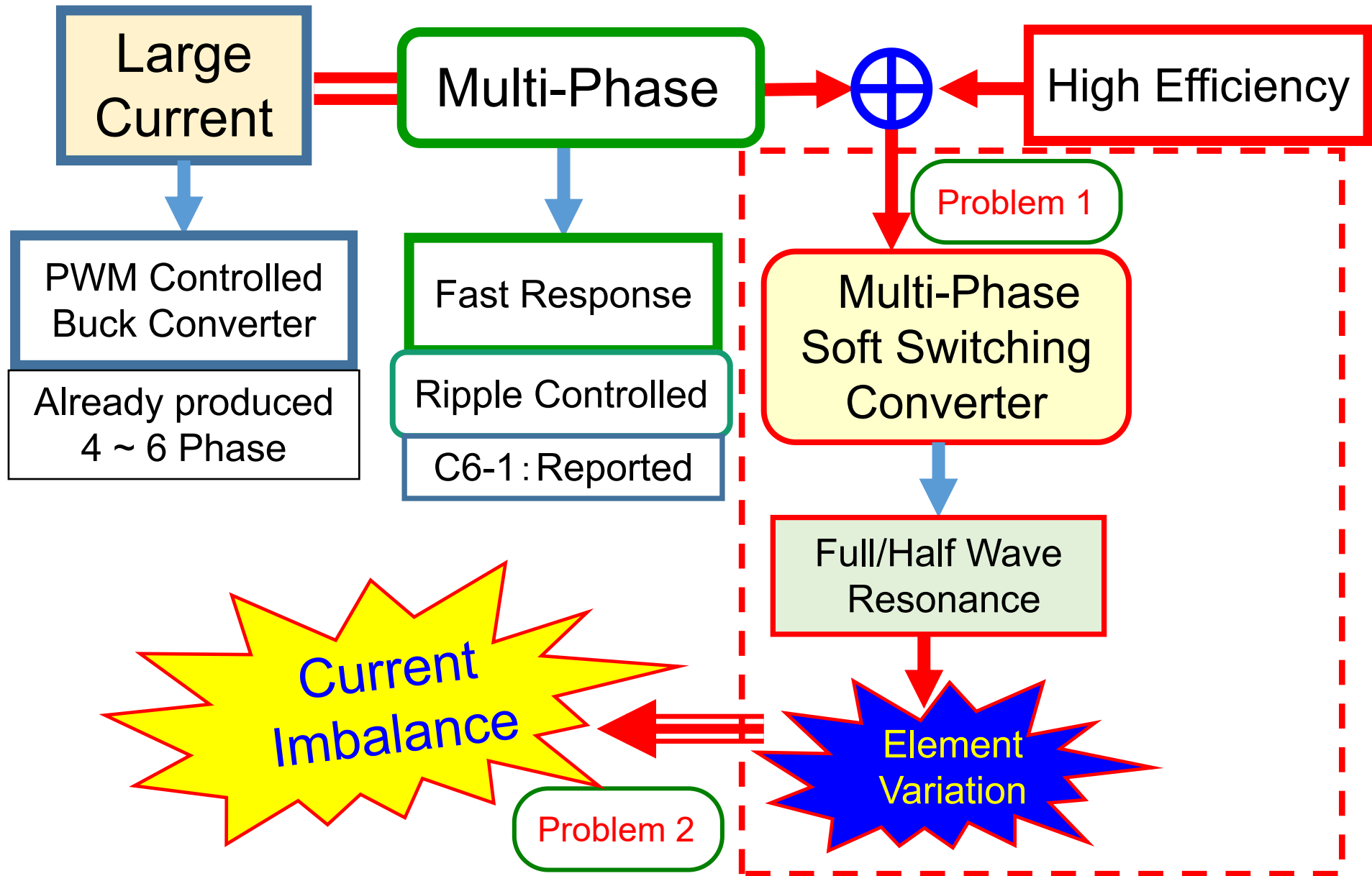
- **Research background**
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Research Background





Today's Presentation



Research Objective

Objective

Development of power supply with

- Multi-phase soft switching converters with full or half wave resonance
- Automatic current balance technology against resonant element variation

Technical Problems

- 1) How to configurate the multi phase constructions when there is no fixed clock pulse?
- 2) How to control the current balance automatically?

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Soft Switching Converter (Full Wave)

Soft Switching Converter with Full Wave Resonance

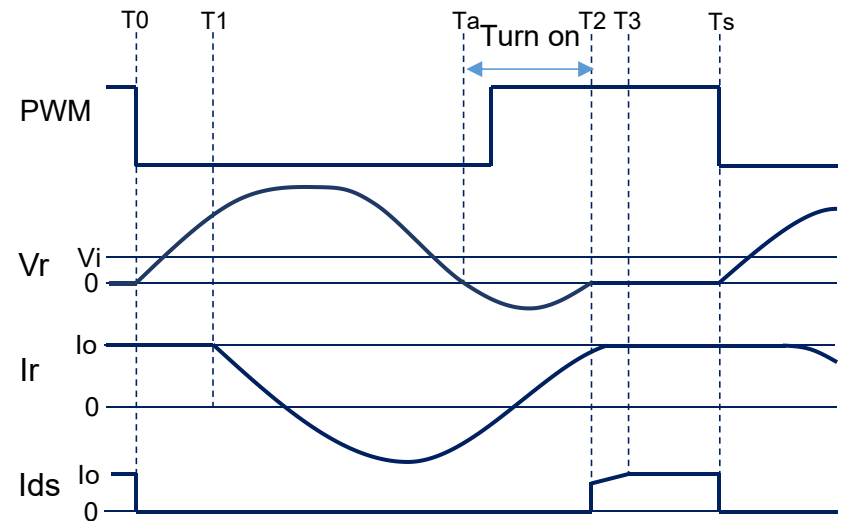
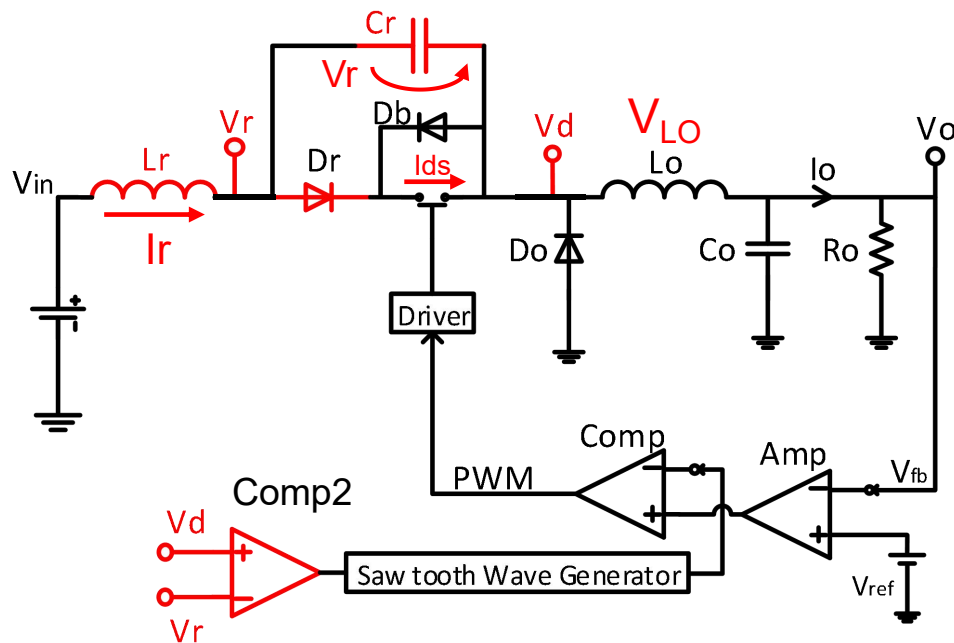


Fig. Full wave soft switching converter

Fig. Signals of full wave converter

- * Resonant elements L_r , C_r , D_r are added.
- * SW turns ON at $V_r = V_d$.
- * $V_o = D \cdot V_i$: D is the duty ratio of PWM.

- * Conditions: $F = 760\text{kHz}$
 $V_i = 12\text{V}$, $V_o = 7.0\text{V}$, $I_o = 1.0\text{A}$
 $L_o = 50\mu\text{H}$, $C_o = 470\mu\text{F}$
 $L_r = 20\mu\text{H}$, $C_r = 100\text{pF}$

Soft Switching Converter (Half Wave)

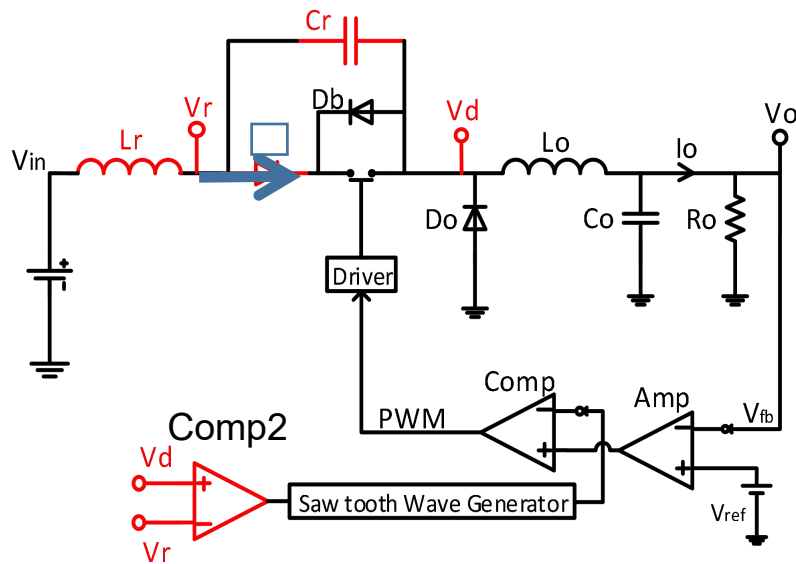


Fig. Half wave soft switching converter

- * Resonant Dr is deleted.
- * SW turns ON at $V_r = V_d$ but V_o is not $= D \cdot V_i$
(D is duty ratio of PWM)

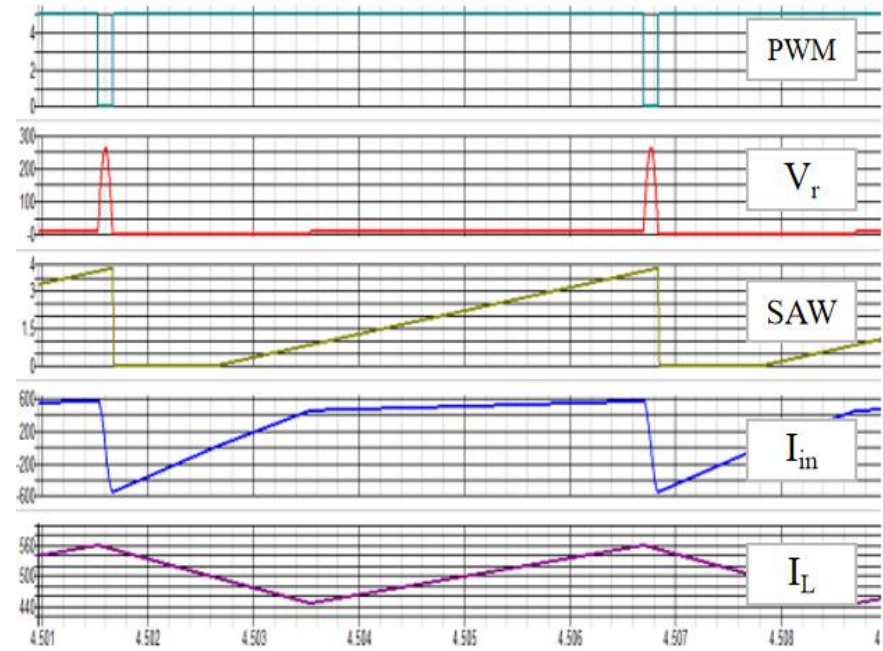
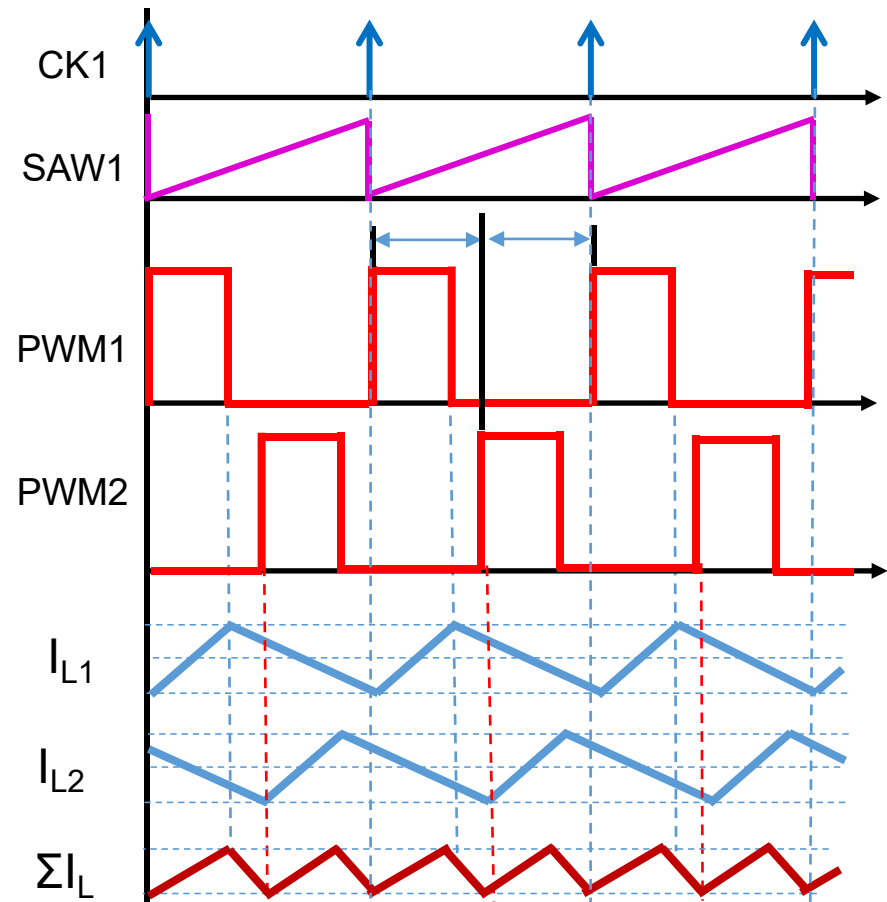
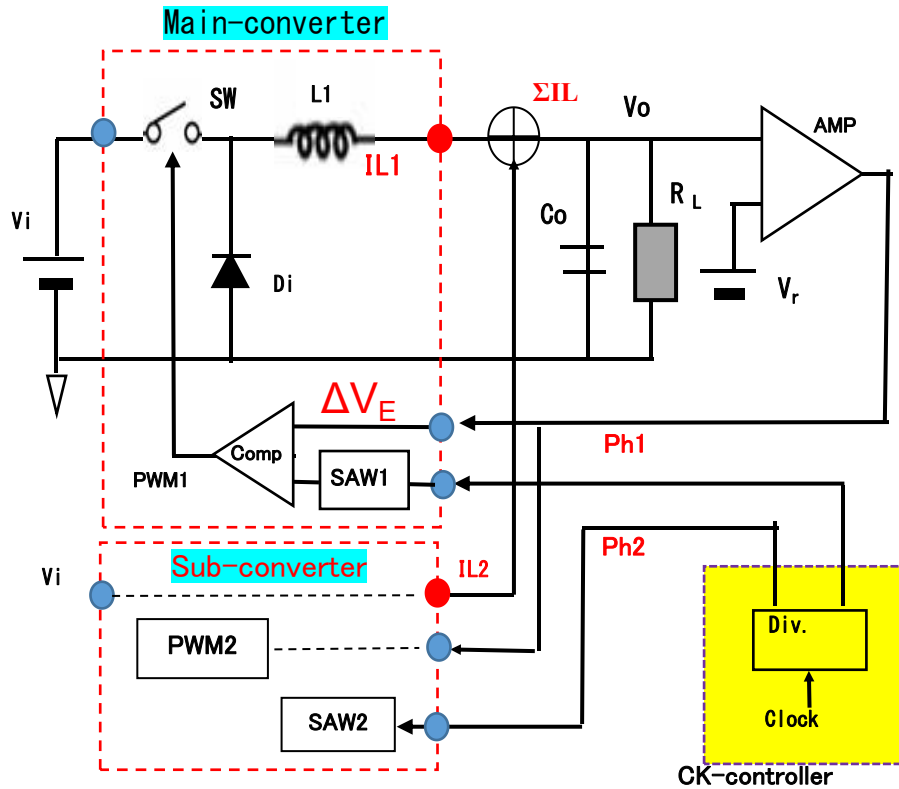


Fig. Signals of half wave converter

- * PWM Duty shows period of T_{OFF} .
- * Duty ratio is represented by inductor current.
- * Operation frequency depends on output current I_o .

- Research background
- Full/Half wave type soft switching converter
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- Automatic current balance technology
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Multi Phase Buck Converter



★ Two-phase is provided by Flip-Flop which divides the clock pulse.

* PWM2 is opposite phase.
* Ripple of ΣI_L is half of I_{L1} .

Dual-Phase Soft-switching Converter

- Opposite phase is generated like ripple-controlled converter.

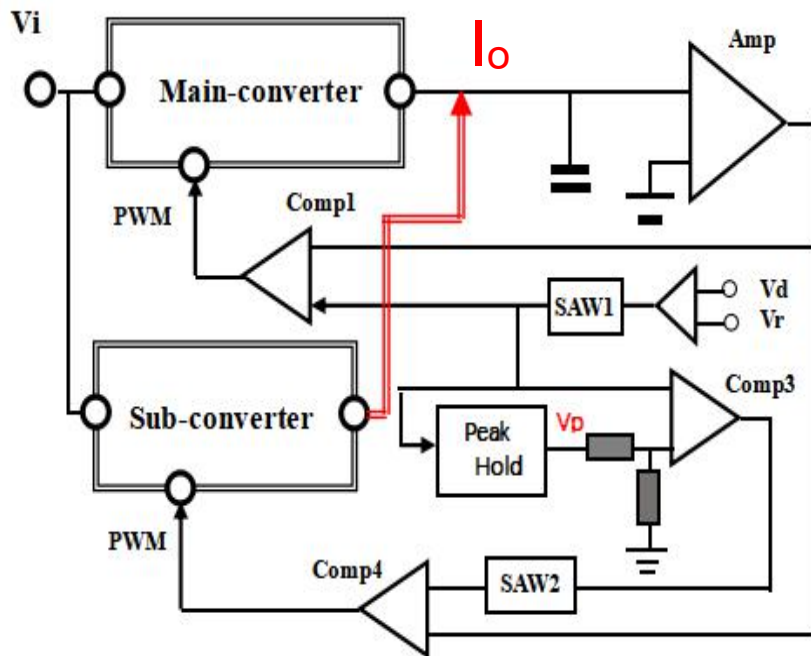
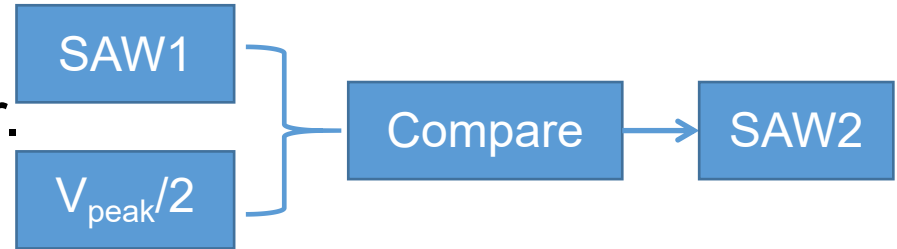


Fig. Dual phase switching converter

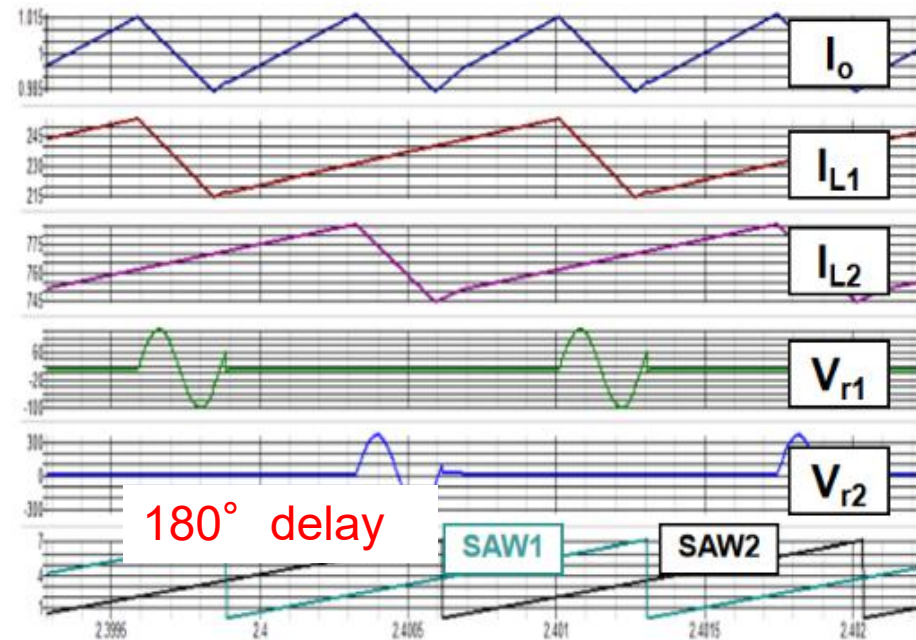
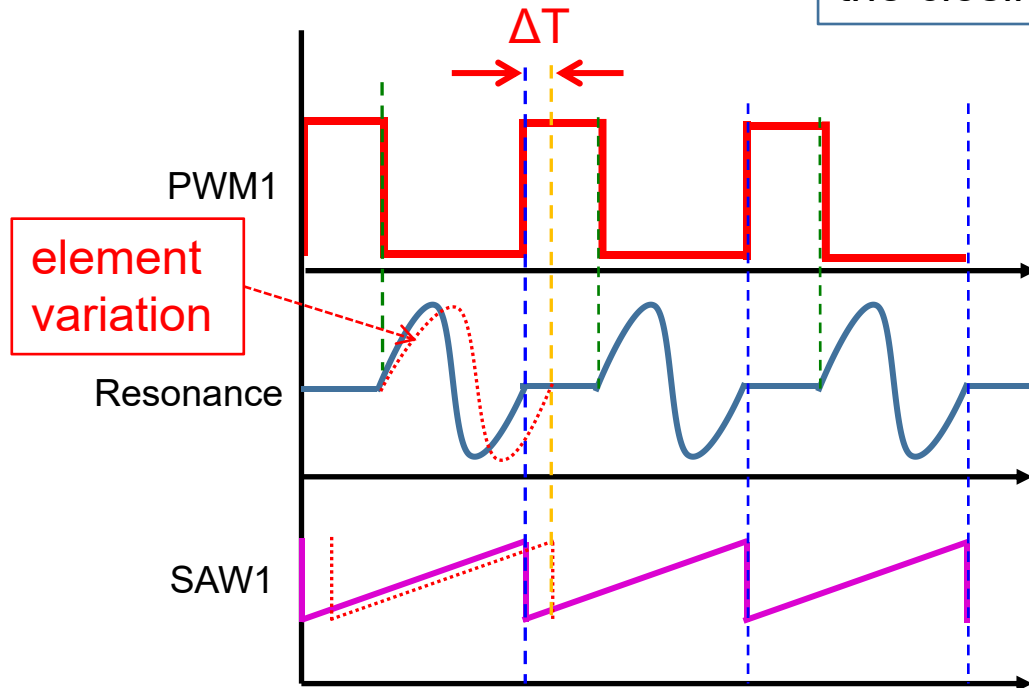
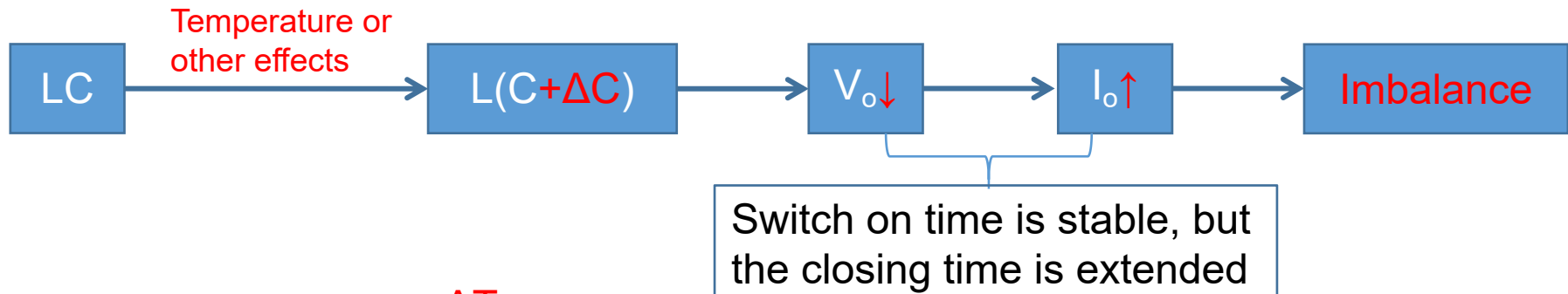


Fig. Signals of dual phase converter

- Research background
- Full/Half wave type soft switching converter
- **Automatic current balance technology**

Conclusion

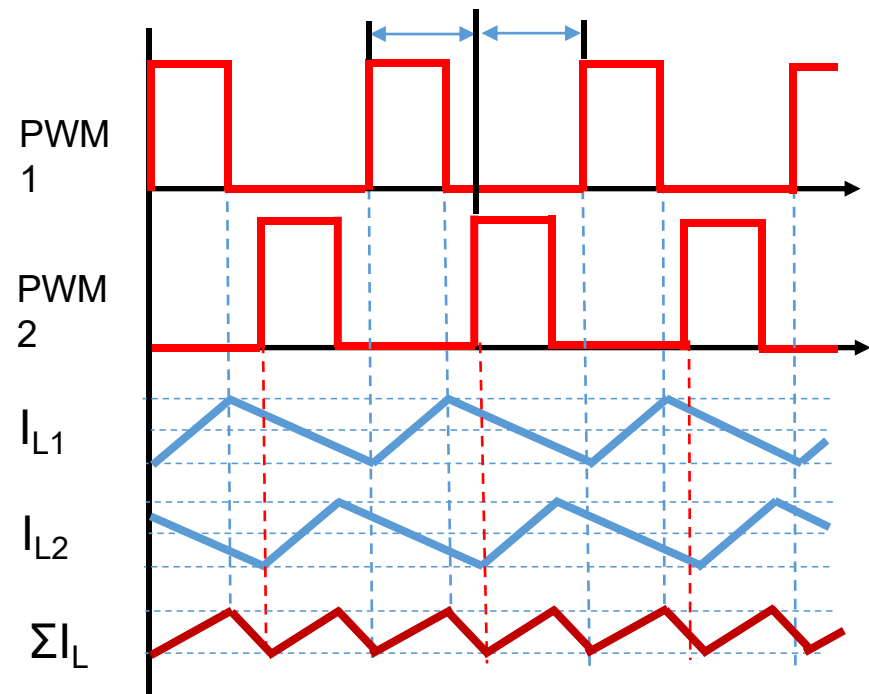
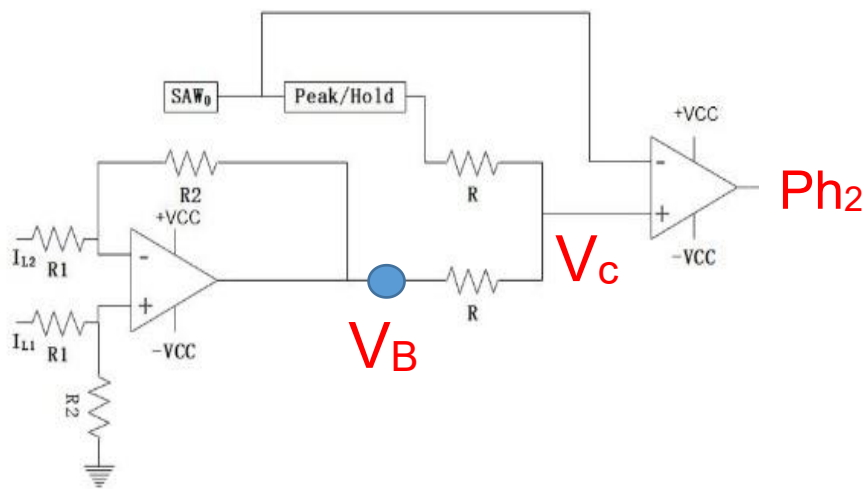
Imbalance of Dual-Phase Converter



$$V_o \downarrow = V_{in} \cdot \frac{T_{on}}{T_{on} + T_{off} \uparrow}$$

Automatic Current balance Technology

- * When phase2 is shift to delay, the current I_{L2} will decrease.
- * Detecting the current balance, When $I_{L2} > I_{L1}$, make the bias voltage V_B down.
 \Rightarrow Phase 2 shifts delayed and I_{L2} is decreased.



Imbalance of Dual-Phase Converter

* Current balance

1) Current balance

with ideal elements

2) Current **imbalance**

with **element variation**



● Demerit of current imbalance

1) Output ripple increases!

2) Inductor current increases
& loss goes up & heat up.

3) Semiconductor (SW) needs
large current & heat capacity

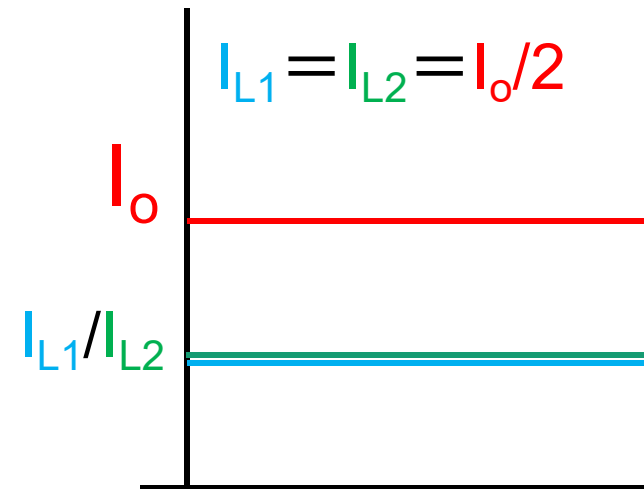


Fig. Current balance with ideal elements

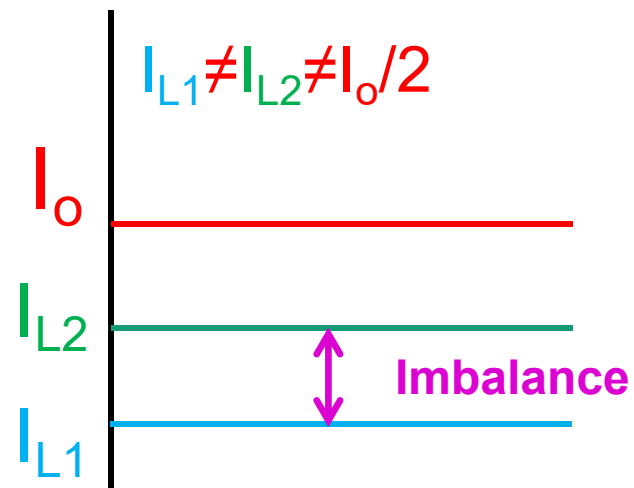
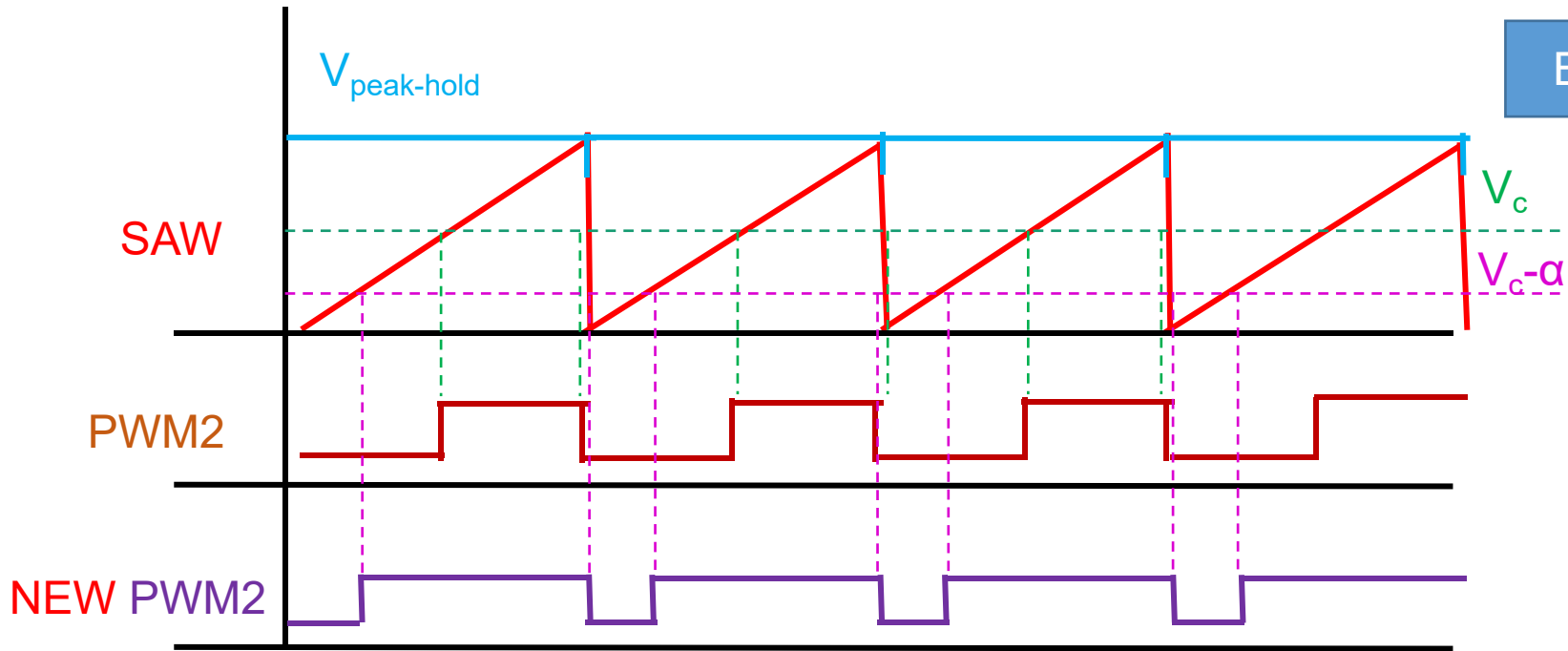
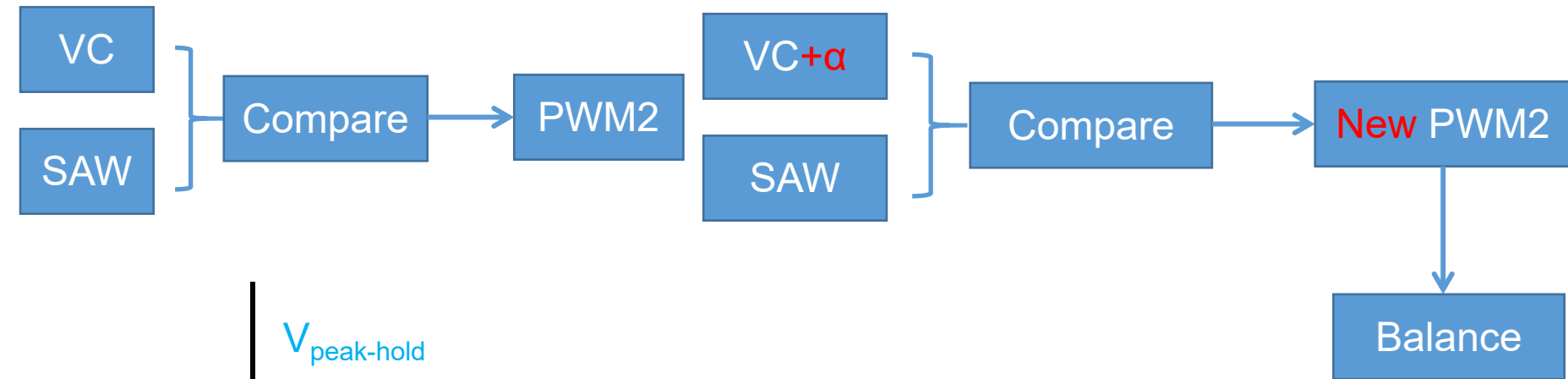


Fig. Current imbalance with element variation

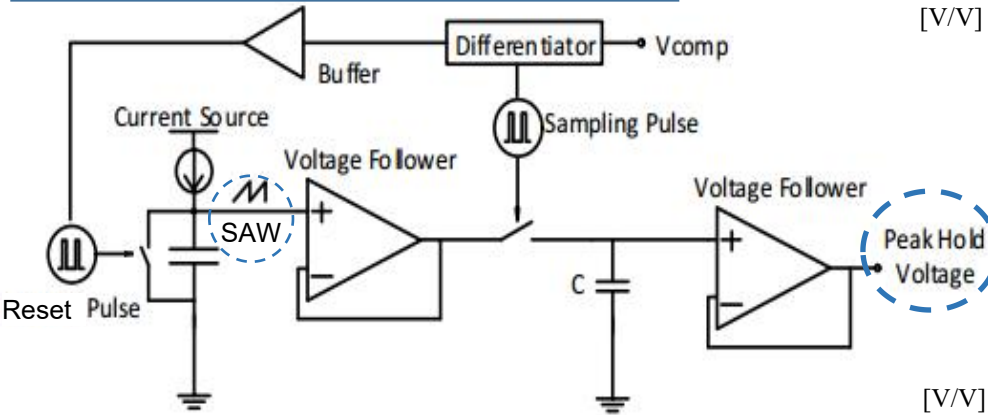
Automatic Current balance Technology



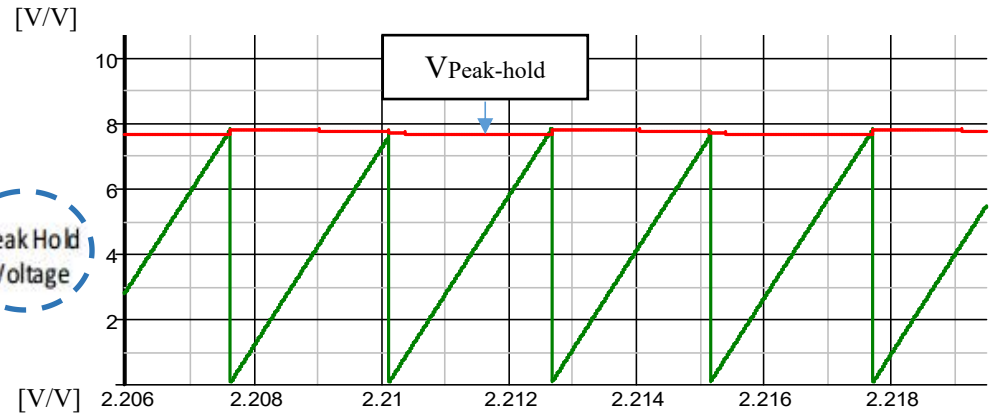
Current balance control signal

Generation of Four-Phase Pulses

SAW Generator & Peak Hold



Operation waveform



Voltage Divider & Comparator

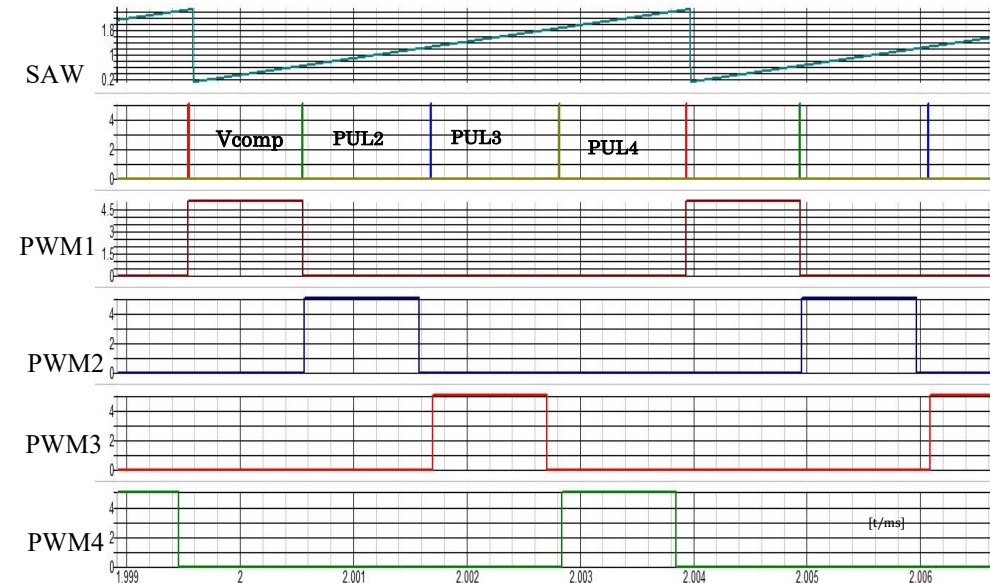
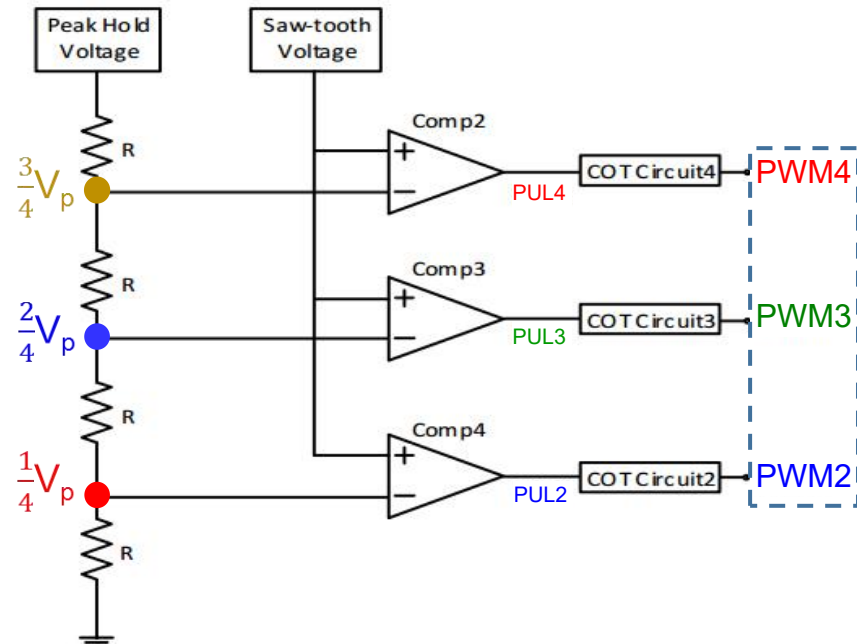
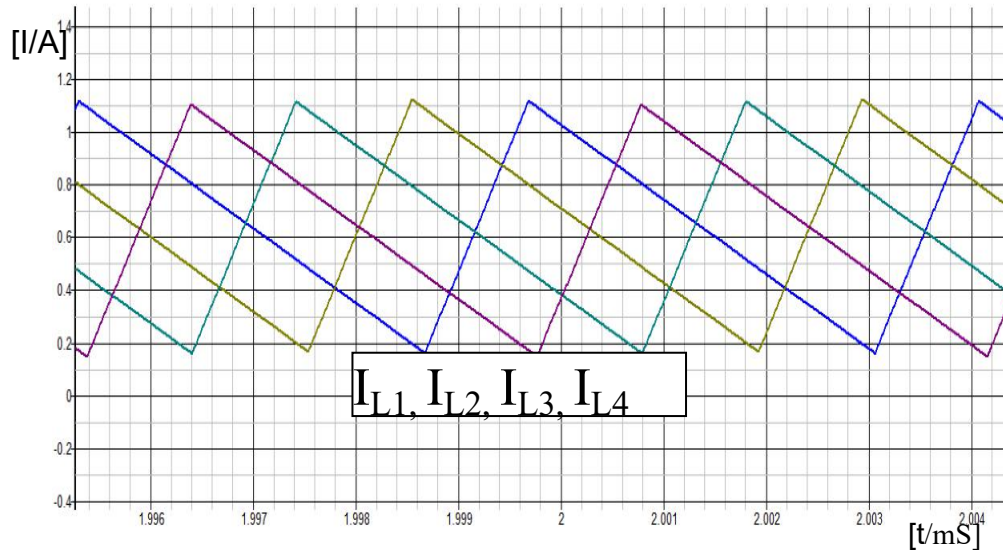


Fig. Signals of Four-phase converter

Current Balance of four-phase Converter

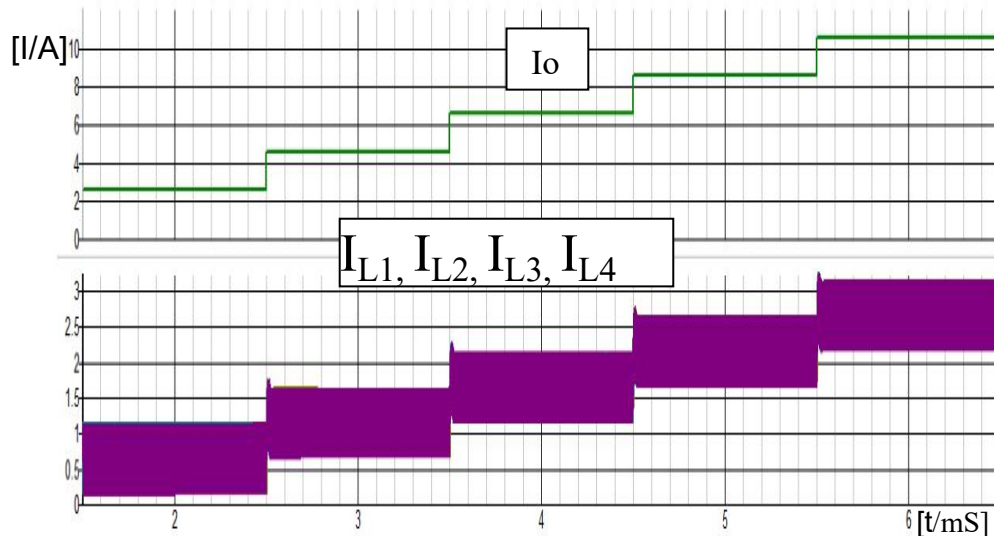
★ Simulation Result



Without element variations
 ΔL , $\Delta T_{CO T}(= \Delta C)$, $\Delta V_{S/H}$



Good current balance



Large load current achieved



Good current balance
 during transient response

Imbalance current (Dual-phase)

● **Two Phase:** With element variation (Inductance)



10μH → 11μH

+ 10%

Inductor

Main power supply

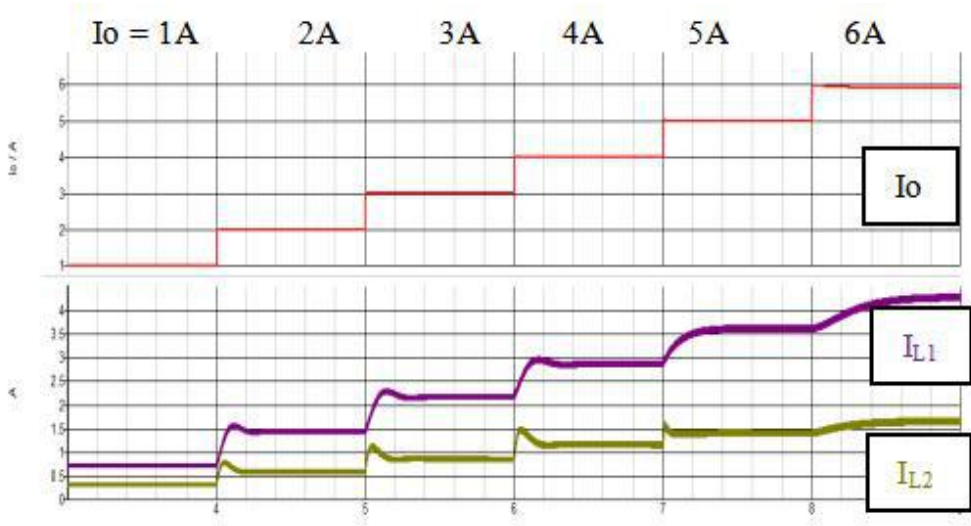


Fig. Dual-phase current imbalance

$I_o = 6A$

$I_{L1} = 4.3A , I_{L2} = 1.7A$

$$\Delta I_L = (I_{L1} - I_{L2}) \dots$$

$$= |4.3 - 1.7| = 2.6A$$

Error Ratio:

$$\delta = (I_o/2 - I_n) / I_o/2$$

$$= (3 - 1.7) / 3 \Rightarrow 43\%$$



Balance current(Dual-phase)

- **Two Phase** : Result of **proposed method** with good current balance



Inductor

10 μ H \rightarrow 11 μ H

+ 10%

Main power supply

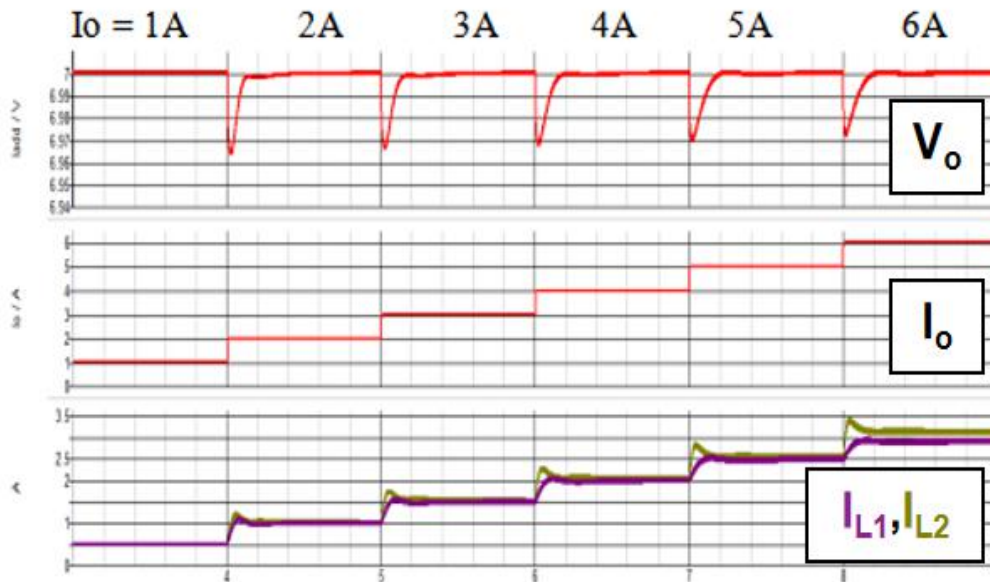
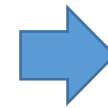


Fig. Multi-phase current balance



Good current balance

$I_o = 6A$

$I_{L1} = I_{L2} = 3A$



Imbalance current (Multi-phase)

● **Four Phase:** With element variation (Inductance)

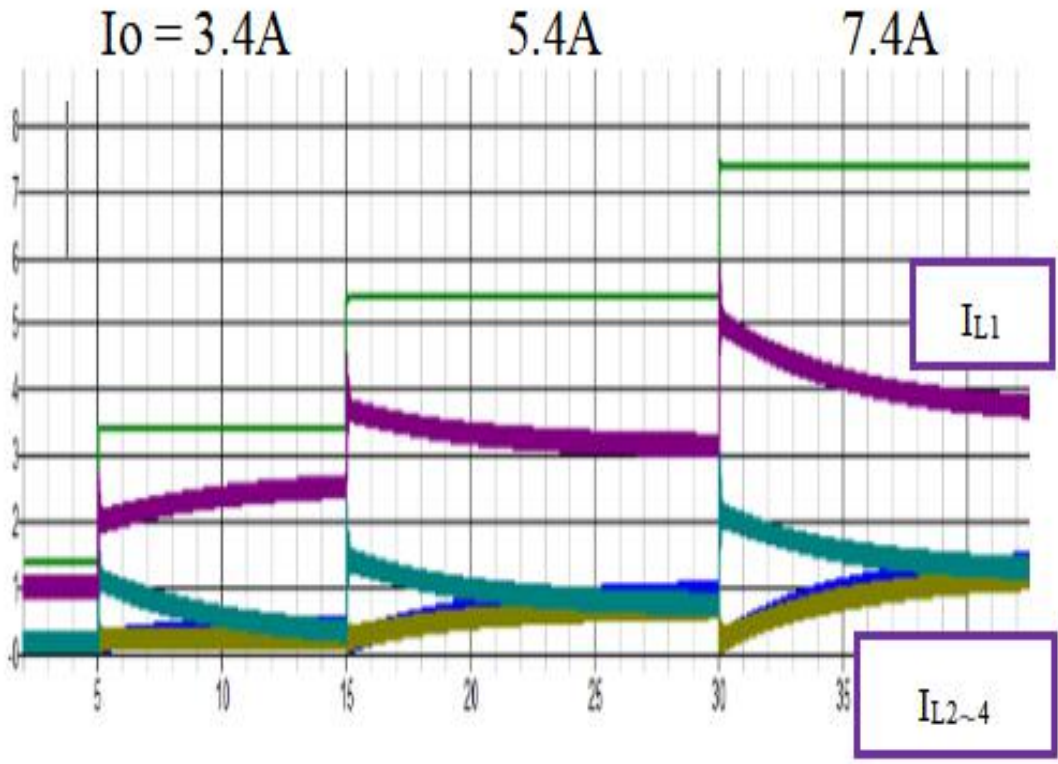


10μH → 11μH

+ 10%

Inductor

Main power supply



$$I_o = 8.58A$$

$$I_{L1} = 5.43A, I_{L2} = 3.15A$$

$$\Delta I_L = (I_{L1} - I_{L2}) \dots$$

$$= |5.43 - 3.15| = 2.28A$$

Error Ratio:

$$\delta = (I_o/2 - I_n) / I_o/2$$

$$= (4.29 - 3.15) / 4.29 \Rightarrow 27\%$$



Fig. Multi-phase current imbalance

Balance current(Multi-phase)

● **Four Phase** : Result of **proposed method** with good current balance

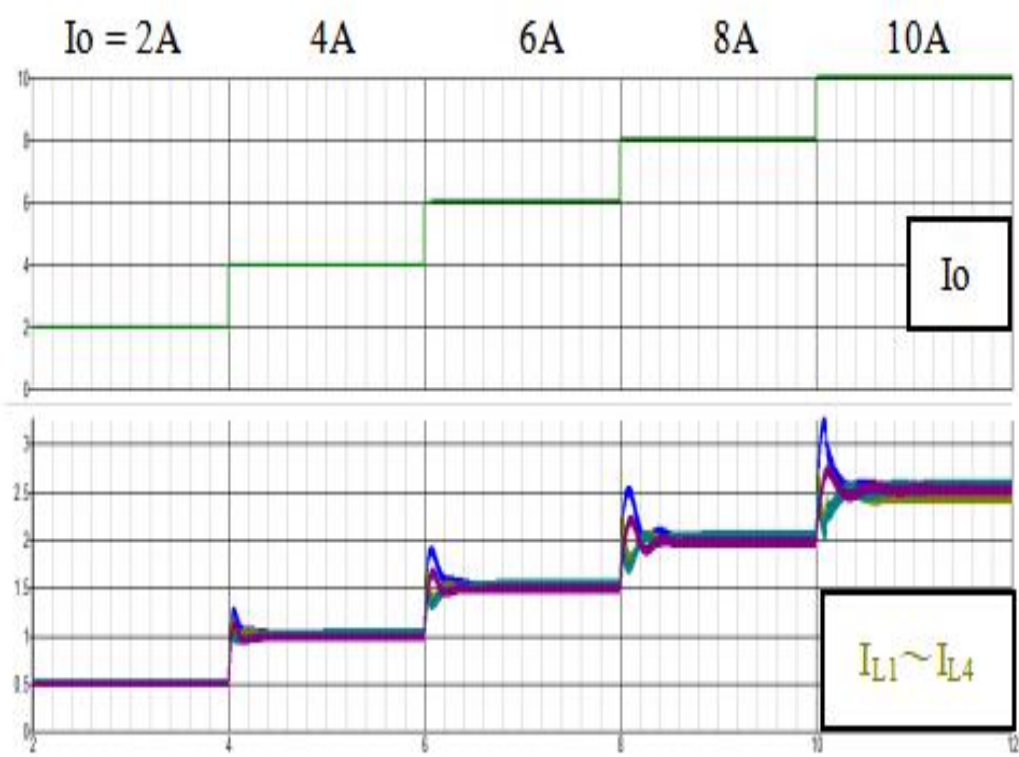


10 μ H \rightarrow 11 μ H

+ 10%

Inductor

Main power supply



➔ **Good current balance**

$I_o = 6.81A$

$I_{L1} = I_{L2} = 3.40A$



Fig. Multi-phase current balance

Conclusion

- The peak hold voltage is extracted by the peak hold circuit to compare it with the SAW1 signal, producing a SAW2 signal with a 180° delay, thereby implementing a dual wave converter without a clock signal. This method has automatic adjustment capability and has faster response speed than traditional PLL methods.
- We have proposed multi-phase full wave and half wave type voltage resonant converters with automatic current balance against the LC elements variation.

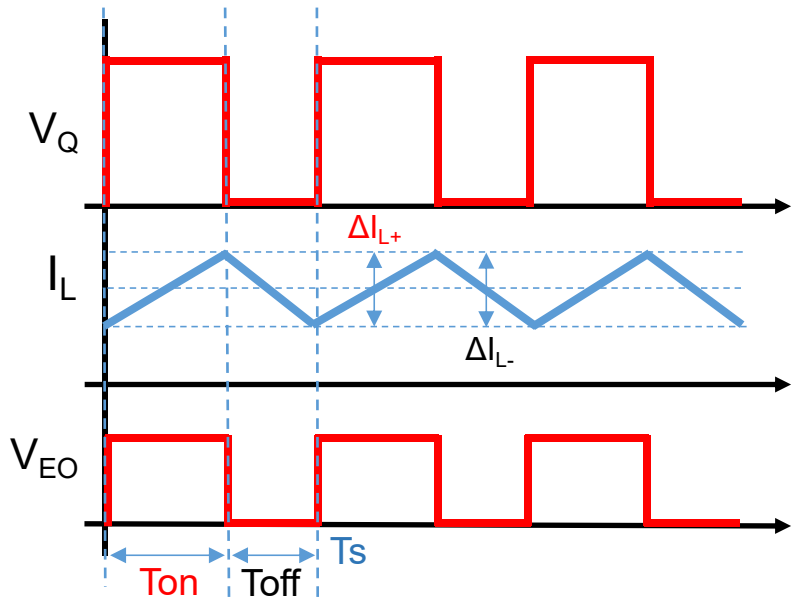
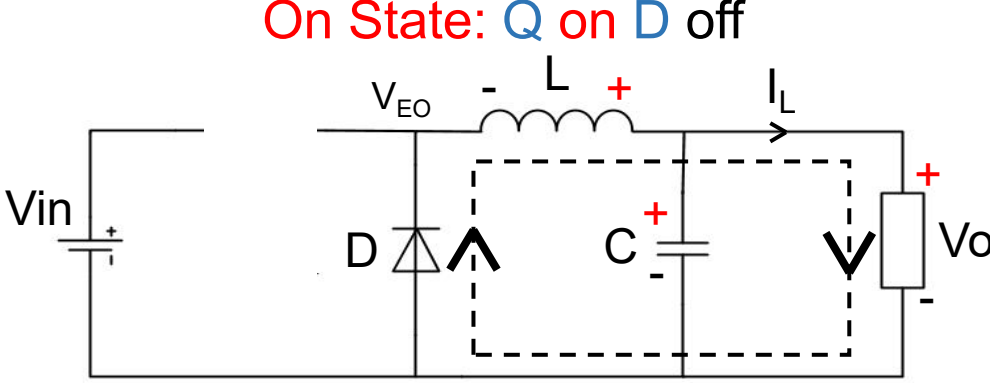
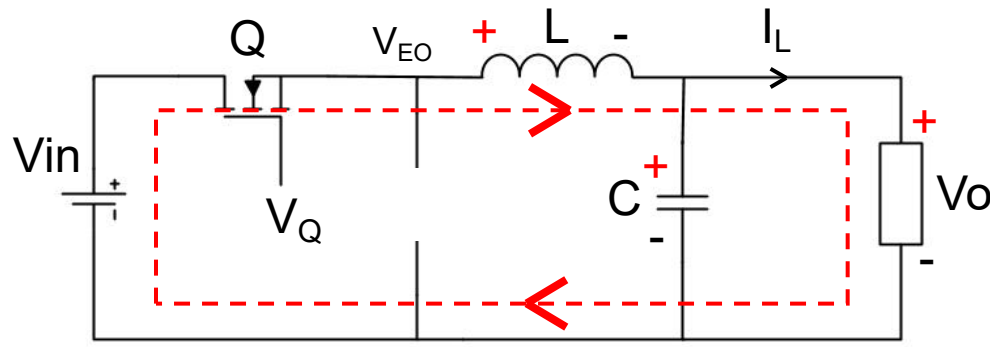
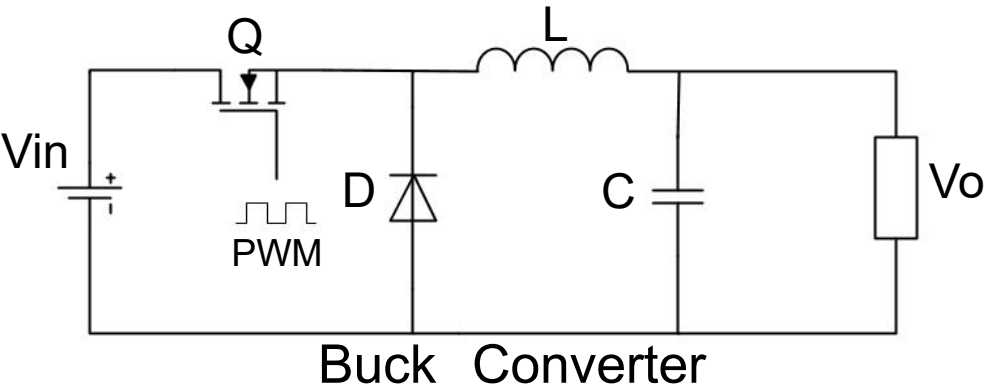
Thank you for your attention

Q&Aに必要と思われる資料を
以下に添付しておくが良い



重庆学会-張湛豪.p
df

Operation of Buck Converter



On State

$$V_{Lon} = V_{in} - V_o = L \cdot (\Delta i_{L+} / \Delta t_{on})$$

Off State

$$V_{Loff} = -V_o = L \cdot (\Delta i_{L-} / \Delta t_{off})$$

Volt-second balance

$$\Delta i_{L+} = \Delta i_{L-}$$

$$V_o = V_{in} \frac{T_{on}}{T_s}$$